

Appendix D

Field data sheets

MOISTURE FIELD DATA SHEET

Project No.: 121511269

Client: Northern Pulp

Plant: Pictou, NS

Location: LIME KILN

Test: PM-1

Date: Aug 21/2014

Analyst: NLM



Stantec

0516-5

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	873.7	630.2	243.5
2	100 mL H ₂ O	774.0	702.5	71.5
3	Blank	643.8	633.8	10
4	200g Silica Gel	1012.0	1000.6	11.4
Total Weight Gain (g)				336.4
Moisture Volume (mL)				336.4

Volume H₂O Collected: 336.4 ml
 $\times 0.048 =$ 16.15 ft³ H₂O (Vwc)

DGM Final 744.55 ft³
 DGM Initial 714.29 ft³
 Final - Initial = 30.26 ft³ (Vmc)

Moisture = $\frac{Vwc}{(Vwc + Vmc)}$

Moisture = $\frac{16.15}{16.15 + 30.26}$

Moisture = 0.35 %

1/2

SOURCE TESTING FIELD DATA SHEET

Job No.: 121511269
 Client: Northern Awp
 Plant: Pichon, MS
 Location: Line Kill
 Test: PM-1
 Date: 21-2-2017
 Operators: TGA/ES
 Gamma: 1.040
 Delta H0: 1.466
 Pitot Coeff.: 0.917
 Start: 8.15
 Finish: 10.30

Static Pressure (in.H2O): 0.51
 Port Length (in): 6.11
 Stack Dia. (in.): 4.311
 Probe Length (ft): 8.1
 Nozzle ID (in.): 3-6 (0.137)
 Console S/N: 1243

Pre-Test Leak Check: 0
 Vacuum Pressure: -1.7
 Post-Test Leak Check: 0
 Vacuum Pressure: -1.3

K: 0.54

Traverse Point	Time (min)	Stack Gas Temp., Ts (F)	Velocity Head, dp (in.H2O)	Orifice dH (in.H2O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F) In Out	Pump Vacuum (in.Hg)
1	2.5	165	0.62	0.32	744.70	285	210	61	64 64	-1
2	5	164	0.68	0.31	745.43	294	225	62	66 64	-1
3	7.5	164	0.65	0.29	746.17	299	226	60	65 64	-1
4	10	105	0.64	0.27	747.90	298	225	60	65 64	-1
5	12.5	165	0.60	0.27	748.58	298	227	60	65 64	-1
6	15	166	0.58	0.26	748.97	299	229	61	65 64	-1
7	17.5	166	0.53	0.24	749.66	299	226	61	65 64	-1
8	20	160	0.51	0.23	750.29	299	227	61	65 64	-1
9	22.5	165	0.45	0.20	750.86	298	210	60	64 64	-1
10	25	166	0.44	0.20	751.46	298	225	60	65 64	-1
11	27.5	166	0.40	0.18	752.03	300	225	60	65 64	-1
12	30	165	0.38	0.17	752.58	300	226	59	65 64	-1
13	32.5	166	0.49	0.22	753.21	300	228	59	65 64	-1
14	35	166	0.49	0.22	753.94	301	227	59	65 64	-1
15	37.5	166	0.50	0.23	754.60	299	229	59	65 64	-1
16	40	165	0.47	0.22	755.11	300	227	57	65 64	-1
17	42.5	165	0.45	0.20	755.70	300	225	56	65 64	-1
18	45	165	0.44	0.20	756.26	301	227	56	66 65	-1
19	47.5	165	0.35	0.16	756.82	300	224	57	66 65	-1
20	50	165	0.38	0.17	757.33	299	225	56	66 65	-1
21	52.5	165	0.35	0.16	757.90	301	226	57	66 65	-1
22	55	165	0.35	0.16	758.42	300	227	57	66 65	-1
23	57.5	165	0.38	0.17	758.97	300	229	57	66 65	-1
24	60	164	0.37	0.16	759.51	300	229	55	66 65	-1

7/2

SOURCE TESTING FIELD DATA SHEET

Job No.: 121511269
 Client: Northern Pulp
 Plant: Pittsburg, N.S.
 Location: Line Kiln
 Test: PM-1
 Date: Aug 21, 2011
 Operators: TRH/ES
 Gamma: 1.040
 Delta H₀: 1.766
 Pilot Coeff.: 0.817
 Start: 10:30
 Finish:

Static Pressure (in.H₂O): 0.51
 Port Length (in): 6"
 Stock Dia. (in.): 4 1/2"
 Probe Length (ft): 8'
 Nozzle ID (in.): 1/6 (0.167)
 Console SN: 12418

Pre-Test Leak Check:
 Vacuum Pressure:
 Post-Test Leak Check:
 Vacuum Pressure:

K: 0.54

Transverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dP (in.H ₂ O)	Orifice dH (in.H ₂ O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in.Hg)
									In	Out	
1	2.5	164	0.158	0.31	760.22	300	231	53	69	66	-1
	5	164	0.163	0.29	760.93	298	234	53	68	66	-1
2	7.5	164	0.160	0.27	761.64	294	231	59	67	67	-1
	10	164	0.161	0.28	762.33	300	230	59	68	67	-1
3	12.5	164	0.159	0.27	763.04	300	231	59	69	67	-1
	15	164	0.157	0.27	763.73	301	231	59	69	67	-1
4	17.5	164	0.156	0.26	764.42	301	231	59	69	67	-2
	20	164	0.155	0.25	765.11	299	233	60	69	69	-2
5	22.5	166	0.145	0.21	765.77	300	231	60	69	68	-2
	25	167	0.146	0.21	766.33	301	231	60	69	68	-2
6	27.5	165	0.140	0.19	766.92	300	232	61	70	68	-2
	30	165	0.138	0.17	767.40	300	231	62	70	68	-2
7	32.5	165	0.135	0.16	768.00	300	233	62	70	69	-2
	35	165	0.135	0.16	768.55	300	233	63	71	70	-2
8	37.5	165	0.148	0.22	769.16	300	232	59	73	69	-2
	40	165	0.149	0.22	769.79	300	234	59	73	70	-2
9	42.5	165	0.147	0.21	770.40	300	232	54	72	70	-2
	45	165	0.148	0.20	771.01	300	232	53	72	70	-3
10	47.5	166	0.142	0.19	771.60	301	233	52	73	70	-3
	50	165	0.141	0.18	772.19	302	233	54	73	71	-3
11	52.5	164	0.142	0.19	772.89	300	236	53	73	71	-3
	55	165	0.135	0.16	773.37	300	235	54	73	71	-3
12	57.5	165	0.130	0.14	773.82	301	236	54	73	71	-3
	60	165	0.133	0.15	774.34	300	235	55	74	72	-3

22
-15
-8
-5
0
0
5
10
10
15
15
18
25

Sampling Methodology: Environment Canada EPS 1/RM/15

Personnel: TBH

[illegible]

MOISTURE FIELD DATA SHEET

Project No.: 121511269

Client: Northern Pulp

Plant: Pictou, NS

Location: Lime Kiln

Test: PM-2

Date: Aug 22, 2014

Analyst: T&H



Stantec

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	465.3	620.0	
2	100 mL H ₂ O	731.3	409.7	
3	Blank	635.4	634.2	
4	200g Silica Gel	1017.8	1011.8	
Total Weight Gain (g)				
Moisture Volume (mL)				

Volume H₂O Collected: _____ ml
 X 0.048 = _____ ft³ H₂O (Vwc)

DGM Final _____ ft³
 DGM Initial _____ ft³
 Final - Initial = _____ ft³ (Vmc)

Moisture = $\frac{Vwc}{(Vwc + Vmc)}$

Moisture = _____

Moisture = _____

SOURCE TESTING FIELD DATA SHEET

Job No.: 121511267
 Client: Northern Pump
 Plant: Pickens
 Location: 1000 Kellin
 Date: Aug 21, 2014
 Operators: TBH/ES
 Gamma: 1.040
 Delta H: 1.746
 Pilot Coeff.: 0.817
 Start: 0.70
 Finish: 11:30

Static Pressure (in.H2O): 0.51
 Port Length (in): 6.5
 Stack Dia. (in.): 4.8
 Probe Length (ft): 8
 Nozzle ID (in.): 2-6 (0.173)
 Console S/N: 1648

Pre-Test Leak Check: ☒
 Vacuum Pressure: -13
 Post-Test Leak Check: ☒
 Vacuum Pressure: -13

K: 0.54

Traverse Point	Time (min)	Stack Gas Temp, T _s (°F)	Velocity Head, dp (in.H2O)	Orifice dH (in.H2O)	Gas Meter Volume (cu.ft)	Probe Temp. (°F)	Oven Temp. (°F)	Impinger Outlet Temp. (°F)	Gas Meter Temp. (°F)	Pump Vacuum (in.Hg)
1	0	163	0.67	0.31	711.29	299	237	68	67	-1
2	5	163	0.68	0.31	715.03	299	241	68	67	-1
3	10	161	0.65	0.30	715.95	299	242	67	67	-1
4	12.5	161	0.63	0.30	717.19	300	240	67	68	-1
5	15	161	0.60	0.29	717.92	297	248	67	68	-1
6	17.5	161	0.58	0.27	718.60	300	258	67	71	-1
7	20	161	0.55	0.25	719.27	300	258	67	71	-1
8	22.5	161	0.50	0.23	719.95	299	254	67	70	-1
9	25	162	0.50	0.23	720.57	299	256	67	70	-1
10	27.5	162	0.45	0.21	721.20	299	257	67	72	-1
11	30	162	0.45	0.21	721.81	301	259	67	72	-1
12	32.5	162	0.43	0.20	722.40	296	259	67	73	-1
13	35	162	0.40	0.19	723.01	296	260	67	73	-1
14	37.5	162	0.39	0.18	723.55	298	260	67	75	-1
15	40	162	0.39	0.18	724.12	299	260	67	75	-1
16	42.5	162	0.50	0.24	724.70	299	260	67	76	-1
17	45	163	0.50	0.24	725.30	298	261	67	76	-1
18	47.5	163	0.52	0.24	725.96	299	261	67	76	-1
19	50	161	0.51	0.24	726.67	300	263	67	76	-1
20	52.5	161	0.45	0.21	727.26	300	263	67	76	-1
21	55	161	0.43	0.21	727.87	299	263	67	77	-1
22	57.5	161	0.43	0.21	728.48	300	263	67	77	-1
23	60	159	0.43	0.20	729.08	301	264	67	78	-1
24	62.5	159	0.43	0.20	729.68	300	265	67	79	-1
25	65	159	0.43	0.20	729.68	300	265	67	79	-1

2/2

SOURCE TESTING FIELD DATA SHEET

Job No.: 12111269
 Client: Northern Pulp
 Location: Limerick
 Test: PM-2
 Date: Aug 21, 2014
 Operators: TBH/ES
 Gamma: 1.042
 Delta H: 1.366
 Phot Coeff: 0.913
 Start: 9:20
 Finish: 11:30

Static Pressure (in.H2O): 0.51
 Port Length (in.): 6"
 Stack Dia. (in.): 4.8"
 Probe Length (ft): 8'
 Nozzle ID (in.): 7/16 (123)
 Console S/N: 1328

Pre-Test Leak Check:
 Vacuum Pressure:
 Post-Test Leak Check:
 Vacuum Pressure:

K: 0.54

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dP (in.H2O)	Orifice dH (in.H2O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in.Hg)
									In	Out	
1	0	151	0.65	0.31	729.63	301	257	68	84	87	-1
2	5	140	0.66	0.31	731.15	301	261	65	85	87	-1
3	10	162	0.64	0.30	731.88	300	264	63	87	84	-1
4	15	160	0.65	0.30	732.60	298	263	61	87	83	-1
5	20	161	0.60	0.28	733.30	298	261	61	88	83	-1
6	25	162	0.58	0.27	733.99	298	263	60	89	84	-1
7	30	162	0.54	0.25	734.65	299	261	59	89	84	-2
8	35	163	0.52	0.24	735.29	299	261	59	89	85	-2
9	40	162	0.52	0.24	735.93	297	261	59	89	85	-2
10	45	167	0.50	0.23	736.58	296	260	59	89	85	-2
11	50	162	0.43	0.20	737.17	297	259	60	89	85	-2
12	55	164	0.40	0.19	737.78	295	261	60	89	85	-2
13	60	164	0.41	0.19	738.35	301	261	61	89	85	-2
14	65	164	0.42	0.19	738.93	298	260	61	89	85	-2
15	70	163	0.41	0.19	739.53	295	253	61	89	86	-2
16	75	163	0.40	0.19	740.11	291	260	61	89	86	-2
17	80	161	0.43	0.20	740.71	292	260	61	89	86	-2
18	85	162	0.44	0.21	741.30	302	260	62	89	85	-2
19	90	161	0.40	0.19	741.91	298	260	62	89	85	-2
20	95	157	0.35	0.16	742.42	300	258	62	89	85	-2
21	100	156	0.39	0.13	742.85	299	261	60	89	85	-2
22	105	161	0.33	0.16	743.40	300	260	59	89	85	-2
23	110	163	0.35	0.13	743.95	294	260	60	89	85	-2
24	115	161	0.36	0.13	744.55	290	259	60	88	85	-2

Sampling Methodology: Environment Canada EPS 1/RM/15

Personnel: TJH

[illegible]

MOISTURE FIELD DATA SHEET

Project No.: 121511269
 Client: NORTHERN PULP
 Plant: PICTON NB
 Location: LIME HILL
 Test: PM-3
 Date: AUG 22/2014
 Analyst: NLM



Filter 10
0516-8

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H2O	1023.9	714.5	
2	100 mL H2O	751.7	734.1	
3	Blank	633.9	632.1	
4	200g Silica Gel	952.7	944.4	
Total Weight Gain (g)				
Moisture Volume (mL)				

Volume H₂O Collected: _____ ml
 X 0.048 = _____ ft³ H₂O (Vwc)

DGM Final _____ ft³
 DGM Initial _____ ft³
 Final - Initial = _____ ft³ (Vmc)

Moisture = $\frac{Vwc}{(Vwc + Vmc)}$

Moisture = _____

Moisture = _____

1/2

SOURCE TESTING FIELD DATA SHEET

Job No.: 121511269
 Client: Northern
 Plant: Northern
 Location: Kilauea
 Test: PM-3
 Date: Aug 22, 2014
 Operators: THT/FS
 Gamma: 1.049
 Delta H₂O: 1.746
 Pilot Coeff.: 0.817
 Start: 1:05
 Finish: 1:00

Static Pressure (in.H₂O): 0.51
 Port Length (in): 6.4
 Stack Dia. (in.): 4.2
 Probe Length (ft): 8
 Nozzle ID (in.): 2.6 (0.127)
 Console S/N: 1343

Pre-Test Leak Check: 0
 Vacuum Pressure: -13
 Post-Test Leak Check: 0
 Vacuum Pressure: -68

K: 0.27

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dp (in.H ₂ O)	Orifice dH (in.H ₂ O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in.Hg)
									In	Out	
1	0	161	0.66	0.30	724.53						
2	7.5	165	0.64	0.30	775.76	225	225	60	71	71	-1
3	10	165	0.60	0.28	775.88	248	226	60	71	70	-1
4	12.5	165	0.39	0.27	776.70	258	225	60	72	71	-1
5	15	162	0.58	0.29	778.51	264	227	59	72	71	-1
6	17.5	164	0.57	0.26	778.70	266	228	59	72	71	-1
7	19.5	167	0.59	0.27	779.83	269	225	58	72	71	-1
8	22	165	0.56	0.26	780.53	273	227	58	72	72	-1
9	24.5	164	0.52	0.24	780.56	273	226	58	72	72	-1
10	27	163	0.47	0.27	780.74	275	230	57	72	72	-1
11	30	164	0.45	0.21	781.36	270	231	56	71	71	-1
12	32.5	163	0.44	0.20	781.93	266	229	57	71	71	-1
13	35	163	0.47	0.22	782.57	262	226	57	72	71	-1
14	37.5	162	0.48	0.22	783.19	266	226	57	72	71	-1
15	40	165	0.45	0.21	783.82	266	228	57	73	73	-1
16	42.5	165	0.44	0.20	784.47	264	230	57	73	73	-1
17	45	162	0.41	0.19	785.07	264	231	60	74	73	-1
18	47.5	162	0.38	0.18	785.68	264	233	61	74	73	-1
19	50	163	0.35	0.16	786.16	265	235	61	75	73	-1
20	52.5	163	0.37	0.17	786.67	269	237	62	74	74	-1
21	55	163	0.30	0.17	787.20	267	237	63	74	74	-1
22	57.5	164	0.29	0.13	787.68	265	238	59	73	73	-1
23	60	161	0.32	0.15	788.17	265	239	51	73	73	-1
24	62	161	0.35	0.16	788.69	266	239	51	73	73	-1
25	64	161	0.35	0.16	789.26	266	239	51	73	73	-1

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SOURCE TESTING FIELD DATA SHEET

Job No.: 121511265
 Client: Northern P-10
 Plant: Victoria NS
 Location: 11-1-1212
 Test: PM-9
 Date: Aug 23, 2014
 Operators: TGH/AS
 Gamma: 1.240
 Delta H₂O: 1.766
 Pilot Coeff.: 0.817
 Start: 11:05
 Finish: 1:10

Static Pressure (in.H₂O): 0.51
 Port Length (in): 6"
 Stock Dia. (in.): 43"
 Probe Length (ft): 8'
 Nozzle ID (in.): 3-6 (0.173)
 Console S/N: 1543

Pre-Test Leak Check: 0
 Vacuum Pressure: -18
 Post-Test Leak Check: 0
 Vacuum Pressure: -8

K: 0.54

Traverse Point	Time (min)	Stack Gas Temp., T _s (°F)	Velocity Head, dP (in.H ₂ O)	Orifice dH (in.H ₂ O)	Gas Meter Volume (cu.ft)	Probe Temp. (°F)	Oven Temp. (°F)	Impinger Outlet Temp. (°F)	Gas Meter Temp. (°F)		Pump Vacuum (in.Hg)
									In	Out	
1	2.5	163	0.65	0.30	789.881	263	241	49	72	73	-1
2	5	162	0.65	0.30	790.413	264	240	49	72	73	-1
3	7.5	161	0.60	0.28	791.14	268	239	50	72	72	-1
4	10	161	0.59	0.27	791.81	261	239	48	72	72	-1
5	12.5	161	0.57	0.26	792.48	258	238	48	72	71	-1
6	15	162	0.56	0.26	793.10	257	238	48	72	71	-1
7	17.5	162	0.49	0.23	793.79	257	238	60	72	71	-1
8	20	163	0.50	0.23	794.208	254	238	50	72	72	-1
9	22.5	164	0.45	0.21	795.03	255	236	51	72	73	-1
10	25	164	0.43	0.20	795.61	257	239	53	72	72	-1
11	27.5	163	0.40	0.18	796.18	260	237	54	74	72	-1
12	30	163	0.38	0.17	796.75	261	239	54	74	73	-1
13	32.5	163	0.35	0.16	797.24*	262	240	54	76	73	-1
14	35	163	0.40	0.18	797.81	264	241	55	76	74	-1
15	37.5	163	0.47	0.22	798.47	269	243	55	76	74	-1
16	40	163	0.47	0.27	799.05	270	243	54	76	74	-1
17	42.5	163	0.45	0.21	799.66	270	244	54	76	76	-1
18	45	163	0.44	0.20	800.23	271	245	54	76	76	-1
19	47.5	163	0.42	0.19	800.80	269	246	54	76	76	-1
20	50	163	0.41	0.19	801.37	267	246	54	75	75	-1
21	52.5	163	0.37	0.18	801.96	268	247	54	75	75	-1
22	55	163	0.38	0.17	802.44	268	247	54	76	75	-1
23	57.5	164	0.35	0.16	802.97	267	248	57	76	76	-1
24	60	164	0.39	0.18	803.53	269	247	57	76	75	-1

-15
-10
-8
-5
0
0
0
5
8
12
15
20

Sampling Methodology: Environment Canada EPS 1/RM/15

Personnel: TBH

[illegible]

MOISTURE FIELD DATA SHEET

Project No.: 121511269

Client: Northern Pulp

Plant: Pictou, NS

Location: Recovery Boiler

Test: PM-1

Date: Aug 19, 2014

Analyst: C.M.



Stantec

FILTR
0128-14

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	907.9	626.7	281.2
2	100 mL H ₂ O	974.0	737.3	236.7
3	Blank	662.6	632.0	30.6
4	200g Silica Gel	1028.8	995.7	33.1
Total Weight Gain (g)				581.6
Moisture Volume (mL)				581.6

$$\text{Volume H}_2\text{O Collected: } \frac{581.6}{27.92} \text{ ml} \\ \times 0.048 = \text{ft}^3 \text{ H}_2\text{O (Vwc)}$$

$$\begin{aligned} \text{DGM Final} &= 530.75 \text{ ft}^3 \\ \text{DGM Initial} &= 470.18 \text{ ft}^3 \\ \text{Final - Initial} &= 60.57 \text{ ft}^3 \text{ (Vmc)} \end{aligned}$$

$$\text{Moisture} = \frac{\text{Vwc}}{(\text{Vwc} + \text{Vmc})}$$

$$\text{Moisture} = \frac{27.92}{27.92 + 60.57}$$

$$\text{Moisture} = 0.315$$

SOURCE TESTING FIELD DATA SHEET

Job No.: 121811269
 Client: Northern Pulp
 Plant: Pulp Mill
 Location: 3610000000
 Test: PM-1
 Date: Aug 19, 2014
 Operators: T817 / M.M.
 Gamma: 1.040
 Delta H@: 1.205
 Pilot Coeff.: 0.833
 Start: 11:10
 Finish: 1:30

Static Pressure (in.H2O): 1.10
 Port Length (in): 6.1
 Stack Dia. (in): 13.8
 Probe Length (ft): 2.1
 Nozzle ID (in): 1.8 (0.235)
 Concrete S/N: 18849

Pre-Test Leak Check:
 Vacuum Pressure:
 Post-Test Leak Check:
 Vacuum Pressure:

K: 1.68

Traverse Point	Time (min)	Stack Gas Temp., T _g (F)	Velocity Head, dP (in.H2O)	Orifice dH (in.H2O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in.Hg)
									In	Out	
1	0	154	0.64	0.91	470.18	275	225	73	72	6.9	-1
2	2.5	154	0.70	0.92	473.00	275	220	73	62	6.2	-1
3	7.5	157	0.66	0.94	473.95	278	237	68	64	6.3	-1
4	10	157	0.65	0.93	475.11	279	243	68	64	6.3	-1
5	12.5	157	0.63	0.90	476.45	278	242	65	65	6.3	-1
6	15	158	0.63	0.87	477.67	273	246	65	66	6.3	-1
1	17.5	156	0.63	0.90	478.91	271	248	65	66	6.3	-1
2	20	157	0.64	0.91	480.15	267	249	65	66	6.3	-1
3	22.5	157	0.64	0.91	481.97	267	250	67	67	6.4	-1
4	25	157	0.61	0.91	482.68	251	252	69	67	6.4	-1
5	27.5	157	0.61	0.87	483.87	248	254	70	68	6.4	-1
6	30	156	0.61	0.87	485.10	248	255	70	69	6.4	-2
1	32.5	157	0.61	0.87	486.95	245	256	70	71	6.6	-2
2	35	160	0.64	0.92	487.60	247	258	70	71	6.6	-2
3	37.5	160	0.63	0.90	488.85	246	259	70	71	6.6	-2
4	40	160	0.62	0.90	490.09	267	260	69	72	6.7	-2
5	42.5	160	0.64	0.93	491.51	270	260	69	72	6.7	-2
6	45	160	0.64	0.92	492.61	273	260	65	73	6.7	-2
1	47.5	156	0.64	0.95	493.90	273	262	65	74	6.8	-2
2	50	157	0.64	0.93	495.17	276	262	65	74	6.8	-2
3	52.5	157	0.63	0.91	496.50	273	263	62	74	6.8	-2
4	55	157	0.61	0.88	497.72	264	264	61	75	6.9	-2
5	57.5	154	0.60	0.87	498.73	260	264	61	75	6.9	-2
6	60	154	0.60	0.87	500.12	260	264	61	75	6.9	-2

SOURCE TESTING FIELD DATA SHEET

Job No.: 121811269
 Client: Northern Pipe
 Plant: Pictou, NS
 Location: Reclamation Pailier
 Test: Pm-1
 Date: Aug 12, 2014
 Operators: TBH/AMM
 Gamma: 1.040
 Delta H₀: 1.305
 Pitot Coeff.: 0.838
 Start: 11:10
 Finish: 1:30

Static Pressure (in.H₂O): 1.10
 Port Length (in): 6"
 Stack Dia. (in.): 13.2
 Probe Length (ft): 21
 Nozzle ID (in.): 1-8 (0.278)
 Console S/N: 1348

Pre-Test Leak Check: ☒
 Vacuum Pressure: -12
 Post-Test Leak Check: ☐
 Vacuum Pressure: ☐

K: 1668

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dP (in.H ₂ O)	Orifice dH (in.H ₂ O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)	Pump Vacuum (in.Hg)
1	2.5	159	0.105	0.94	501.41	230	263	59	75	-4
2	5	158	0.106	0.95	502.72	250	263	59	75	-4
3	7.5	159	0.105	0.94	504.00	255	263	59	74	-4
4	10	160	0.103	0.91	505.27	268	264	58	74	-5
5	12.5	158	0.105	0.94	506.60	277	264	58	74	-5
6	15	158	0.103	0.91	507.95	281	265	59	75	-5
7	17.5	158	0.104	0.93	509.11	284	265	58	76	-5
8	20	157	0.101	0.88	510.28	276	266	58	76	-5
9	22.5	158	0.102	0.90	511.49	275	265	58	77	-5
10	25	157	0.101	0.89	512.90	277	268	59	77	-5
11	27.5	157	0.104	0.93	514.11	272	268	60	77	-5
12	30	157	0.102	0.92	515.39	265	269	59	77	-5
13	32.5	156	0.104	0.93	516.65	268	272	60	77	-6
14	35	161	0.104	0.95	517.92	276	275	60	77	-6
15	37.5	158	0.105	0.95	519.72	283	277	60	77	-6
16	40	159	0.102	0.90	520.46	294	279	60	77	-6
17	42.5	162	0.105	0.97	521.76	293	281	60	77	-7
18	45	161	0.104	0.93	526.03	299	281	60	78	-7
19	47.5	159	0.102	0.90	524.26	300	283	61	78	-7
20	50	154	0.105	0.95	525.56	294	284	62	78	-7
21	52.5	158	0.100	0.90	524.87	292	285	63	78	-7
22	55	154	0.104	0.93	528.17	275	284	63	78	-7
23	57.5	154	0.104	0.97	529.43	267	285	64	77	-7
24	60	155	0.105	0.95	530.75	264	284	64	77	-8

Sampling Methodology: Environment Canada EPS 1/RM/15



Stantec

Location: Recovery Boiler

Fuel Type: _____

Date: Aug 19, 2014

Time Finish: 12:45

Personnel: TBH

[illegible]

MOISTURE FIELD DATA SHEET

Project No.: 121511269

Client: Northern Pulp

Plant: Pictou, NS

Location: RECOVERY BOILER

Test: PM-2

Date: AUG. 19/2014

Analyst: NLM



FILTER 10
0120-17

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	918.2	622.5	295.7
2	100 mL H ₂ O	976.8	701.8	275
3	Blank	645.2	634.6	10.6
4	200g Silica Gel	1047.8	1028.7	19.1
Total Weight Gain (g)				600.4
Moisture Volume (mL)				

$$\text{Volume H}_2\text{O Collected: } \frac{600.4}{1} \text{ ml}$$

$$\times 0.048 = \frac{28.82}{1} \text{ ft}^3 \text{ H}_2\text{O (Vwc)}$$

$$\text{DGM Final } \frac{590.42}{1} \text{ ft}^3$$

$$\text{DGM Initial } \frac{530.97}{1} \text{ ft}^3$$

$$\text{Final - Initial} = \frac{59.45}{1} \text{ ft}^3 \text{ (Vmc)}$$

$$\text{Moisture} = \frac{\text{Vwc}}{(\text{Vwc} + \text{Vmc})}$$

$$\text{Moisture} = \frac{28.82}{(28.82 + 59.45)} \rightarrow \frac{28.82}{88.27}$$

$$\text{Moisture} = \underline{32.6\%}$$

$$\Delta H = k' \times \frac{T_m}{T_b} \times AP \times \frac{1}{2}$$

SOURCE TESTING FIELD DATA SHEET

Job No.: 121211269
 Client: Alcatraz Pump
 Plant: P-100, NJ
 Location: Raccoon River
 Test: P-100-2
 Date: Apr 15, 2014
 Operators: JOR/MAM
 Gamma: 0.040
 Delta H: 1.905
 Pilot Coeff.: 0.353
 Start: 3:00
 Finish:

Static Pressure (in.H2O): 1.10
 Port Length (in.): 6.1
 Stack Dia. (in.): 13.2
 Probe Length (ft): 2
 Nozzle ID (in.): 1.3 (0.233)
 Console S/N: 1648

Pre-Test Leak Check: -
 Vacuum Pressure: -12
 Post-Test Leak Check:
 Vacuum Pressure:

K: 1.68

Traverse Point	Time (min)	Stack Gas Temp., Ts (F)	Velocity Head, dh (in.H2O)	Orifice dh (in.H2O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)	Pump Vacuum (in.Hg)
					530.97					
1	2.5	157	0.61	0.89	532.25	274	222	69	75	-1
	5	157	0.61	0.94	533.50	299	231	67	75	-1
2	7.5	158	0.62	0.90	534.69	218	232	65	75	-1
	10	158	0.60	0.87	535.92	303	234	62	75	-2
3	12.5	158	0.64	0.93	537.24	298	242	59	75	-2
	15	157	0.63	0.91	538.45	299	247	58	75	-2
4	17.5	157	0.60	0.87	538.62	300	257	58	75	-2
	20	157	0.62	0.92	540.89	301	260	59	75	-3
5	22.5	156	0.61	0.89	542.13	298	264	59	75	-3
	25	155	0.61	0.89	543.35	299	266	60	75	-3
6	27.5	157	0.60	0.87	544.57	298	266	62	75	-3
	30	157	0.60	0.87	545.78	299	266	62	75	-3
1	32.5	158	0.62	0.90	547.03	298	268	62	75	-3
	35	156	0.61	0.89	548.26	298	269	63	75	-3
2	37.5	159	0.58	0.85	549.48	297	269	63	75	-3
	40	154	0.61	0.87	550.68	296	268	64	75	-4
3	42.5	157	0.59	0.86	551.92	294	269	64	75	-4
	45	158	0.58	0.85	553.16	294	267	65	75	-4
4	47.5	157	0.53	0.77	554.40	294	268	65	75	-4
	50	160	0.60	0.87	555.67	295	270	65	75	-5
5	52.5	157	0.60	0.87	556.92	291	272	65	75	-5
	55	158	0.60	0.89	557.78	290	271	67	75	-5
6	57.5	160	0.62	0.90	559.04	291	270	66	80	-5
	60	159	0.64	0.93	560.29	291	269	65	75	-5

2/2

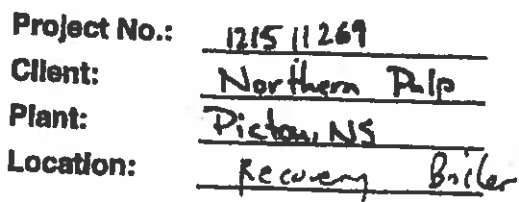
SOURCE TESTING FIELD DATA SHEET

Job No.: 121011269
 Client: Northern Pipe
 Plant: Pictou, NS
 Location: Recovery Boiler
 Test: PM-2
 Date: Aug 14, 2014
 Operators: T. H. L. P.
 Gammar: 1.040
 Delta H₂O: 6.965
 Pilot Coeff.: 0.878
 Start: 3:00
 Finish:

Static Pressure (in. H₂O): 1.10
 Port Length (in): 4"
 Stack Dia. (in.): 13.3
 Probe Length (ft): 2.0
 Nozzle ID (in.): 1-9 (0.235)
 Console S/N: 18416
 Pre-Test Leak Check: _____
 Vacuum Pressure: _____
 Post-Test Leak Check: _____
 Vacuum Pressure: _____
 K: 1.68

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dP (in. H ₂ O)	Orifice dH (in. H ₂ O)	Gas Meter Volume (cu. ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in. Hg)
									In	Out	
1	2.5	157	0.67	0.97	561.59	283	271	57	76	74	-6
1	5	159	0.64	0.93	561.33	286	271	57	76	74	-6
2	7.5	159	0.68	0.99	564.13	282	269	57	76	75	-6
2	10	159	0.70	1.07	565.44	281	269	57	77	75	-6
3	12.5	160	0.63	0.99	566.73	286	267	57	77	75	-6
3	15	160	0.67	0.97	567.96	284	266	57	77	76	-6
4	17.5	165	0.65	0.97	569.25	287	264	58	78	75	-6
4	20	159	0.60	0.87	570.40	277	263	58	78	76	-6
5	22.5	158	0.60	0.87	571.60	273	263	58	78	76	-6
5	25	156	0.63	0.97	572.53	274	263	58	78	76	-6
6	27.5	158	0.61	0.91	573.12	280	261	59	79	76	-6
6	30	159	0.61	0.89	575.36	281	261	59	79	76	-6
1	32.5	158	0.61	0.89	576.59	283	260	60	78	76	-6
1	35	159	0.61	0.89	577.84	285	260	60	78	76	-6
2	37.5	158	0.67	0.91	579.10	286	259	60	78	76	-6
2	40	158	0.62	0.91	580.35	287	260	60	78	76	-6
3	42.5	159	0.63	0.97	581.64	284	259	60	77	76	-6
3	45	160	0.61	0.89	582.89	284	257	62	77	76	-6
4	47.5	157	0.64	0.94	584.13	287	257	62	77	76	-6
4	50	157	0.65	0.92	585.40	282	256	62	77	76	-6
5	52.5	158	0.60	0.88	586.73	282	256	65	78	76	-6
5	55	157	0.60	0.88	587.96	280	256	64	78	76	-6
6	57.5	156	0.63	0.92	589.18	280	256	64	78	76	-6
6	60	157	0.60	0.88	590.42	279	255	60	76	76	-6

Sampling Methodology: Environment Canada EPS 1/RM/15



Time Start: 4:30
Time Finish: 5:00

Test No.: Car # 2
Date: Aug 19, 2014

Personnel: TBH/ES

[illegible]

MOISTURE FIELD DATA SHEET

Project No.: 121811269
 Client: NORTHOLW PULP
 Plant: PILTON NS
 Location: RECOVERLY BOILER
 Test: PM-24
 Date: AUG 20/2021
 Analyst: NLM



Stantec

FILTER 10 #
0516-20

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	905.4	620.0	285.4
2	100 mL H ₂ O	993.6	696.8	296.8
3	Blank	655.9	634.7	21.2
4	200g Silica Gel	991.9	973.5	18.4
Total Weight Gain (g)				621.8
Moisture Volume (mL)				

Volume H₂O Collected: 621.8 ml
 X 0.048 = 29.85 ft³ H₂O (Vwc)

DGM Final 714.08 ft³
 DGM Initial 653.81 ft³
 Final - Initial = 60.27 ft³ (Vmc)

Moisture = $\frac{Vwc}{(Vwc + Vmc)}$

Moisture = $\frac{29.85}{(29.85 + 60.27)} = \frac{29.85}{90.12}$

Moisture = 0.331 $\approx$ 33.1%

1/2

SOURCE TESTING FIELD DATA SHEET

Job No.: 121511269
 Client: MARINEWAY Pulp
 Plant: DIXON
 Location: AGRICULTURE
 Test: 01/13
 Date: 12/12/2014
 Operators: TSH / FS
 Gamma: 1.040
 Delta H₀: 1.821
 Pitot Coeff.: 0.833
 Start: 1:00
 Finish: 2:10

Static Pressure (in. H₂O): 1.15
 Port Length (in.): 6.11
 Stack Dia. (in.): 13.5
 Probe Length (ft): 2
 Nozzle ID (in.): 1-8 (0.237)
 Console SN: 1748

Pre-Test Leak Check: 0
 Vacuum Pressure: -1.8
 Post-Test Leak Check:
 Vacuum Pressure:

K': 1.064

Traverse Point	Time (min)	Stack Gas Temp., T _g (F)	Velocity Head, dp (in. H ₂ O)	Orifice dH (in. H ₂ O)	Gas Meter Volume (cu. ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in. Hg)
									In	Out	
1	0	159	0.65	0.95	653.81	225	225	60	84	84	-1
2	2.5	160	0.64	0.92	655.07	232	234	58	85	84	-1
3	7.5	159	0.65	0.94	657.57	268	244	48	85	84	-2
4	10	158	0.66	0.95	658.84	286	254	47	86	85	-2
5	12.5	154	0.64	0.88	660.06	299	258	44	87	85	-2
6	15	159	0.65	0.94	661.35	291	261	44	88	85	-2
7	17.5	160	0.63	0.91	662.59	292	262	43	89	86	-2
8	20	159	0.61	0.89	663.81	291	270	43	91	86	-2
9	22.5	159	0.61	0.89	665.04	287	275	43	90	86	-2
10	25	158	0.60	0.87	666.26	289	280	44	90	87	-3
11	27.5	158	0.64	0.92	667.55	285	280	45	91	87	-3
12	30	157	0.62	0.90	668.74	285	284	46	91	87	-3
13	32.5	157	0.64	0.93	669.99	289	284	46	91	87	-4
14	35	158	0.65	0.95	671.19	291	286	47	91	87	-4
15	37.5	157	0.62	0.90	672.41	288	288	47	92	88	-4
16	40	158	0.62	0.90	673.70	279	288	47	92	88	-5
17	42.5	157	0.62	0.90	674.94	280	289	48	92	88	-5
18	45	158	0.63	0.92	676.17	286	290	49	93	90	-5
19	47.5	158	0.65	0.95	677.44	289	290	48	93	90	-5
20	50	157	0.65	0.95	678.72	293	290	48	93	90	-5
21	52.5	158	0.67	0.91	679.95	294	291	48	94	89	-5
22	55	155	0.67	0.91	681.18	290	292	48	95	90	-5
23	57.5	159	0.64	0.84	682.44	289	294	48	95	90	-5
24	60	158	0.64	0.84	683.69	285	296	49	95	90	-7

7/2

SOURCE TESTING FIELD DATA SHEET

Job No.: 121811269
 Client: A&H L&W Pump
 Plant: Pileon N5
 Location: Arcadia 801561
 Test: P&N-18
 Date: Aug 29/2014
 Operators: J&H / J&S
 Gamma: 0.1040
 Delta H0: 1.505
 Pitot Coeff.: 0.838
 Start: 2:10
 Finish: 8:20

Static Pressure (In. H2O): 1.10
 Port Length (In.): 6
 Stack Dia. (In.): 13 1/2
 Probe Length (ft): 2
 Nozzle ID (In.): 1-3/16 (0.231)
 Console S/N: 18244

Pre-Test Leak Check: 0
 Vacuum Pressure: 0
 Post-Test Leak Check: 0
 Vacuum Pressure: -14
 K: 1.64

Transverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dP (In. H2O)	Orifice dH (In. H2O)	Gas Meter Volume (cu. ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (In. Hg)
									In	Out	
1	2.5	154	0.67	0.92	685.00	280	295	49	96	91	-7
1	5	154	0.65	0.95	686.21	280	295	50	95	91	-7
2	7.5	158	0.64	0.94	687.50	282	295	50	95	91	-7
3	10	158	0.61	0.89	688.70	283	295	50	95	91	-8
3	12.5	160	0.64	0.93	689.95	278	294	52	95	91	-8
4	15	160	0.64	0.93	691.71	280	293	53	94	91	-8
4	17.5	158	0.65	0.95	692.55	281	294	53	94	91	-8
5	20	159	0.63	0.93	693.35	279	293	53	95	92	-8
5	22.5	159	0.65	0.95	695.01	281	294	54	95	91	-8
6	25	160	0.63	0.93	696.77	284	292	54	95	92	-9
6	27.5	158	0.64	0.94	697.54	286	294	54	97	97	-9
7	30	158	0.64	0.94	698.80	286	294	54	97	92	-9
1	32.5	160	0.64	0.93	700.06	284	294	55	97	93	-9
2	35	158	0.65	0.95	701.34	288	293	56	97	93	-10
2	37.5	158	0.65	0.95	702.63	286	292	57	96	93	-10
3	40	159	0.61	0.89	703.85	284	290	58	97	93	-10
3	42.5	157	0.64	0.94	705.16	275	292	58	99	94	-10
4	45	157	0.64	0.94	706.41	279	292	60	98	94	-10
4	47.5	158	0.64	0.94	707.68	281	292	61	98	94	-10
5	50	158	0.64	0.94	708.96	279	292	62	98	94	-10
5	52.5	157	0.64	0.94	710.24	279	292	62	98	94	-10
6	55	157	0.64	0.94	711.53	277	291	60	98	95	-11
6	57.5	158	0.65	0.95	712.80	276	291	58	98	95	-11
6	60	158	0.64	0.94	714.08	277	291	61	98	95	-12

Sampling Methodology: Environment Canada EPS 1/RM/15

Fuel Type: _____

Time Start: ~~8:00~~ 1:10 PM
Time Finish: ~~8:30~~ 1:40 PM

Test No.: Gas # 3
Date: Aug 20, 2014

Personnel: TBH

[illegible]

MOISTURE FIELD DATA SHEET

Project No.: 121511269

Client: Northern Pulp

Plant: Pictou, NS

Location: DISSOLVING TANK

Test: PM-1

Date: Aug 20/2014

Analyst: NLM



0516-19

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	Blank 100 mL H ₂ O	665.4 1049.6	615.3 720.0	50.10 329.6
2	100 mL H ₂ O	1022.6	699.2	323.4
3	Blank	719.1	621.4	97.7
4	200g Silica Gel	1015.1	1007.0	8.1
Total Weight Gain (g)				808.9
Moisture Volume (mL)				5.1

Volume H₂O Collected: 8.08, 9 ml
 $\times 0.048 = \underline{38.9}$ L ft³ H₂O (Vwc)

DGM Final 349.34 ft³
 DGM Initial 312.24 ft³
 Final - Initial = 37.1 ft³ (Vmc)

Moisture = $\frac{Vwc}{(Vwc + Vmc)}$

Moisture = .52

Moisture = 42% 52%

Job No.:	12511269
Client:	Northern Pulp
Plant:	Disolving
Location:	Pictou, NS
Test:	PM-1
Date:	Aug 29, 2004
Operator:	CM/FS
Gemma:	1.002
Delta H ₂ O:	1.724
Pitot Coeff.:	0.834
Start:	2:50
Finish:	4:30

Port Length (in):	6"
Stack Dia. (in.):	42"
Probe Length (ft):	5'
Nozzle ID (in.):	2-10 (0.39)
Console S/N:	VES MS-06

Pre-Test Leak Check: 15
 Vacuum Pressure: _____
 Post-Test Leak Check: _____
 Vacuum Pressure: _____

K: 256

[illegible]

2/2

SOURCE TESTING FIELD DATA SHEET

Job No.: 171511269
 Client: Northern Pump
 Plant: Dyeing Tank
 Location: Pichon, NJ
 Test: PM-1
 Date: Aug 20, 2014
 Operators: CM7 MA
 Gamma: 1.002
 Delta H₀: 1.724
 Pilot Coeff.: 0.556
 Start: 4:15:00
 Finish: 4:30

Static Pressure (in.H₂O): 0.20
 Port Length (in): 6"
 Stack Dia. (in.): 4"
 Probe Length (ft): 2
 Nozzle ID (in.): 2-10/32
 Console S/N: VES M3-002

Pre-Test Leak Check: -1.5
 Vacuum Pressure:
 Post-Test Leak Check:
 Vacuum Pressure:

K: 2.56

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dp (in.H ₂ O)	Orifice dH (in.H ₂ O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in.Hg)
									In	Out	
1	2.5	214	.13	.27	331.95	230	240	66	101	100	
2	5	198	.14	.31	332.75	230	239	67	102	100	
3	7.5	200	.18	.39	333.63	230	239	67	102	100	-3
4	10	196	.16	.35	334.48	230	241	67	102	100	
5	12.5	198	.18	.39	335.30	230	241	67	103	100	
6	15	201	.17	.37	336.17	230	239	68	103	100	
7	17.5	205	.17	.37	337.12	230	240	68	103	100	-5
8	20	205	.17	.37	338.10	230	240	67	103	100	
9	22.5	204	.17	.37	339.03	230	240	67	104	100	-5
10	25	206	.17	.37	339.99	230	240	67	104	101	
11	27.5	201	.08	.17	340.70	230	238	66	104	101	
12	30	198	.16	.35	341.81	230	240	66	104	101	
13	32.5	196	.14	.31	342.46	230	239	66	104	101	
14	35	198	.14	.42	343.44	230	239	67	104	101	
15	37.5	209	.19	.41	344.44	230	240	67	104	101	
16	40	204	.19	.41	345.42	230	240	67	104	101	-6
17	42.5	209	.18	.39	346.44	230	240	67	104	101	
18	45	212	.18	.39	347.41	230	240	67	105	101	
19	47.5	213	.18	.38	348.38	230	240	67	104	101	-7
20	50	215	.18	.38	349.34	230	240	67	104	101	

Sampling Methodology: Environment Canada EPS 1/RM/15

[illegible]

MOISTURE FIELD DATA SHEET

Project No.: 121511269
 Client: Northern Pulp
 Plant: Pictou, NS
 Location: Dissolving Tank
 Test: PM-2
 Date: Aug 20, 2011
 Analyst: H.A.C.H.



Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	<u>Blank</u> 100 mL H ₂ O	<u>681.2</u> <u>1050.2</u>	<u>614.4</u> <u>721.7</u>	<u>70.0</u> <u>328.5</u>
2	100 mL H ₂ O	<u>1033.4</u>	<u>717.3</u>	<u>316.1</u>
3	Blank	<u>701.8</u>	<u>622.6</u>	<u>79.2</u>
4	200g Silica Gel	<u>1022.7</u>	<u>1015.0</u>	<u>7.7</u>
Total Weight Gain (g)				<u>801.3</u>
Moisture Volume (mL)				<u>801.3</u>

Volume H₂O Collected: 801.3 ml
 $\times 0.048 =$ 38.5 ft³ H₂O (Vwc)

DGM Final 388.76 ft³
 DGM Initial 349.53 ft³
 Final - Initial = 39.23 ft³ (Vmc)

Moisture = $\frac{Vwc}{(Vwc + Vmc)}$

Moisture = $\frac{38.5}{38.5 + 39.23}$

Moisture = 50%

Job No.: 121511269
 Client: Northern Pipe
 Plant: Pictou N.S.
 Location: Pictou N.S.
 Test: 1A-2
 Dates: Aug 21, 2014
 Operators: G.A.A.
 Gamma: 1.002
 Delta H₀: 1.224
 Pilot Coeff.: 0.336
 Start: 8:20
 Finish: 10:20

SOURCE TESTING FIELD DATA SHEET

Static Pressure (in.H₂O): -0.20
 Port Length (in): 6"
 Stack Dia. (in.): 4.31"
 Probe Length (ft): 5'
 Nozzle ID (in.): (2-10)/0.3115
 Console SN: VES 445-002

Pre-Test Leak Check: -15
 Vacuum Pressure:
 Post-Test Leak Check:
 Vacuum Pressure:

K: 3.26

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dP (in.H ₂ O)	Orifice dH (in.H ₂ O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)	Pump Vacuum (in.Hg)
1	2.5	184	.16	.45	349.53	204	198	68	90	-1
2	5	187	.16	.45	350.54	224	206	68	91	
3	7.5	184	.19	.52	351.66	233	218	68	91	
4	10	194	.17	.52	352.54	231	229	67	92	
5	12.5	194	.18	.47	353.89	230	236	67	93	
6	15	203	.18	.44	354.92	230	239	67	94	
7	17.5	211	.21	.48	355.48	230	242	67	94	
8	20	214	.19	.56	357.00	230	242	67	95	
9	22.5	215	.18	.51	358.00	230	241	68	95	
10	25	215	.16	.48	359.17	230	241	67	96	-2
11	27.5	207	.18	.43	360.12	230	241	67	96	
12	30	213	.18	.48	361.10	230	242	68	97	
13	32.5	203	.15	.48	362.17	230	240	68	97	
14	35	193	.15	.41	363.14	230	242	68	97	
15	37.5	196	.13	.42	363.89	230	242	68	98	
16	40	201	.10	.40	364.58	230	241	68	98	-3
17	42.5	211	.18	.44	365.25	230	240	67	98	
18	45	211	.19	.44	366.03	230	240	67	98	
19	47.5	205	.18	.44	367.13	230	238	68	98	
20	50	210	.18	.44	368.18	230	240	68	98	
					369.23	230	240	68	99	-4

2/2

SOURCE TESTING FIELD DATA SHEET

Job No.: 121511269
 Client: Northern Cal
 Plant: Pl. Pictou 119
 Location: Durbin, Va. Test K
 Test: PM-2
 Date: Aug 20, 2014
 Operators: C. M. M. M.
 Gamma: 1.002
 Delta H₀: 1.724
 Plot Coeff.: 0.836
 Start: 9:20
 Finish: 10:14

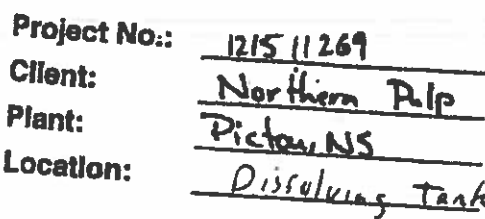
Static Pressure (in. H₂O): -0.20
 Port Length (in.): 64
 Stack Dia. (in.): 42"
 Probe Length (ft): 5'
 Nozzle ID (in.): 2-10 (0.241)
 Console S/N: WFS MS-002

Pre-Test Leak Check: -15
 Vacuum Pressure:
 Post-Test Leak Check:
 Vacuum Pressure:

K: 3.26

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dp (in. H ₂ O)	Orifice dH (in. H ₂ O)	Gas Meter Volume (cu. ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)	Pump Vacuum (in. Hg)
1	2.5	197	.14	.39	370.18	230	241	68	98	
2	5	203	.15	.41	371.10	230	240	68	98	
3	7.5	198	.16	.28	371.80	230	240	68	98	
4	10	199	.18	.50	372.83	230	240	68	99	-4
5	12.5	200	.14	.52	372.89	230	240	68	99	
6	15	213	.20	.54	374.99	230	240	68	100	
7	17.5	199	.19	.50	376.07	230	238	68	100	-5
8	20	203	.18	.49	377.13	230	241	67	101	
9	22.5	206	.17	.47	378.17	230	239	68	101	
10	24	209	.17	.44	379.21	230	238	68	102	
11	26.5	203	.17	.43	380.25	230	240	68	102	-6
12	30	200	.14	.37	381.19	230	239	67	102	
13	32.5	205	.15	.41	382.13	230	240	67	102	
14	35	196	.16	.43	383.16	230	239	68	102	
15	37.5	190	.12	.34	383.90	230	240	68	102	-6
16	40	205	.18	.49	384.56	230	240	68	102	
17	42.5	208	.16	.44	385.66	230	240	68	102	-7
18	45	204	.17	.47	386.77	230	240	67	102	
19	47.5	199	.16	.47	387.79	230	242	67	102	
20	50	197	.14	.39	388.76	230	241	67	103	-6

Sampling Methodology: Environment Canada EPS 1/RM/15



Time Start: 8:30
Time Finish: 9:00

Test No.: Gas # 2
Date: Aug 21st

Personnel: _____

[illegible]

MOISTURE FIELD DATA SHEET

Project No.: 121511269

Client: Northern Pulp

Plant: Pictou, NS

Location: Dissolving Tank

Test: PH-3

Date: Aug 22, 2014

Analyst: C.M. H.M.



Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	973.0	614.8	358.2
		1019.2	737.4	281.8
2	100 mL H ₂ O	963.4	718.9	244.5
3	Blank	676.0	622.9	53.1
4	200g Silica Gel	997.6	991.6	6
Total Weight Gain (g)				943.6
Moisture Volume (mL)				943.6

Volume H₂O Collected: 943.6 ml
 X 0.048 = 45.2928 ft³ H₂O (Vwc)

DGM Final 424.56 ft³
 DGM Initial 388.93 ft³
 Final - Initial = 36.63 ft³ (Vmc)

Moisture = $\frac{Vwc}{(Vwc + Vmc)}$

Moisture = .5597

Moisture = 56%

80.9228

SOURCE TESTING FIELD DATA SHEET

Job No.: 121511265
 Client: Northern Pipe
 Plant: Pittsford, N.Y.
 Location: Disinfection Tank
 Test: DPM-3
 Date: 4/19/83 20:20
 Operator: C.H. H.A.
 Gamma: 1.002
 Delta H₀: 1.324
 Pilot Coeff.: 0.836
 Start: 8:10
 Finish:

Static Pressure (in.H₂O): -0.20
 Port Length (in.): 14
 Stack Dia. (in.): 4.5
 Probe Length (ft): 3
 Nozzle ID (in.): 2-10 (0.311)
 Console S/N: VES MS-902

Pre-Test Leak Check: -10
 Vacuum Pressure:
 Post-Test Leak Check:
 Vacuum Pressure:

K: 2.56

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dP (in.H ₂ O)	Orifice dH (in.H ₂ O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F) In Out	Pump Vacuum (in.Hg)
1	8.5	193	.13	.28	328.93	300	239	67	93	
2	5	192	.12	.26	389.80	316	241	67	93	
3	7.5	185	.13	.29	390.45	322	241	67	94	
4	10	191	.16	.35	391.46	330	241	66	94	-1
5	12.5	197	.19	.41	392.16	330	240	66	95	
6	15	206	.20	.52	392.90	330	240	65	95	
7	17.5	194	.20	.52	393.87	330	239	65	96	
8	20	192	.17	.37	394.85	330	240	65	96	
9	22.5	198	.18	.34	395.77	330	240	63	97	
10	25	193	.18	.35	396.73	330	241	63	97	
11	27.5	203	.16	.34	397.67	330	240	62	98	-2
12	30	209	.19	.38	398.50	330	237	63	98	
13	32.5	213	.17	.36	399.51	330	238	63	98	
14	35	209	.18	.38	400.39	330	243	64	99	
15	37.5	203	.08	.17	401.32	330	237	63	99	
16	40	199	.19	.41	402.25	330	242	64	99	
17	42.5	209	.19	.41	403.91	330	242	66	97	
18	45	196	.12	.54	404.71	330	241	65	100	
19	47.5	196	.18	.39	405.90	330	238	66	100	-3
20	50	203	.18	.39	406.83	330	240	66	100	

SOURCE TESTING FIELD DATA SHEET

Job No.: 121511269

Client: Northrup Corp.

Plant: St. Louis, Mo.

Location: Disposal Tank

Test: PM-3

Date: Aug 22

Operator: CH-42

Gammeter: 1.002

Delta H₀: 1.704

Pilot Coeff.: 0.836

Start: _____

Finish: _____

Static Pressure (in. H₂O): -1.20

Port Length (in.): 6

Stack Dia. (in.): 4.8

Probe Length (ft): 5'

Nozzle ID (in.): 2.710 (0.31)

Console S/N: _____

Pre-Test Leak Check:

Vacuum Pressure:

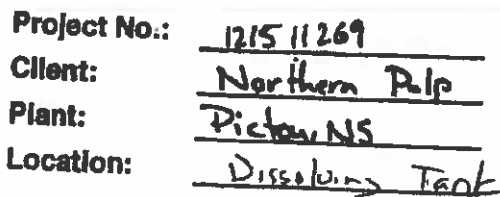
Post-Test Leak Check:

Vacuum Pressure:

K: 2.56

Traverse Point	Time (min)	Stack Gas Temp, T _s (F)	Velocity Head, dP (in. H ₂ O)	Orifice dH (in. H ₂ O)	Gas Meter Volume (cu. ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in. Hg)
									In	Out	
1	2.5	205	.15	.38	407.66	230	240	67	98	97	
	5	201	.13	.38	409.42	230	239	67	100	97	
2	7.5	204	.14	.30	409.16	230	238	66	100	97	
	10	216	.13	.38	410.04	230	241	67	101	97	-3
3	12.5	198	.15	.33	410.86	230	243	66	101	98	
	15	195	.16	.33	411.64	230	238	66	101	98	
4	17.5	201	.18	.34	412.41	230	242	65	101	98	
	20	213	.20	.43	413.30	230	244	66	101	98	
5	22.5	211	.19	.41	414.26	230	241	66	101	98	-4
	25	211	.19	.41	415.24	230	238	66	101	98	
6	27.5	209	.19	.41	416.22	230	241	67	102	98	
	30	218	.19	.41	417.18	230	238	67	102	99	
7	32.5	202	.19	.41	418.14	230	238	67	102	99	-4
	35	200	.17	.37	419.01	230	243	67	102	99	
8	37.5	218	.18	.38	419.92	230	238	67	102	97	
	40	214	.18	.38	420.87	230	245	66	103	97	-5
"	42.5	218	.19	.40	421.77	230	239	66	102	97	
	45	204	.14	.30	422.73	230	243	66	102	99	
10	47.5	202	.21	.45	423.58	230	241	66	103	97	
	50	223	.23	.48	424.56	230	236	66	103	99	-6

Sampling Methodology: Environment Canada EPS 1/RM/15



Time Start: 8:30
Time Finish: 9:00

Personnel: Cam

[illegible]

MOISTURE FIELD DATA SHEET

Project No.: 121511269
 Client: Northern Pipe
 Plant: Pictou, NS
 Location: Pipe Hauler
 Test: PM-1
 Date: Aug 19th
 Analyst: CM



FILED ID
0508-24

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	935.7	717.8	217.9
2	100 mL H ₂ O	741.1	705.1	36
3	Blank	626.0	620.7	5.3
4	200g Silica Gel	956.9	944.5	12.4
Total Weight Gain (g)				271.6
Moisture Volume (mL)				271.6

Volume H₂O Collected: 271.6 ml
 $\times 0.048 =$ 13.04 ft³ H₂O (Vwc)

DGM Final 210.47 ft³
 DGM Initial 155.93 ft³
 Final - Initial = 54.55 ft³ (Vmc)

Moisture = $\frac{Vwc}{(Vwc + Vmc)}$ 67.6

Moisture = 19.3

Moisture = 19%

Job No.: 121511269

Client: Northern Air

Plant: Power Boiler

Location: Victoria

Test: 15M 11

Date: Aug 19 2004

Operators: M.H./PS

Gamma: 100%

Delta H₀: 1.394

Pilot Coeff.: 0.812

Start: 11:00

Finish: 1:00

SOURCE TESTING FIELD DATA SHEET

Static Pressure (in.H₂O): 0.20
 Port Length (in): 6
 Stack Dia. (in): 32
 Probe Length (ft): 8-2
 Nozzle ID (in): 1.6 (0.173)
 Console S/N: VES-AS-002

Pre-Test Leak Check: ☒
 Vacuum Pressure: -13
 Post-Test Leak Check: ☒
 Vacuum Pressure: -13

K: 0.64

Traverse Point	Time (min)	Stack Gas Temp, T _s (F)	Velocity Head, dp (in.H ₂ O)	Orifice dH (in.H ₂ O)	Gas Motor Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Motor Temp. (F)		Pump Vacuum (in.Hg)
									In	Out	
1	0	141	0.80	0.45	155.92						
2	2.5	144	.78	.44	158.97	230	243	67	70	69	-1
3	5	138	.69	.39	157.47	229	236	67	69	69	
4	10	142	.72	.40	158.93	235	239	65	69	69	
5	12.5	142	.60	.34	159.99	232	239	64	68	69	
6	15	139	.59	.35	160.77	231	240	63	68	69	
7	17.5	142	.59	.34	161.69	232	242	63	68	69	
8	20	142	.58	.34	162.57	231	245	61	69	69	
9	22.5	142	.61	.34	163.37	230	235	60	69	69	
10	25	142	.61	.34	164.37	230	234	61	69	69	
11	27.5	142	.84	.47	165.26	230	238	61	69	69	
12	30	142	.87	.49	166.28	229	237	61	69	69	
13	32.5	144	1.7	.95	167.32	230	242	61	70	69	-1
14	35	143	1.7	.96	168.74	230	243	61	70	69	
15	37.5	143	1.7	.96	170.18	229	240	62	71	69	-2
16	40	148	1.8	1.00	171.63	230	231	61	71	69	
17	42.5	142	1.8	1.02	173.10	229	224	61	71	69	
18	45	143	1.8	1.01	174.73	231	226	61	71	69	
19	47.5	142	1.8	1.01	176.27	230	230	62	72	69	-3
20	50	143	1.8	1.01	177.76	229	230	62	72	69	
21	52.5	142	1.7	.96	179.27	230	235	62	72	69	-3
22	55	140	.94	.53	180.69	230	229	62	72	69	
23	57.5	141	1.5	.85	181.81	230	232	64	73	69	-3
24	60	139	1.7	.96	183.16	230	232	64	73	69	-2
25					184.60	229	238	65	73	70	

2/2

SOURCE TESTING FIELD DATA SHEET

Job No.: 171511269
 Client: Northern Plains
 Location: Pioneer Boiler
 Test: PA-1
 Date: Aug 12 2014
 Operators: JPH/FJS
 Gamma: 1.002
 Delta H₀: 1.724
 Pilot Coeff.: 0.817
 Start: 11:00
 Finish: 1:00

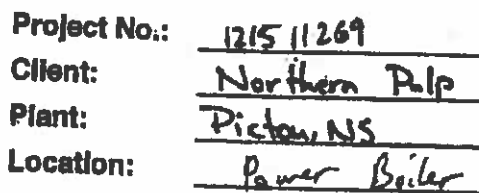
Static Pressure (in.H₂O): 0.20
 Port Length (in.): 60
 Stack Dia. (in.): 72
 Probe Length (ft): 8-2
 Nozzle ID (in.): 1.6 (0.73)
 Console S/N: VES MS-007

Pre-Test Leak Check:
 Vacuum Pressure:
 Post-Test Leak Check:
 Vacuum Pressure:

K: 0604

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, v _p (in.H ₂ O)	Orifice dH (in.H ₂ O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in.Hg)
									In	Out	
1	0				184.60						
	2.5	139	1.3	.74	185.92	232	237	67	70	70	-1
	5	137	1.3	.68	187.16	224	234	66	71	70	
2	7.5	142	1.2	.68	189.39	230	242	63	71	70	
	10	140	1.1	.62	189.46	230	241	62	72	70	
3	12.5	141	1.1	.62	190.64	230	242	60	73	70	-2
	15	143	1	.56	191.74	231	240	60	73	70	
4	17.5	143	1.2	.68	192.99	230	242	59	74	70	
	20	141	1.1	.62	193.91	230	238	58	75	71	-3
5	22.5	141	1.2	.68	195.36	231	242	59	76	71	
	25	141	1.2	.68	196.55	221	238	54	76	71	
6	27.5	143	1.2	.68	197.16	232	241	60	77	73	
	30	142	1.2	.68	198.00	230	242	61	77	73	
7	32.5	143	1.2	.68	200.33	230	240	62	77	73	-2.5
	35	142	.79	.45	201.25	230	238	62	78	73	
8	37.5	142	.60	.34	202.15	229	241	63	78	73	
	40	142	.59	.34	203.05	229	236	63	78	73	
9	42.5	143	.60	.34	203.95	229	241	65	78	74	
	45	143	.60	.34	204.83	230	237	65	79	74	
10	47.5	146	.72	.41	205.80	230	238	65	79	74	-2
	50	144	.73	.41	206.78	230	237	65	79	75	
11	52.5	147	.68	.39	207.73	230	238	65	79	75	
	55	145	.64	.36	208.65	230	238	64	80	75	-2.5
12	57.5	143	.61	.35	209.56	230	238	65	80	75	
	60	142	.68	.34	210.47	230	242	65	80	75	

Sampling Methodology: Environment Canada EPS 1/RM/15



Time Start: 11:44
Time Finish: 12:15

Test No.: Gas # 1
Date: Aug 19, 2013

Personnel: IBH/CM

[illegible]

MOISTURE FIELD DATA SHEET

Project No.: 121511269

Client: Northern Pulp

Plant: Pictou, NS

Location: Power Boiler

Test: PM-3

Date: Aug 19, 2014

Analyst: C.M



FILED 210 /
0128-15

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	965.3	739.7	225.6
2	100 mL H ₂ O	735.6	711.5	24.1
3	Blank	625.2	621.7	3.5
4	200g Silica Gel	966.6	956.6	10
Total Weight Gain (g)				263.2
Moisture Volume (mL)				263.2

Volume H₂O Collected: 263.2 ml
 $\times 0.048 =$ 12.67 ft³ H₂O (Vwc)

DGM Final 261.67 ft³
 DGM Initial 210.76 ft³
 Final - Initial = 50.91 ft³ (Vmc)

Moisture = $\frac{Vwc}{(Vwc + Vmc)}$

Moisture = $\frac{12.67}{12.67 + 50.91}$

Moisture = 19.87%

SOURCE TESTING FIELD DATA SHEET

Job No.: 121511269
 Client: Northern Poly
 Plant: Pictou, NS
 Location: Pictou, NS
 Test: DM-2
 Date: Aug 19, 2014
 Operators: L.O.L.
 Gamma: 1.724
 Delta H₀: 0.917
 Pilot Coeff.: 5.00
 Start: 5:00
 Finish: 5:08

Static Pressure (In.H₂O): 0.20
 Port Length (in): 1.1
 Stack Dia. (in.): 2.24
 Probe Length (ft): 9.2 (0.173)
 Nozzle ID (in.): 1.6 (0.173)
 Console S/N: UES M1-002

Pre-Test Leak Check:
 Vacuum Pressure:
 Post-Test Leak Check:
 Vacuum Pressure:

K: 0.64

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dp (In.H ₂ O)	Orifice dH (In.H ₂ O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (In.Hg)
									In	Out	
1	2.5	143	1.1	.63	210.76	231	244	75	78	79	-1
2	5	143	1	.57	213.09	230	239	73	78	78	
	7.6	143	1	.57	214.20	230	236	71	78	78	
3	15	143	.99	.63	215.29	229	239	67	77	78	
	2.5	145	.97	.55	216.41	229	239	65	77	78	
	15	144	.95	.54	217.49	230	243	62	78	78	
4	25	140	.97	.56	218.61	230	240	60	78	78	
	20	141	.97	.56	219.74	230	241	59	78	78	
5	25	142	1	.57	220.88	230	239	58	78	77	
	25	140	.97	.56	222.00	238	240	58	78	77	
6	27	137	1	.57	222.92	232	240	57	78	77	-2
	20	144	.96	.55	224.28	239	242	57	79	77	
7	22.5	142	.52	.30	225.13	230	239	57	79	77	-1.5
	25	145	.52	.30	225.80	228	239	58	79	79	
8	21.5	145	.44	.25	226.76	229	238	59	78	77	
	40	145	.44	.25	227.54	229	239	60	78	78	
9	42.5	138	.49	.28	228.33	230	243	60	78	77	-1.5
	45	141	.49	.28	229.15	230	237	61	78	77	
10	42.5	144	.54	.31	229.98	230	237	61	78	77	
	50	143	.54	.31	230.64	230	237	62	78	77	-1.5
11	52.5	145	.58	.33	231.40	230	240	62	78	77	
	55	144	.59	.34	232.15	230	242	62	78	77	
12	57.5	145	.50	.28	232.97	230	240	62	78	77	
	60	144	.50	.29	233.78	230	238	63	78	77	-2

212

SOURCE TESTING FIELD DATA SHEET

Job No.: 121511269
 Client: Northern Pipe
 Location: Piffers N.S.
 Test: Buggy Valve
 Date: Aug 19, 2014
 Operators: C.M.
 Gamma: 1.003
 Delta H₀: 1.225
 Pilot Coeff.: 0.319
 Start: 4:08 PM
 Finish: 5:06 PM

Static Pressure (in.H₂O): 0.20
 Port Length (in.): 0
 Stack Dia. (in.): 72
 Probe Length (ft):
 Nozzle ID (in.):
 Console S/N:

Pre-Test Leak Check:
 Vacuum Pressure:
 Post-Test Leak Check:
 Vacuum Pressure:

K: .64

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dP (in.H ₂ O)	Orifice dH (in.H ₂ O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)	Pump Vacuum (in.Hg)
								In	Out	
1	2.5	152	.83	.46	233.78	48	233	77	77	
	5	152	.85	.48	234.81	189	232	77	77	
2	7.5	151	.63	.36	235.88	213	237	77	77	
	10	151	.63	.36	236.80	211	235	77	77	
3	12.5	153	.53	.30	237.69	227	240	77	77	
	15	156	.56	.31	238.51	231	241	77	77	
4	17.5	147	.55	.31	239.34	230	240	77	77	
	20	147	.55	.31	240.20	231	241	77	77	
5	22.5	147	.61	.35	241.91	231	241	77	77	
	25	144	.59	.34	242.69	231	235	77	77	
6	27.5	145	.60	.34	243.65	230	245	77	77	
	30	144	.79	.45	244.69	230	238	77	77	
7	32.5	147	.80	.46	245.67	220	235	77	77	
	35	147	1.6	.91	247.03	230	238	77	77	
8	37.5	146	1.7	.97	248.49	228	226	77	77	
	40	147	1.7	.97	249.84	229	238	77	77	
9	42.5	147	1.7	.97	251.39	230	237	77	77	
	45	146	1.7	.97	252.87	230	232	77	77	
10	47.5	145	1.7	.98	254.33	230	237	77	77	
	50	145	1.7	.98	255.79	230	225	77	77	
11	52.5	147	1.7	.98	257.26	230	231	77	77	
	55	147	1.7	.98	258.81	230	242	77	77	
12	57.5	147	1.7	.98	260.17	230	240	77	77	
	60	148	1.3	.74	261.62	231	237	77	77	

MOISTURE FIELD DATA SHEET



Stantec

Project No.: 121511269
 Client: Northern Pulp
 Plant: Pictou NS
 Location: Power Boiler
 Test: D.M.3
 Date: Aug 20/2014
 Analyst: [Signature]

1 / 0128-11
 2 / 0128-10

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	923.5	724.3	199.2
2	100 mL H ₂ O	720.2	696.5	23.7
3	Blank	624.1	621.5	2.6
4	200g Silica Gel	975.8	966.5	9.3
Total Weight Gain (g)				234.8
Moisture Volume (mL)				234.8

Volume H₂O Collected: 234.8 ml
 X 0.048 = 11.2704 ft³ H₂O (Vwc)

DGM Final 311.76 ft³
 DGM Initial 262.03 ft³
 Final - Initial = 49.73 ft³ (Vmc)

Moisture = $\frac{Vwc}{(Vwc + Vmc)}$ 6'

Moisture = 0.18476

Moisture = 18%

SOURCE TESTING FIELD DATA SHEET

Job No.: 121511269
 Client: Northern Pipe
 Plant: Pittou NS
 Location: Power Boiler
 Test: PA-3
 Date: Aug 20, 2014
 Operators: CX
 Gamma: 1.207
 Delta H: 1.214
 Pilot Coeff.: 0.217
 Start: 4:10
 Finish: 11:20

Static Pressure (in.H2O):
 Port Length (in.):
 Stack Dia. (in.):
 Probe Length (in.):
 Nozzle ID (in.):
 Console S/N:

Pre-Test Leak Check:
 Vacuum Pressure:
 Post-Test Leak Check:
 Vacuum Pressure:

K': -64

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dV (in.H2O)	Orifice dH (in.H2O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in.Hg)
									In	Out	
1	2.5	144	.66	.37	262.98	233	242	64	73	83	
2	5	146	.65	.37	263.92	233	244	62	72	72	
3	7.5	148	.57	.32	264.81	229	240	61	75	72	
4	10	145	.57	.33	265.70	229	240	60	73	72	-1
5	12.5	145	.46	.26	266.51	231	241	59	73	72	
6	15	146	.46	.26	267.29	231	242	59	74	72	
7	17.5	146	.41	.23	268.04	230	236	58	74	73	
8	20	147	.42	.24	268.90	230	239	58	74	73	
9	22.5	146	.46	.26	269.62	230	245	59	75	73	
10	25	149	.49	.27	270.45	239	242	59	75	73	-1
11	27.5	146	.65	.37	271.40	229	236	59	75	73	
12	30	146	.66	.37	272.31	230	239	59	76	73	
13	32.5	143	.64	.74	273.53	230	240	59	76	73	
14	35	145	.64	.74	274.91	228	229	59	77	74	
15	37.5	144	.64	.80	276.20	229	233	58	78	74	-2
16	40	144	.65	.85	277.53	231	230	58	79	74	
17	42.5	144	.65	.85	278.87	231	229	58	79	74	
18	45	145	.65	.85	280.17	230	230	58	80	75	
19	47.5	144	.66	.91	281.56	229	231	58	80	75	-2
20	50	144	.66	.91	282.94	230	241	59	80	74	
21	52.5	146	.65	.85	284.27	230	236	59	81	75	
22	55	146	.65	.85	285.59	231	238	60	81	75	
23	57.5	145	.64	.80	286.92	230	235	60	81	76	-2
24	60	143	.63	.74	288.20	230	234	60	82	77	-2.3

2/2

SOURCE TESTING FIELD DATA SHEET

Job No.: 121811269
 Client: Northern Pulp
 Plant: Pirtou N.S.
 Location: Power Boiler
 Test: PA-3
 Date: Aug 20, 2014
 Operators: C.M.
 Gamma: 1.002
 Delta H₀: 1.224
 Pitot Coeff.: 0.817
 Start: 9:12
 Finish: 11:10

Static Pressure (in.H₂O):
 Port Length (in.):
 Stack Dia. (in.):
 Probe Length (ft):
 Nozzle ID (in.):
 Console S/N:

Pre-Test Leak Check:
 Vacuum Pressure: -17
 Post-Test Leak Check:
 Vacuum Pressure:

K': .64

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, q _p (in.H ₂ O)	Orifice dH (in.H ₂ O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in.Hg)
									In	Out	
1	2.5	146	1	.57	288.20	233	243	64	77	76	-5
2	5	146	1	.57	289.42	231	238	68	78	77	
3	7.5	145	1	.57	290.70	231	230	63	78	77	
4	10	144	.47	.56	291.79	230	232	59	80	77	
5	12.5	144	.46	.55	292.83	231	239	57	81	77	
6	15	144	.48	.56	293.95	230	241	56	81	77	-1
7	17.5	144	.48	.56	295.09	230	236	56	81	77	
8	20	145	.90	.51	296.23	230	239	55	83	78	
9	22.5	144	.89	.51	297.31	230	245	52	83	78	
10	25	144	.96	.55	298.41	219	243	56	83	78	
11	27.5	142	.99	.57	299.56	232	242	56	83	78	
12	30	142	.96	.55	300.70	232	241	56	83	78	
13	32.5	143	.67	.38	301.84	230	243	56	83	78	
14	35	144	.60	.34	302.78	230	242	56	83	79	-1.5
15	37.5	144	.46	.26	303.67	232	237	56	84	79	
16	40	144	.46	.26	304.55	229	241	57	83	79	
17	42.5	144	.46	.26	305.37	229	239	58	84	79	
18	45	145	.53	.30	306.16	230	240	59	84	79	-1.5
19	47.5	143	.47	.27	306.94	230	242	60	84	80	
20	50	143	.47	.27	307.73	231	241	60	84	80	
21	52.5	142	.47	.27	308.50	230	236	64	85	81	
22	55	141	.46	.27	309.32	231	241	61	85	81	
23	57	142	.47	.27	310.15	231	245	61	85	81	
24	60	142	.47	.27	310.95	230	241	61	86	80	
25	62.5	142	.47	.27	311.76	230	241	61	86	81	

COMBUSTION GAS ANALYSIS CONCENTRATION FIELD SHEET

Sampling Methodology: Environment Canada EPS 1/RM/15



Project No.: 121511269

Client: Northern Pulp

Plant: Pictou, NS

Location: Paper Boiler

Fuel Type: _____

Time Start: 4:00

Time Finish: 4:30

Test No.: Gas # 2

Date: Aug 19, 2014

Personnel: TBF/cm

Time	Concentrations							
	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	NO _x (ppm)	NO (ppm)	NO ₂ (ppm)	THC (%)
0	12.4	6.3	448	0	36			
5	12.4	6.1	473	0	37			
10	12.5	6.2	541	0	36			
15	12.7	6.0	666	0	37			
20	12.0	6.7	734	0	40			
25	11.7	6.8	665	0	41			
30	10.8	7.4	560	0	46			
0	14.2	5.0	857	0	25			7:00-7:30
5	13.7	5.3	1003	0	28			
10	13.7	5.6	853	0	31			
15	13.8	5.3	1432	0	30			
20	14.2	4.9	1291	0	29			
25	13.5	5.6	633	0	35			
30	13.1	5.8	484	0	35			

Gas #
3

VOLUMETRIC FLOWRATE DETERMINATION FIELD SHEET

Project No.: 121511269
Client: Northern Pulp
Location: HLRV
Personnel: C.M.

Barometric Press. (in. Hg): _____
Static Press. (in. H₂O): _____
Gas Moisture (%): _____
CO₂ (%): _____
O₂ (%): _____

Stack Diameter (in.) _____
Pitot Coefficient, C_p: _____

Date: Aug 20th
Time: 11:58 AM

Point	Test: 1	
	ΔP (in. H ₂ O)	Temp T _s (°F)
1	0.8	134
2	0.77	140
3	0.79	142
4	0.77	142
5	0.78	142
6	0.79	142
7	.81	141
8	.79	140
9	.78	139
10	.75	147
11	.75	137
12	.77	137

Date: Aug 20th
Time: 12:00

Point	Test: 2	
	ΔP (in. H ₂ O)	Temp T _s (°F)
1	.72	129
2	.76	137
3	.79	139
4	.79	141
5	.79	142
6	.80	142
7	.81	142
8	.81	141
9	.80	140
10	.79	139
11	.77	139
12	.76	138

Date: Aug 20th
Time: 12:05

Point	Test: 3	
	ΔP (in. H ₂ O)	Temp T _s (°F)
1	.8	135
2	.78	137
3	.79	140
4	.81	141
5	.8	141
6	.8	143
7	.81	144
8	.82	147
9	.8	146
10	.79	144
11	.72	142
12	.76	141

Date: Aug 20th
Time: 12:10

Point	Test: 4	
	ΔP (in. H ₂ O)	Temp T _s (°F)
1	.7	136
2	.87	138
3	.85	135
4	.8	140
5	.81	141
6	.8	141
7	.83	145
8	.82	144
9	.8	141
10	.81	142
11	.8	141
12	.79	139

VOLUMETRIC FLOWRATE DETERMINATION FIELD SHEET

Project No.: 171511269
Client: Northern Pulp
Location: HLRV
Personnel: C.A.

Barometric Press. (In. Hg): _____
Static Press. (In. H₂O): _____
Gas Moisture (%): _____
CO₂ (%): _____
O₂ (%): _____

Stack Diameter (In.) _____
Pitot Coefficient, C_p: _____

Date: Aug 20th
Time: 12:15

Point	Test: <u>5</u>	
	ΔP (In. H ₂ O)	Temp T _s (°F)
1	.78	134
2	.78	135
3	.79	136
4	.8	140
5	.8	141
6	.81	145
7	.83	145
8	.8	144
9	.81	144
10	.78	141
11	.77	140
12	.76	139

Date: Aug 20th
Time: 12:20

Point	Test: <u>6</u>	
	ΔP (In. H ₂ O)	Temp T _s (°F)
1	.8	143
2	.81	144
3	.82	145
4	.81	144
5	.8	143
6	.79	142
7	.78	141
8	.77	140
9	.77	140
10	.77	141
11	.79	142
12	.8	143

Date: Aug 20th
Time: 12:25

Point	Test: <u>7</u>	
	ΔP (In. H ₂ O)	Temp T _s (°F)
1	0.79	140
2	0.80	139
3	0.81	140
4	0.82	139
5	0.81	141
6	0.83	142
7	0.79	145
8	0.78	145
9	0.78	142
10	0.77	142
11	0.77	140
12	0.76	140

Date: Aug 20th
Time: 12:30

Point	Test: <u>8</u>	
	ΔP (In. H ₂ O)	Temp T _s (°F)
1	0.8	142
2	0.79	143
3	0.81	145
4	0.81	141
5	0.82	141
6	0.81	145
7	0.81	144
8	0.79	143
9	0.79	144
10	0.78	144
11	0.76	145
12	0.76	141

VOLUMETRIC FLOWRATE DETERMINATION FIELD SHEET

Project No.: 121511269
Client: Northern Pac
Location: HLRV
Personnel: C.M.

Barometric Press. (In. Hg): _____
Static Press. (In. H₂O): _____
Gas Moisture (%): _____
CO₂ (%): _____
O₂ (%): _____

Stack Diameter (In.) _____
Pitot Coefficient, Cp: _____

Date: Aug 20th
Time: 12:35

Point	Test:	
	ΔP (In. H ₂ O)	Temp T _s (°F)
1	0.79	141
2	0.80	142
3	0.81	144
4	0.92	145
5	0.81	145
6	0.83	144
7	0.80	141
8	0.79	144
9	0.78	142
10	0.77	143
11	0.77	142
12	0.76	140

Date: Aug 20th
Time: 12:40

Point	Test:	
	ΔP (In. H ₂ O)	Temp T _s (°F)
1	0.78	142
2	0.75	141
3	0.80	143
4	0.81	141
5	0.82	142
6	0.81	141
7	0.83	142
8	0.81	143
9	0.77	143
10	0.79	144
11	0.77	145
12	0.76	141

Date: Aug 20th
Time: 12:45

Point	Test:	
	ΔP (In. H ₂ O)	Temp T _s (°F)
1	0.79	141
2	0.80	142
3	0.81	143
4	0.81	144
5	0.82	145
6	0.83	142
7	0.82	143
8	0.81	144
9	0.79	144
10	0.79	144
11	0.77	144
12	0.76	141

Date: Aug 20th
Time: 12:50

Point	Test:	
	ΔP (In. H ₂ O)	Temp T _s (°F)
1	0.80	142
2	0.79	141
3	0.80	142
4	0.81	141
5	0.82	141
6	0.81	142
7	0.80	143
8	0.80	144
9	0.77	144
10	0.77	145
11	0.77	142
12	0.77	141

Sampling Methodology: Environment Canada EPS 1/RM/16



Startec

Fuel Type: gas

Time Start: _____

Time Finish: _____

Personnel: 10

[illegible]

Appendix E

Calculations

Raw Data for: Northern Pulp Summer Source Testing Test #1

Client: Northern Pulp
Job Number: 1218-1230

Plant: Pulp
Location: Line 14A
Test: P42
Date: 11-Aug-11
Personnel: JHT
Test Start: 8:11 AM
Test Finish: 10:30 AM

Parameters
Barometric Pressure, Pbar (in. Hg)
Stack Gas Pressure, Psg (in. Hg)
Stack Gas Temp, Tg (°F)
H2O Vapor Collected, Vw (in.)
Total Gas Collected, Vg (in.)
Sampling Time per Point, t (min)
Readings Taken Every ___ min
Regulatory Agency

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Solids (g)
1	100 mL H2O	873.7	880.2	6.5
2	100 mL H2O	774.0	782.5	7.5
3	Blank	943.5	953.8	10.3
4	200g Silica Gel	1012.0	1000.6	11.4
Total Weight Gals (g)				338.4
Moisture Volume (in.)				338.4

Stack Diameter, (in.)
Stack Area, (sq. ft.)
Probe Length, (ft.)
Nozzle Diameter, (in.)
Flow Coefficient, (Cp)
Orifice, restrict constant

Particulate Collected from Filter (mg):
Particulate Collected from Probe Wash (mg):
Particulate Collected from Impinger Wash (mg):
Total Particulate Collected (mg):

164.8
28.8
7.6
220.4

O2, (%)
CO2, (%)
H2, (%)

5.91
11.33
82.9

Transverse Point	Time (min)	Stack Gas Temp, Tg (°F)	S-type Probe delta P (in. H2O)	Orifice delta H (in. H2O)	Gas Meter Volume (cu. ft.)	Gas Meter Temp (°F)	Gas Meter Orifice (°F)	Nozzle Angle (Cylindrical Probe) (deg. from vert.)
Transverse 1	1	2.5	0.6	0.23	244.700	64	64	-30
	2	8	0.62	0.23	163.370	64	64	-30
	3	7.5	0.61	0.23	244.960	64	64	-30
	4	10	0.64	0.23	215.480	64	64	-30
	5	12.5	0.69	0.27	248.350	64	64	-30
	6	16.5	0.74	0.26	278.910	64	64	-30
	7	17.5	0.91	0.24	289.600	64	64	-30
	8	20	0.81	0.21	220.250	64	64	-30
	9	22.5	0.43	0.22	220.140	64	64	-30
	10	25	0.14	0.26	271.960	64	64	-30
	11	27.5	0.78	0.14	226.030	64	64	-30
	12	32.5	0.48	0.17	272.000	64	64	-30
Transverse 2	1	16.5	0.48	0.27	251.210	64	64	-30
	2	16.5	0.48	0.22	231.840	64	64	-30
	3	16.5	0.48	0.22	231.670	64	64	-30
	4	16.5	0.48	0.22	231.670	64	64	-30
	5	16.5	0.48	0.22	231.670	64	64	-30
	6	16.5	0.48	0.22	231.670	64	64	-30
	7	16.5	0.48	0.22	231.670	64	64	-30
	8	16.5	0.48	0.22	231.670	64	64	-30
	9	16.5	0.48	0.22	231.670	64	64	-30
	10	16.5	0.48	0.22	231.670	64	64	-30
	11	16.5	0.48	0.22	231.670	64	64	-30
	12	16.5	0.48	0.22	231.670	64	64	-30

Transverse Point	Time (min)	Stack Gas Temp, Tg (°F)	S-type Probe delta P (in. H2O)	Orifice delta H (in. H2O)	Gas Meter Volume (cu. ft.)	Gas Meter Temp (°F)	Gas Meter Orifice (°F)	Nozzle Angle (Cylindrical Probe) (deg. from vert.)
Transverse 1	1	62.5	0.62	0.11	260.250	67	67	-33
	2	65	0.62	0.11	220.440	67	67	-33
	3	67.5	0.69	0.11	221.640	67	67	-33
	4	70	0.61	0.18	262.310	67	67	-33
	5	72.5	0.59	0.27	263.810	67	67	-33
	6	75	0.59	0.27	263.810	67	67	-33
	7	77.5	0.74	0.14	261.430	67	67	-33
	8	80	0.95	0.24	267.110	67	67	-33
	9	82.5	0.66	0.21	263.220	67	67	-33
	10	85	0.46	0.11	264.330	67	67	-33
	11	87.5	0.38	0.18	261.680	67	67	-33
	12	90	0.38	0.11	261.680	67	67	-33
Transverse 2	1	62.5	0.62	0.11	260.250	67	67	-33
	2	65	0.62	0.11	220.440	67	67	-33
	3	67.5	0.69	0.11	221.640	67	67	-33
	4	70	0.61	0.18	262.310	67	67	-33
	5	72.5	0.59	0.27	263.810	67	67	-33
	6	75	0.59	0.27	263.810	67	67	-33
	7	77.5	0.74	0.14	261.430	67	67	-33
	8	80	0.95	0.24	267.110	67	67	-33
	9	82.5	0.66	0.21	263.220	67	67	-33
	10	85	0.46	0.11	264.330	67	67	-33
	11	87.5	0.38	0.18	261.680	67	67	-33
	12	90	0.38	0.11	261.680	67	67	-33

Calculations for: Northern Pop Cancer Source Testing
Test #1

Total 31

Client: Northern Pledge

Job Number: 131730

Plant Pillow

L'Espresso

Test PM 1

Date: 27-Aug-94

Unsub: Timothy
Perpetrator: TONYE,

Calculated Parameters

Blank Gas Pressure, P_0 (in. Hg)
Blank Gas Molecular Weight, Dry Basis, M_0 (g/mole)
Volume of Water Vapour Collected, V_{wc} (cu ft)
Blank Gas Molecular Weight, Wet Basis, M_0 (g/mole)

Combustion Gas Data for: Northern Pulp

Client: Northern Pulp
Job Number: 121611289

Plant: Picou
Location: Urne Kiln
Test: PM-1
Date: 22-Aug-14
Personnel: TBH/FS

Test Start: 11:00
Test Finish: 11:30

Time (min)	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	NO _x (ppm)
0	8.63	11.50	0	0	98
5	5.98	11.20	0	0	104
10	5.60	11.26	0	0	184
15	5.60	11.30	0	0	189
20	5.60	11.30	0	0	103
25	5.68	11.40	0	0	111
30	5.80	11.40	0	0	110
Average:	5.81	11.33	0	0	108

Flow Data for:
Test #2

Client: Northern Poly
Job Number: 121511358

Plant: Pabco
Location: Lines 14th
Test: PM-2
Date: 12-14-74
Personnel: TBST,1

Test Start: 9:30 AM
Test Finish: 11:30 AM

Parameters
Barometric Pressure, Pbar (in. Hg)
Stack Static Pressure, Pstatic (in. H₂O)
Ambient Temp. (°F)
H₂O Volume Collected, V₀ (mL)
Zeit & Sampling Points,
Sampling Time per Point, (min)
Readings Taken Every ____ min
Regulatory Agency

Inspirer No.	Inspirer Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	986.4	620.0	346.3
2	100 mL H ₂ O	711.3	100.7	21.8
3	Blank	628.9	634.2	1.7
4	200g Silica Gel	1017.2	1011.9	6.0
Total Weight Gain (g)				374.8
Mixture Volume (mL)				374.6
Slack Diameter, (in.)		48		
Stack Area, (sq. ft.)		12.57		
Piston Length, (in.)		96		
Stroke Diameter, (in.)		0.177		
Pist. Coefficient, (Cp)		0.817		
Cal (lit), meter collected		1.04		
Particulate Collected from Filter (mg):		183.9		
Particulate Collected from Piston Wash (mg):		20.0		
Particulate Collected from Inspirer Wash (mg):		8.7		
Total Particulates Collected (mg):		218.5		
O ₂ , (%)		5.8		
CO ₂ , (%)		74		
H ₂ , (%)		374.6		
N ₂ , (%)		21		
Ar,		1		
CH ₄ ,		2.9		
C ₂ H ₆ ,		23.3		

[illegible]

1	2.6	18.5	8.47	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.
2	5	180	8.46	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.
3	7.8	181	8.46	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.
4	10	181	8.46	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.
5	12.5	184	8.46	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.
6	15	184	8.46	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.
7	17.5	184	8.46	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.
8	35	182	8.46	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.
9	37.5	182	8.46	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.
10	40	182	8.46	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.
11	42.5	181	8.46	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.
12	45	181	8.46	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.
13	57.5	181	8.46	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.
14	80	181	8.46	8.21	716.280	68	67	66	65	64	63	62	61	60	59	58	57	56	55	54	53	52	51	50	49	48	47	46	45	44	43	42	41	40	39	38	37	36	35	34	33	32	31	30	29	28	27	26	25	24	23	22	21	20	19	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0	neg. from vert.

[illegible]

Calculations For: Hoffman Poly Norene Sauer Trading
Test #2

Client: Hoffman Poly
Job Number: 12151500
Plant: Pines
Location: Greenbush
Test: EN 2
Date: 2/2/99
Personnel: TBS/SP

Calculated Parameters

Stock Gas Pressure, P_g (psi) 20.04
Stock Gas Molecular Weight, Dry Basis, M_d (lb/lbmole) 28.87
Volume of Water Vapor, V_w (cc) 17.90
Stock Gas Molecular Content, P_g (cc/lbmole) 9.24
Stock Gas Molecular Weight, Wet Basis, M_w (lb/lbmole) 29.16

Isokinetic Checks

Within Criteria

Check average

Transverse Point	Time (min)	Stock Gas Temp, T _g (°F)	Stagnation P _g (psi)	Orifice Vel, V _o (ft/sec)	Measured Stock Gas Velocity, V _m (ft/sec)	Vertical Stock Gas Velocity, V _v (ft/sec)	Mean Press., P _m (in. Hg)	Avg. Temp., T _m (°F)	Gas Meter Volume, V _m (cc. ft)	Vel. @ End, V _e (ft/sec)	Isokinetic (°F)
Transverse 1	1	2.0	0.67	0.31	51.91	48.60	30.22	525	0.740	0.788	104.08
	2	7.5	0.66	0.31	52.21	49.08	30.22	529	0.720	0.764	104.86
	3	12.0	0.66	0.30	52.84	48.11	30.02	531	0.730	0.771	105.81
	4	15.0	0.66	0.28	51.16	48.40	30.02	530	0.710	0.752	103.80
	5	17.0	0.66	0.28	48.75	48.51	30.02	531	0.700	0.744	103.13
	6	20.0	0.66	0.27	47.75	47.75	30.02	533	0.690	0.734	102.87
	7	22.0	0.66	0.25	46.69	46.69	30.02	535	0.679	0.705	102.89
	8	25.0	0.66	0.23	44.32	44.32	30.02	535	0.650	0.680	102.33
	9	27.0	0.66	0.23	44.56	44.56	30.02	535	0.650	0.680	102.33
	10	30.0	0.66	0.21	42.27	42.27	30.02	536	0.620	0.650	101.79
	11	32.0	0.66	0.21	42.27	42.27	30.02	536	0.620	0.650	101.79
	12	35.0	0.66	0.20	41.32	41.32	30.02	537	0.610	0.640	101.35
Transverse 2	1	2.0	0.69	0.31	50.87	47.52	30.02	543	0.700	0.723	104.48
	2	7.5	0.66	0.31	51.10	48.02	30.02	544	0.770	0.794	104.89
	3	12.0	0.65	0.30	50.72	48.08	30.02	546	0.730	0.760	105.38
	4	15.0	0.66	0.28	48.78	48.02	30.02	547	0.700	0.740	102.87
	5	17.0	0.66	0.25	47.80	47.22	30.02	547	0.690	0.718	104.38
	6	20.0	0.66	0.25	46.30	46.12	30.02	547	0.680	0.708	104.35
	7	22.0	0.66	0.24	45.47	45.30	30.02	547	0.660	0.687	103.32
	8	25.0	0.66	0.24	45.43	45.30	30.02	547	0.640	0.666	102.29
	9	27.0	0.66	0.23	44.56	44.56	30.02	547	0.630	0.656	102.29
	10	30.0	0.66	0.23	43.32	43.32	30.02	548	0.610	0.633	101.31
	11	32.0	0.66	0.18	38.91	40.25	30.01	547	0.570	0.625	101.31
	12	35.0	0.66	0.18	38.91	40.25	30.01	547	0.570	0.625	101.31
Total	1	2.0	0.67	0.31	51.91	48.60	30.22	525	0.740	0.788	104.08
	2	7.5	0.66	0.31	52.21	49.08	30.22	529	0.720	0.764	104.86
	3	12.0	0.66	0.30	52.84	48.11	30.02	531	0.730	0.771	105.81
	4	15.0	0.66	0.28	51.16	48.40	30.02	530	0.710	0.752	103.80
	5	17.0	0.66	0.28	48.75	48.51	30.02	531	0.700	0.744	103.13
	6	20.0	0.66	0.27	47.75	47.75	30.02	533	0.690	0.734	102.87
	7	22.0	0.66	0.25	46.69	46.69	30.02	535	0.679	0.705	102.89
	8	25.0	0.66	0.23	44.32	44.32	30.02	535	0.650	0.680	102.33
	9	27.0	0.66	0.23	44.56	44.56	30.02	535	0.650	0.680	102.33
	10	30.0	0.66	0.21	42.27	42.27	30.02	536	0.620	0.650	101.79
	11	32.0	0.66	0.21	42.27	42.27	30.02	536	0.620	0.650	101.79
	12	35.0	0.66	0.20	41.32	41.32	30.02	537	0.610	0.640	101.35

Combustion Gas Data for: Northern Pulp

Client: Northern Pulp
Job Number: 121511289

Plant: Pictou
Location: Lime Kiln
Test: PM-2
Date: 22-Aug-14
Personnel: TBH/FS

Test Start: 9:00
Test Finish: 9:30

Time (min)	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
0	5.90	8.40	0	0.0	112
5	5.90	8.60	0	0.0	111
10	5.90	8.40	0	0.0	111
15	5.90	8.40	0	0.0	110
20	5.90	8.40	0	0.0	109
25	5.90	8.40	0	0.0	112
30	5.90	8.40	0	0.0	110
Average:	5.8	8.3	0.0	0.0	111

Test 2

Client: Northern Pipe
Job Number: 12111289

PMA# 71204
 Location: Lewis Rd
 Test: PM-J
 Date: 11-Aug-11
 Personnel: JERTY
 Test Start: 11:30 AM
 Test Finish: 1:14 PM

Parameters
Barometric Pressure, Pbar (in. Hg)
Stack Static Pressure, Pstatic (in. H₂O)
Ambient Temp. (°F)
H₂O Volume Collected, Vw (ml.)
Total # Sampling Paths,
Sampling Time per Path, (min)
Readings Taken Every — min
Regulatory Agency

Sample No.	Impinger Contents	Flask Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	162.9	714.5	309.4
2	100 mL H ₂ O	781.3	724.3	17.8
3	Blank	698.9	362.1	1.8
4	200g silica Gel	362.9	644.5	0.5
			Total Weight Gain (g)	337.3
			Moisture Volume (mL)	337.3

Particulate Collected from Filter (mg):
 Particulate Collected from Probe Wash (mg):
 Particulate Collected from Impinger Wash (mg):
 Total Particulate Collected (mg):

Parameter	Value
CO ₂ (%)	8.40
CH ₄ (%)	5.71
N ₂ (%)	86.9

Transverse Plane	Thin (in.)	Stock Gas Temp, T _g (°F)	B-type Pilot diam P (in. 1000)	Orifice diam H (in. 1000)	Gas Meter Volume (cc. ft.)	Gas Meter Temp Inlet (°F)	Gas Meter Temp Outlet (°F)	Nozzle Angle (Cyclic Flow) (deg. from vert.)
1	2.5	141	0.64	0.20	79.540	71	71	14
2	5	153	0.61	0.20	77.264	71	70	14
3	7.5	153	0.64	0.20	77.790	71	71	14
4	10	145	0.59	0.20	77.460	71	71	14
5	12.5	141	0.58	0.20	77.160	71	71	14
6	16	144	0.57	0.20	77.160	71	71	14
7	17.5	141	0.55	0.20	77.160	71	71	14
8	20	144	0.55	0.20	77.160	71	71	14
9	22.5	144	0.55	0.20	77.160	71	71	14
10	25	144	0.55	0.20	77.160	71	71	14
11	27.5	144	0.55	0.20	77.160	71	71	14
12	30	144	0.55	0.20	77.160	71	71	14
13	32.5	144	0.55	0.20	77.160	71	71	14
14	35	144	0.55	0.20	77.160	71	71	14
15	37.5	144	0.55	0.20	77.160	71	71	14
16	40	144	0.55	0.20	77.160	71	71	14
17	42.5	144	0.55	0.20	77.160	71	71	14
18	45	144	0.55	0.20	77.160	71	71	14
19	47.5	144	0.55	0.20	77.160	71	71	14
20	50	144	0.55	0.20	77.160	71	71	14
21	52.5	144	0.55	0.20	77.160	71	71	14
22	55	144	0.55	0.20	77.160	71	71	14
23	57.5	144	0.55	0.20	77.160	71	71	14
24	60	144	0.55	0.20	77.160	71	71	14
25	62.5	144	0.55	0.20	77.160	71	71	14
26	65	144	0.55	0.20	77.160	71	71	14
27	67.5	144	0.55	0.20	77.160	71	71	14
28	70	144	0.55	0.20	77.160	71	71	14

1	82.5	162	0.65	0.10	765 000	71	11
2	85	163	0.71	0.10	790 430	72	12
3	87.5	162	0.65	0.08	791 110	73	13
4	70	151	0.99	0.27	771 610	74	14
5	72.5	161	0.97	0.26	792 150	75	15
6	75	167	0.75	0.24	793 100	76	16
7	77.5	161	0.90	0.23	795 700	77	17
8	80	164	0.94	0.21	794 400	78	18
9	82.5	164	0.88	0.21	799 050	79	19
10	85	164	0.81	0.20	797 610	80	20
11	87.5	162	0.60	0.18	796 100	81	21
12	90	167	0.38	0.17	798 700	82	22
13	92.5	167	0.33	0.17	797 200	83	23
14	95	169	0.10	0.16	797 610	84	24
15	97.5	168	0.07	0.17	798 100	85	25
16	100	167	0.07	0.21	799 050	86	26
17	102.5	163	0.15	0.21	799 600	87	27
18	105	161	0.34	0.20	800 200	88	28
19	107.5	163	0.42	0.19	800 900	89	29
20	110	166	0.41	0.19	801 500	90	30
21	112.5	165	0.49	0.22	800 910	91	31
22	115	163	0.38	0.17	802 400	92	32
23	117.5	161	0.35	0.16	801 900	93	33
24	120	164	0.31	0.18	801 500	94	34

Теневая 2

Calculations for: stream Pulp in water balance Testing

Client: Medline Pulp
Job Number: 12151287

Plant Name:
Location: Uru Kila
Test PML3
Date: 22 Aug-11
Parameter: TMB-UPD

Calculated Parameters

Stack Gas Pressure, Pa (a.Hg)
Stack Gas Molecular Weight, Dry Basis, Md (a.Hg-mole)
Volume of Water Vapor Collected, Vwc (cc/L)
Stack Gas Molecular Content (% on dry basis)
Stack Gas Molecular Weight, Wet Basis, Mw (a.Hg-mole)

10.04
18.87
16.190
0.247
.7586

Individuality Checks

Check average

Within Criteria

Transverse Point	Time (min)	Stack Gas Temp, T _s (°F)	2-Stage Prol. coll. P (Pa (a.Hg))	Orifice Coll. H (Pa (a.Hg))	Measured Stack Gas Velocity, U _g (ft/s)	Vertical Stack Gas Velocity, U _v (ft/s)	Water Pressure, P _m (in. Hg)	Avg. Temp, T _g (°F)	Gas Meter Vol (cc. L)	Vol. @ Std. Vwc (cc. L)	Uncertainty (%)
Transverse 1	1	2.5	0.80	0.30	50.84	48.44	30.02	531	0.730	0.770	104.08
	2	5	0.80	0.30	50.32	47.80	30.02	531	0.730	0.770	104.13
	3	7.5	0.80	0.29	48.72	47.86	30.02	532	0.710	0.749	101.40
	4	10	0.58	0.27	48.32	47.26	30.02	532	0.700	0.738	105.78
	5	12.5	0.58	0.27	47.78	46.73	30.02	532	0.700	0.738	106.44
	6	15	0.57	0.28	47.45	46.73	30.02	532	0.700	0.737	107.44
	7	17.5	0.58	0.28	47.85	46.88	30.02	532	0.680	0.737	108.43
	8	20	0.56	0.28	47.07	46.32	30.02	532	0.680	0.685	108.73
	9	22.5	0.52	0.22	45.32	45.05	30.02	532	0.590	0.621	94.30
	10	25	0.47	0.21	43.05	42.16	30.02	531	0.620	0.654	104.80
	11	27.5	0.44	0.20	41.88	41.80	30.02	531	0.560	0.621	107.28
	12	30	0.44	0.22	43.05	43.05	30.02	532	0.620	0.622	103.07
Transverse 2	1	2.5	0.85	0.30	50.85	48.81	30.02	533	0.640	0.674	81.54
	2	5	0.85	0.30	50.59	48.87	30.02	533	0.640	0.674	81.54
	3	7.5	0.80	0.29	48.81	47.87	30.02	532	0.630	0.663	80.33
	4	10	0.57	0.27	48.16	47.43	30.02	532	0.670	0.708	102.05
	5	12.5	0.56	0.28	48.80	48.80	30.02	532	0.670	0.708	102.84
	6	15	0.48	0.23	43.83	43.78	30.02	532	0.620	0.654	85.84
	7	17.5	0.50	0.23	44.34	44.34	30.02	532	0.630	0.664	86.21
	8	20	0.45	0.21	42.16	42.16	30.02	532	0.630	0.670	104.21
	9	22.5	0.43	0.20	41.21	41.21	30.02	532	0.580	0.683	108.70
	10	25	0.38	0.17	38.72	38.72	30.02	532	0.580	0.610	108.71
	11	27.5	0.35	0.16	37.15	37.15	30.02	531	0.570	0.580	104.16
	12	30	0.40	0.18	38.72	38.72	30.02	531	0.490	0.514	85.43
Total	1	2.5	0.85	0.30	50.85	48.81	30.02	533	0.640	0.674	81.54
	2	5	0.85	0.30	50.59	48.87	30.02	533	0.640	0.674	81.54
	3	7.5	0.80	0.29	48.81	47.87	30.02	532	0.630	0.663	80.33
	4	10	0.57	0.27	48.16	47.43	30.02	532	0.670	0.708	102.05
	5	12.5	0.56	0.28	48.80	48.80	30.02	532	0.670	0.708	102.84
	6	15	0.48	0.23	43.83	43.78	30.02	532	0.620	0.654	85.84
	7	17.5	0.50	0.23	44.34	44.34	30.02	532	0.630	0.664	86.21
	8	20	0.45	0.21	42.16	42.16	30.02	532	0.630	0.670	104.21
	9	22.5	0.43	0.20	41.21	41.21	30.02	532	0.580	0.683	108.70
	10	25	0.38	0.17	38.72	38.72	30.02	532	0.580	0.610	108.71
	11	27.5	0.35	0.16	37.15	37.15	30.02	531	0.570	0.580	104.16
	12	30	0.40	0.18	38.72	38.72	30.02	531	0.490	0.514	85.43
Average		623	0.47	0.22	42.72	41.88	30.02	533.06	20.000	20.440	102.05

Combustion Gas Data for: Northern Pulp

Client: Northern Pulp
Job Number: 121511269

Plant: Picou
Location: Lime Kiln
Test: PM-3
Date: 4-Jul-13
Personnel: TBHFS

Test Start: 11:30
Test Finish: 12:00

All gases except NOx are obtained from the 24 hr TRS testing

Time (min)	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
0	5.70	8.40	0	0	85
5	5.70	8.40	0	0	84
10	5.80	8.40	0	0	85
15	5.70	8.48	0	0	85
20	5.10	8.40	0	0	86
25	5.70	8.40	0	0	80
30	5.70	8.40	0	0	88
Average:	5.7	8.4	0.0	0.0	85

DATA ENTRY

Northern Pulp

Lime Kiln

Stack Height from Grade: 37 m

Stack Diameter: 1.22 m

Standard Temperature, Tstd (F): 77
(K): 298
Standard Pressure, Pstd (in.Hg): 29.92
(Bar): 1.0

Parameter	Symbol	Units	Test 1	Test 2	Test 3	Average
Test ID	-	-	PM-1	PM-2	PM-3	-
Date	-	-	21-Aug-14	22-Aug-14	22-Aug-14	-
Start Time	-	-	8:15 AM	9:20 AM	11:48 AM	n/a
End Time	-	-	10:30 AM	11:30 AM	1:48 PM	n/a
Total Sampling Time	-	min	120	120	120	120
Stack Diameter	D	in.	48	48	48	48
Average Stack Gas Temperature	Ts	F	185	162	183	163
Average Dry Gas Meter Temperature	Tm	F	67	81	73	74
Barometric Pressure	Pbar	in.Hg	30.00	30.00	30.00	30.00
Stack Static Pressure	Pstatic	in.H2O	0.51	0.51	0.51	0.51
Average Pressure Drop (Head)	dP	in.H2O	0.48	0.49	0.47	0.48
Average delta H Orifice	dH	in.H2O	0.22	0.23	0.22	0.22
Average Meter Temperature	Tm	F	67	81	73	74
Gas Sample Volume	Vm	cu.ft	29.7	30.3	29.0	29.7
Average Isokinetics	I	%	104.6	105.2	102.6	104.2
Nozzle Diameter	Dn	in.	0.177	0.177	0.177	0.177
Pitot Coefficient	Cp	-	0.817	0.817	0.817	0.817
Gamma, meter constant	J	-	1.040	1.040	1.040	1.040
Reference Temperature	Tref	R	537	537	537	537
Reference Pressure	Pref	in.Hg	29.92	29.92	29.92	29.92
Stack Gas Oxygen Content	Co1	%	5.81	5.80	5.71	5.78
Stack Gas Carbon Dioxide Content	Cco2	%	11.3	8.3	8.4	9.4
Stack Gas Nitrogen Content	Ca2	%	82.9	85.9	85.9	84.9
Stack Gas Sulphur Dioxide Content	CSO2	ppm	0.0	0.0	0.0	0.0
Stack Gas Nitrogen Oxides Content	CAox	ppm	106.4	110.7	84.7	100.6
Stack Gas Carbon Monoxide Content	Cco	ppm	0.0	0.0	0.0	0.0
Volume of Water Collected	Vw	mL	338	375	337	349
Particulate Collected from Filter	-	mg	185	184	183	177
Particulate Collected from Probe Wash	-	mg	28.8	29.0	7.35	21.8
Particulate Collected from Impinger Wash	-	mg	7.03	5.73	0.87	4.54
Total Particulate Collected (excl. impingers)	Mp	mg	213	213	171	199

Legend: F - degrees Fahrenheit
K - degrees Kelvin
Bar - bars
in.Hg - inches of mercury
in. - inches

in.H2O - inches of water
cu.ft - cubic feet
R - degrees Rankin
NOx - as NO2

CALCULATIONS

Northern Pulp
Line K10

Stack Height from Grade: 37 m
Stack Diameter: 1.22 m

Variable	Symbol	Units	Calculation	Test 1	Test 2	Test 3	Average
Stack Area	A_s	sq.ft. sq.m.	$A_s = P \pi \times (D/2)^2 \times 1/4$ $A_s (\text{sq.m.}) = A_s (\text{sq.ft.}) \times 0.0929$	12.57 1.17	12.57 1.17	12.57 1.17	12.57 1.17
Barometric Pressure	P_{bar}	hPa	$P_{bar} (\text{hPa}) = P_{bar} (\text{in.Hg}) \times 2.54$	102	102	102	102
Stack Static Pressure	P_{static}	hPa	$P_{static} (\text{hPa}) = P_{static} (\text{in.Hg}) \times 2.54$	0.13	0.13	0.13	0.13
Avg. Stack Temperature	T_s	$^{\circ}\text{C}$	$T_s (^{\circ}\text{C}) = T_s (^{\circ}\text{F}) - 32$	625	622	623	623
Avg. Meter Temperature	T_m	$^{\circ}\text{C}$	$T_m (^{\circ}\text{C}) = T_m (^{\circ}\text{F}) - 32$	627	641	633	634
Nozzle Diameter	D_n	mm	$D_n (\text{mm}) = D_n (\text{in.}) \times 25.4$	4	4	4	4
Gas Meter Pressure	P_m	in.Hg	$P_m = P_{bar} + (P_{static} \times 13.6)$	30.0	30.0	30.0	30.0
Sample Volume at STP	V_{mst}	cu.ft.	$V_{mst} = T_{std} P_{std} / (P_m \times T_m \times 1/14.7)$	31.8	31.3	30.5	31.1
Volume of Water Vapour	V_{wc}	cu.ft.	$V_{wc} (\text{cu.ft.}) = 0.0132 \times V_{mst} (\text{cu.ft.})$	0.89	0.89	0.88	0.88
Water Fraction	D_{wc}	-	$D_{wc} = V_{wc} / (V_{wc} + V_{mst})$	16.1 0.34	18.0 0.36	16.2 0.35	16.8 0.35
Molecular Weight, Dry	M_d	lb/lb-mol	$M_d = 0.44 (\text{CO}_2) + 0.33 (\text{CO}) + 0.23 (\text{O}_2)$	30.0	29.8	29.8	29.7
Molecular Weight, Wet	M_w	lb/lb-mol	$M_w = M_d (1 - D_{wc}) / (1 - D_{wc})$	28.0	25.4	25.8	25.8
Stack Pressure	P_s	in.Hg	$P_s = P_{bar} + (P_{static} \times 13.6)$	30.0	30.0	30.0	30.0
Stack Gas Velocity	V_s	ft/s m/s	$V_s = 40.82 \times C_p \times (P_s / T_s) / (M_d \times 1/14.7)$ $V_s (\text{m/s}) = V_s (\text{ft/s}) \times 0.3048$	41.8 12.7	42.1 12.8	42.0 12.8	42.0 12.8
Actual Stack Gas Flow Rate	Q	acfm	$Q = V_s \times A_s$	31,533	31,718	31,858	31,836
Dry Stack Gas Flow Rate	Q_d	dscfm dscms	$Q_d = Q \times (1 - D_{wc}) \times (T_{std} / T_s) \times (P_s / P_{std})$ $Q_d (\text{dscms}) = 0.00072 \times Q_d (\text{dscfm})$	17,883 8.49	17,478 8.25	17,891 8.44	17,787 8.40
Sulphur Dioxide - SO ₂							
SO ₂ Measured Concentration	C_{m2}	ppm	Measurement from Flue Gas Analyser	0.0	0.0	0.0	ND
Uncorrected @ Ref Cond	C_{u2}	mg/lscm	$C_{u2} (\text{mg/lscm}) = C_{m2} (\text{ppm}) \times 2.63$	0	0	0	ND
SO ₂ Emission Rate	E_{R2}	g/hr	$E_{R2} = C_{u2} / 0.00072 \times Q_d$ $E_{R2} (\text{g/hr}) = 2.6 \times E_{R2} (\text{g/hr})$	0.00	0.00	0.00	ND
SO ₂ Concentration							
Corrected to 11% O ₂	C_{c2}	mg/lscm	$C_{c2} (11\% \text{ O}_2) = C_{u2} (\text{mg/lscm}) \times (20.9 - 11) / (20.9 - C_{u2})$	0	0	0	ND
Corrected to 3% O ₂	C_{c2}	mg/lscm	$C_{c2} (3\% \text{ O}_2) = C_{u2} (\text{mg/lscm}) \times (20.9 - 3) / (20.9 - C_{u2})$	0	0	0	ND
Corrected to 12% CO ₂	C_{c2}	mg/lscm	$C_{c2} (12\% \text{ CO}_2) = C_{u2} (\text{mg/lscm}) \times (12 / C_{u2})$	0	0	0	ND
Nitrogen Oxides - NO _x							
NO _x Measured Concentration	C_{m1}	ppm	Measurement from Flue Gas Analyser	108.4	110.7	84.7	100.6
Uncorrected @ Ref Cond	C_{u1}	mg/lscm	$C_{u1} (\text{mg/lscm}) = C_{m1} (\text{ppm}) \times 1.882$	200	208	159	189
NO _x Emission Rate	E_{R1}	g/hr	$E_{R1} = C_{u1} / 0.00072 \times Q_d$ $E_{R1} (\text{g/hr}) = 3.6 \times E_{R1} (\text{g/hr})$	1.70 8.12	1.72 8.19	1.36 4.85	1.59 5.72
NO _x Concentration							
Corrected to 11% O ₂	C_{c1}	mg/lscm	$C_{c1} (11\% \text{ O}_2) = C_{u1} (\text{mg/lscm}) \times (20.9 - 11) / (20.9 - C_{u1})$	131	137	104	124
Corrected to 3% O ₂	C_{c1}	mg/lscm	$C_{c1} (3\% \text{ O}_2) = C_{u1} (\text{mg/lscm}) \times (20.9 - 3) / (20.9 - C_{u1})$	238	247	188	224
Corrected to 12% CO ₂	C_{c1}	mg/lscm	$C_{c1} (12\% \text{ CO}_2) = C_{u1} (\text{mg/lscm}) \times (12 / C_{u1})$	212	300	228	247
Carbon Monoxide - CO							
CO Measured Concentration	C_{m0}	ppm	Measurement from Flue Gas Analyser	0.00	0.00	0.00	0.00
Uncorrected @ Ref Cond	C_{u0}	mg/lscm	$C_{u0} (\text{mg/lscm}) = C_{m0} (\text{ppm}) \times 1.145$	0.00	0.00	0.00	0.00
CO Emission Rate	E_{R0}	g/hr	$E_{R0} = C_{u0} / 0.00072 \times Q_d$ $E_{R0} (\text{g/hr}) = 3.6 \times E_{R0} (\text{g/hr})$	0.00	0.00	0.00	0.00
CO Concentration							
Corrected to 11% O ₂	C_{c0}	mg/lscm	$C_{c0} (11\% \text{ O}_2) = C_{u0} (\text{mg/lscm}) \times (20.9 - 11) / (20.9 - C_{u0})$	0.00	0.00	0.00	0.00
Corrected to 3% O ₂	C_{c0}	mg/lscm	$C_{c0} (3\% \text{ O}_2) = C_{u0} (\text{mg/lscm}) \times (20.9 - 3) / (20.9 - C_{u0})$	0.00	0.00	0.00	0.00
Corrected to 12% CO ₂	C_{c0}	mg/lscm	$C_{c0} (12\% \text{ CO}_2) = C_{u0} (\text{mg/lscm}) \times (12 / C_{u0})$	0.00	0.00	0.00	0.00
Particulate Concentration	C_p	mg/lscm	$C_p = M_p / V_{mst}$	239	240	198	225
Particulate Emission Rate	E_{Rp}	g/hr	$E_{Rp} = C_p / 0.00072 \times Q_d$ $E_{Rp} (\text{g/hr}) = 2.6 \times E_{Rp} (\text{g/hr})$	2.03 7.30 690	1.98 7.12 831	1.67 6.01 831	1.89 6.81 764
Plant Production		m³/day					
Particulate Concentration							
Corrected to 11% O ₂	C_{c1}	mg/lscm	$C_{c1} (11\% \text{ O}_2) = C_p \times (20.9 - 11) / (20.9 - C_{u1})$	157	157	129	148
Corrected to 3% O ₂	C_{c1}	mg/lscm	$C_{c1} (3\% \text{ O}_2) = C_p \times (20.9 - 3) / (20.9 - C_{u1})$	283	284	233	287
Corrected to 12% CO ₂	C_{c1}	mg/lscm	$C_{c1} (12\% \text{ CO}_2) = C_p \times (12 / C_{u1})$	253	345	282	293
Emission Metric		g/hr/dscm		0.25	0.21	0.17	0.21

Legend:

sq.ft. - square feet
sq.m. - square metres
PI - 1.142
R - degrees Rankin
ppm - parts per million

in. Hg - inches of mercury
cu.ft. - cubic feet
cu.m. - cubic metres
STP - standard temperature and pressure
dscfm - dry standard cubic feet per minute
dscms - dry standard cubic metres per second

OFFICIAL STACK TESTING RESULTS

Northern Pulp

Lime Kiln

Stack Height from Grade: 37 m

Stack Diameter: 1.22 m

Parameter	Test 1	Test 2	Test 3	Average	NSENV Limits
Test ID	PM-1	PM-2	PM-3	-	-
Test Date	21-Aug-14	22-Aug-14	22-Aug-14	-	-
Stack Gas Temperature (C)	74	72	73	73	-
Moisture Content (%)	33.8	36.5	34.7	35.0	-
Velocity (m/s)	12.7	12.8	12.8	12.8	-
Volumetric Flow (dscms)	8.49	8.25	8.44	8.40	-
Oxygen - O2 (%)	5.81	5.80	5.71	5.78	-
Carbon Dioxide - CO2 (%)	11.3	8.34	8.40	8.36	-
Sulphur Dioxide - SO2					-
SO2 Measured Concentration (ppm)	ND	ND	ND	ND	-
Uncorrected at Ref Cond (mg/Rcm)	ND	ND	ND	ND	-
Emission Rate (kg/hr)	ND	ND	ND	ND	-
Nitrogen Oxides - NOx					-
NOx Measured Concentration (ppm)	108	111	84.7	101	-
Uncorrected at Ref Cond (mg/Rcm)	200	208	159	189	-
Emission Rate (kg/hr)	8.12	8.19	4.85	5.72	-
Carbon Monoxide - CO					-
CO Measured Concentration (ppm)	ND	ND	ND	ND	-
Uncorrected at Ref Cond (mg/Rcm)	ND	ND	ND	ND	-
Emission Rate (kg/hr)	ND	ND	ND	ND	-
Particulate Matter - PM					-
Particulate Concentration (mg/dscm)	239	240	198	225	-
Particulate Emission Rate (kg/hr)	7.30	7.12	6.01	6.81	-
Particulate Emission Rate (kg/adubmt)	0.25	0.21	0.17	0.21	0.50

Legend: C - degrees Celsius
m/s - metres per second
dscms - dry standard cubic metres per second
ppm - parts per million
adubmt - air dried unbleached metric tonne (1,039 adubmt/d)

STP - standard temperature and pressure (25 C and 101.3 kPa)
mg/dscm - milligrams per dry standard cubic metre
NOx - as NO2
ND - non-detectable

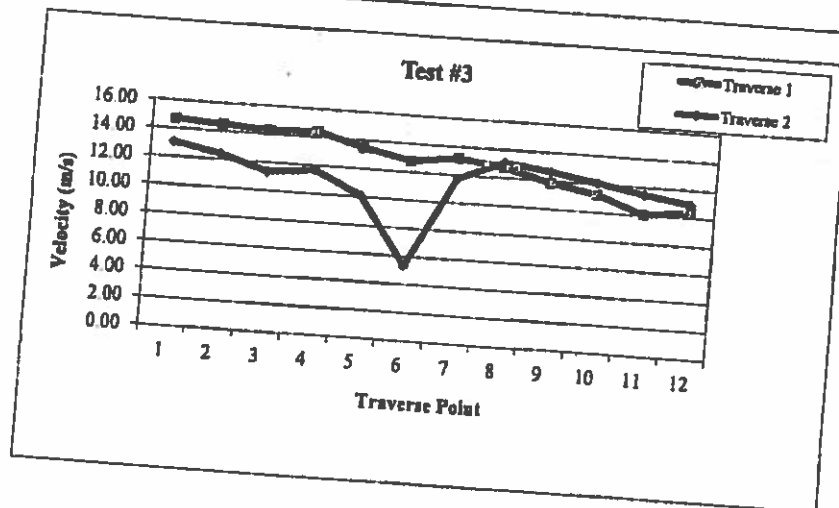
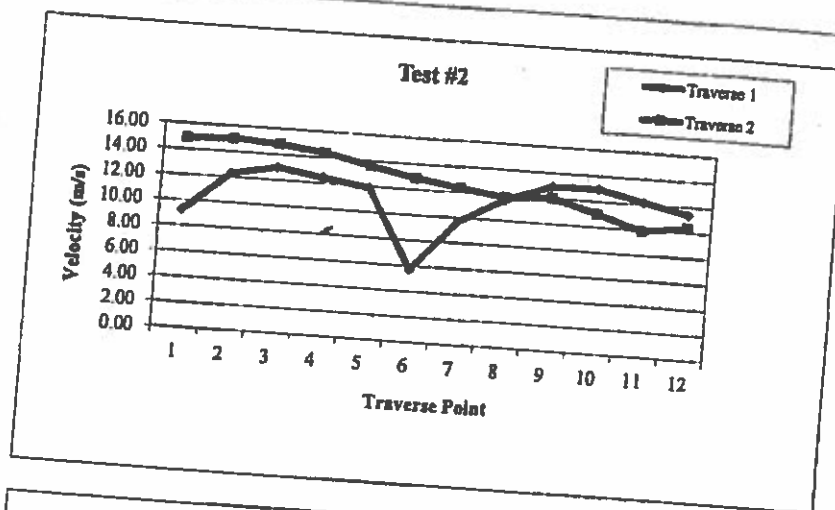
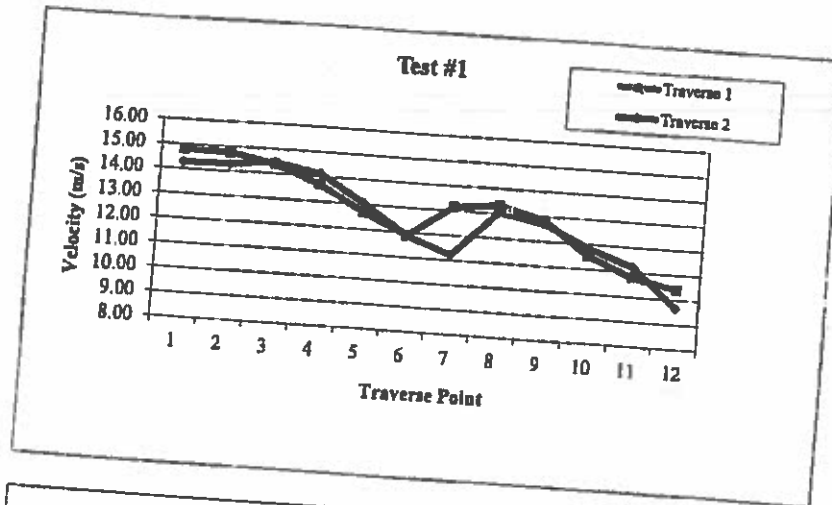
Client: Prophet's Cafe
 Facility: Albany/Troy, NY
 Location: 1000 10th
 Job Number: 17181340

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Constituents ID	Residue Pro Weights (g)				Sample ID	Residue Weights			Total Ashes (g)	Total Protein (g)	Residue Pro Weights (g)	Unresidue Proteins Weight (g)	Constituent Proteins Weight (g)
	Aspartic		Glu			Ser	Threonine	Alanine					
	Protein 1	Protein 2	Protein 1	Protein 2									
T2	113.1725	173.1725	113.1725	113.1725	P4-1	43.1	37.0	65.1	24.4	112.2570	112.2570	112.2570	0.0265
E1	110.0718	110.0718	110.0718	110.0718	P4-2	60.0	30.7	105.9	36.0	115.1025	115.1025	115.1025	0.0260
L4	120.0870	120.0870	120.0870	120.0870	P4-3	435.0	378.9	38.2	38.0	109.0545	109.0545	109.0545	0.0274
V1	100.1349	100.1349	100.1349	100.1349	AB	477	376.7	121.9	121.9	109.1343	109.1343	109.1343	-0.0023

Factor #3	Pre-Variables (1)			Sample ID	Post-Variables (2)			Pre-Variables (3) Initial Inner Filter (4)	Post-Variables (4) Initial Inner Filter (5)
	A-Filtered by Date				A-Filtered by Date				
	Time 1	Time 2	Time 3		Time 1	Time 2	Time 3		
09-05-6	0.3325	0.3323	0.3324	PA-1	0.5172	0.5172	0.5172	0.1144	
09-16-2	0.2315	0.2317	0.2316	PA-2	0.5153	0.5156	0.5159	0.1428	
09-04-3	0.2308	0.2307	0.2307	PA-3	0.5200	0.5203	0.5203	0.1932	

Stack Gas Velocity Profiles
Line Kln



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Project No. Northern P.

1

Year	Day	Hour	C ₁	C ₂	C ₃	C ₄	C ₅	C ₆	C ₇	C ₈	C ₉	C ₁₀	C ₁₁	C ₁₂	C ₁₃	C ₁₄	C ₁₅	C ₁₆	C ₁₇	C ₁₈	C ₁₉	C ₂₀	C ₂₁	C ₂₂	C ₂₃	C ₂₄	C ₂₅	C ₂₆	C ₂₇	C ₂₈	C ₂₉	C ₃₀	C ₃₁	C ₃₂	C ₃₃	C ₃₄	C ₃₅	C ₃₆	C ₃₇	C ₃₈	C ₃₉	C ₄₀	C ₄₁	C ₄₂	C ₄₃	C ₄₄	C ₄₅	C ₄₆	C ₄₇	C ₄₈	C ₄₉	C ₅₀	C ₅₁	C ₅₂	C ₅₃	C ₅₄	C ₅₅	C ₅₆	C ₅₇	C ₅₈	C ₅₉	C ₆₀	C ₆₁	C ₆₂	C ₆₃	C ₆₄	C ₆₅	C ₆₆	C ₆₇	C ₆₈	C ₆₉	C ₇₀	C ₇₁	C ₇₂	C ₇₃	C ₇₄	C ₇₅	C ₇₆	C ₇₇	C ₇₈	C ₇₉	C ₈₀	C ₈₁	C ₈₂	C ₈₃	C ₈₄	C ₈₅	C ₈₆	C ₈₇	C ₈₈	C ₈₉	C ₉₀	C ₉₁	C ₉₂	C ₉₃	C ₉₄	C ₉₅	C ₉₆	C ₉₇	C ₉₈	C ₉₉	C ₁₀₀	C ₁₀₁	C ₁₀₂	C ₁₀₃	C ₁₀₄	C ₁₀₅	C ₁₀₆	C ₁₀₇	C ₁₀₈	C ₁₀₉	C ₁₁₀	C ₁₁₁	C ₁₁₂	C ₁₁₃	C ₁₁₄	C ₁₁₅	C ₁₁₆	C ₁₁₇	C ₁₁₈	C ₁₁₉	C ₁₂₀	C ₁₂₁	C ₁₂₂	C ₁₂₃	C ₁₂₄	C ₁₂₅	C ₁₂₆	C ₁₂₇	C ₁₂₈	C ₁₂₉	C ₁₃₀	C ₁₃₁	C ₁₃₂	C ₁₃₃	C ₁₃₄	C ₁₃₅	C ₁₃₆	C ₁₃₇	C ₁₃₈	C ₁₃₉	C ₁₄₀	C ₁₄₁	C ₁₄₂	C ₁₄₃	C ₁₄₄	C ₁₄₅	C ₁₄₆	C ₁₄₇	C ₁₄₈	C ₁₄₉	C ₁₅₀	C ₁₅₁	C ₁₅₂	C ₁₅₃	C ₁₅₄	C ₁₅₅	C ₁₅₆	C ₁₅₇	C ₁₅₈	C ₁₅₉	C ₁₆₀	C ₁₆₁	C ₁₆₂	C ₁₆₃	C ₁₆₄	C ₁₆₅	C ₁₆₆	C ₁₆₇	C ₁₆₈	C ₁₆₉	C ₁₇₀	C ₁₇₁	C ₁₇₂	C ₁₇₃	C ₁₇₄	C ₁₇₅	C ₁₇₆	C ₁₇₇	C ₁₇₈	C ₁₇₉	C ₁₈₀	C ₁₈₁	C ₁₈₂	C ₁₈₃	C ₁₈₄	C ₁₈₅	C ₁₈₆	C ₁₈₇	C ₁₈₈	C ₁₈₉	C ₁₉₀	C ₁₉₁	C ₁₉₂	C ₁₉₃	C ₁₉₄	C ₁₉₅	C ₁₉₆	C ₁₉₇	C ₁₉₈	C ₁₉₉	C ₂₀₀	C ₂₀₁	C ₂₀₂	C ₂₀₃	C ₂₀₄	C ₂₀₅	C ₂₀₆	C ₂₀₇	C ₂₀₈	C ₂₀₉	C ₂₁₀	C ₂₁₁	C ₂₁₂	C ₂₁₃	C ₂₁₄	C ₂₁₅	C ₂₁₆	C ₂₁₇	C ₂₁₈	C ₂₁₉	C ₂₂₀	C ₂₂₁	C ₂₂₂	C ₂₂₃	C ₂₂₄	C ₂₂₅	C ₂₂₆	C ₂₂₇	C ₂₂₈	C ₂₂₉	C ₂₃₀	C ₂₃₁	C ₂₃₂	C ₂₃₃	C ₂₃₄	C ₂₃₅	C ₂₃₆	C ₂₃₇	C ₂₃₈	C ₂₃₉	C ₂₄₀	C ₂₄₁	C ₂₄₂	C ₂₄₃	C ₂₄₄	C ₂₄₅	C ₂₄₆	C ₂₄₇	C ₂₄₈	C ₂₄₉	C ₂₅₀	C ₂₅₁	C ₂₅₂	C ₂₅₃	C ₂₅₄	C ₂₅₅	C ₂₅₆	C ₂₅₇	C ₂₅₈	C ₂₅₉	C ₂₆₀	C ₂₆₁	C ₂₆₂	C ₂₆₃	C ₂₆₄	C ₂₆₅	C ₂₆₆	C ₂₆₇	C ₂₆₈	C ₂₆₉	C ₂₇₀	C ₂₇₁	C ₂₇₂	C ₂₇₃	C ₂₇₄	C ₂₇₅	C ₂₇₆	C ₂₇₇	C ₂₇₈	C ₂₇₉	C ₂₈₀	C ₂₈₁	C ₂₈₂	C ₂₈₃	C ₂₈₄	C ₂₈₅	C ₂₈₆	C ₂₈₇	C ₂₈₈	C ₂₈₉	C ₂₉₀	C ₂₉₁	C ₂₉₂	C ₂₉₃	C ₂₉₄	C ₂₉₅	C ₂₉₆	C ₂₉₇	C ₂₉₈	C ₂₉₉	C ₃₀₀	C ₃₀₁	C ₃₀₂	C ₃₀₃	C ₃₀₄	C ₃₀₅	C ₃₀₆	C ₃₀₇	C ₃₀₈	C ₃₀₉	C ₃₁₀	C ₃₁₁	C ₃₁₂	C ₃₁₃	C ₃₁₄	C ₃₁₅	C ₃₁₆	C ₃₁₇	C ₃₁₈	C ₃₁₉	C ₃₂₀	C ₃₂₁
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Summary of AWWA DATA

Client: Northern Pulp
Project No.: 12191288
Block: Linn 10N
Tall No.: 1

Year	Day	Hour	O ₂	CO ₂	DO	BO ₅	BOC + TRS	TRR	Year	Day	Hour	O ₂	CO ₂	CO	BO ₅	BOC + TRS	TRR
(Julian)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(Julian)	(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2014	237	1005	0.611	21.88	1.88	0.263	-4.291	-4.628	2014	238	005	0.602	20.32	2.888	0.286	0.918	0.523
2014	237	1006	0.623	22.04	1.89	0.277	-4.276	-4.658	2014	238	006	0.601	20.84	2.881	0.287	0.744	0.487
2014	237	1007	0.627	22.16	1.88	0.272	-4.338	-4.81	2014	238	007	0.602	20.68	2.881	0.289	0.783	0.474
2014	237	1008	0.604	22.11	1.88	0.284	-4.341	-4.825	2014	238	008	0.601	20.8	2.881	0.285	0.859	0.586
2014	237	1009	0.715	21.88	1.88	0.276	-4.438	-4.713	2014	238	009	0.603	20.82	2.876	0.288	1.032	0.784
2014	237	1010	0.708	21.9	1.778	0.278	-4.401	-4.677	2014	238	010	0.602	20.82	2.876	0.288	1.25	0.884
2014	237	1011	0.682	21.9	1.888	0.278	-4.811	-4.788	2014	238	011	0.604	20.84	2.881	0.284	1.081	0.787
2014	237	1012	0.786	21.81	1.88	0.278	-4.387	-4.683	2014	238	012	0.606	20.86	2.881	0.281	1.054	0.763
2014	237	1013	0.717	21.9	1.823	0.278	-4.387	-4.683	2014	238	013	0.602	20.88	2.881	0.285	0.872	0.677
2014	237	1014	0.694	21.81	1.88	0.272	-4.442	-4.714	2014	238	014	0.607	20.88	2.881	0.283	0.817	0.676
2014	237	1015	0.788	21.83	1.88	0.278	-4.387	-4.683	2014	238	015	0.604	20.81	2.889	0.288	0.948	0.85
2014	237	1016	0.823	21.83	1.888	0.273	-4.887	-4.87	2014	238	016	0.603	20.81	2.884	0.283	1.018	0.727
2014	237	1017	0.828	21.82	1.884	0.280	-4.738	-4.808	2014	238	017	0.605	20.85	2.878	0.288	1.021	0.723
2014	237	1018	0.782	21.84	1.88	0.272	-4.887	-4.829	2014	238	018	0.605	20.84	2.882	0.288	1.147	0.854
2014	237	1019	0.788	21.72	1.88	0.273	-4.88	-4.77	2014	238	019	0.605	20.84	2.882	0.288	1.004	0.713
2014	237	1020	0.834	21.86	1.88	0.273	-4.48	-4.68	2014	238	020	0.605	20.47	4.08	0.282	1.281	0.878
2014	237	1021	0.871	21.88	1.88	0.278	-4.738	-4.813	2014	238	021	0.604	20.4	4.022	0.288	1.138	0.884
2014	237	1022	0.81	21.82	1.88	0.278	-4.738	-4.813	2014	238	022	0.602	20.48	4.022	0.282	1.154	0.903
2014	237	1023	0.81	21.87	1.778	0.278	-4.788	-4.881	2014	238	023	0.784	20.15	4.022	0.284	1.088	0.773
2014	237	1024	0.781	21.81	1.88	0.278	-4.824	-4.8	2014	238	024	0.788	20.17	4.044	0.284	0.3	0.588
2014	237	1025	0.884	21.88	1.88	0.278	-4.888	-4.887	2014	238	025	0.784	20.14	4.022	0.283	0.823	0.71
2014	237	1026	0.73	21.87	1.738	0.278	-4.881	-4.74	2014	238	026	0.788	20.12	4.022	0.278	0.821	0.648
2014	237	1027	0.712	21.88	1.88	0.288	-4.888	-4.877	2014	238	027	0.788	20.12	4.022	0.277	1.087	0.78
2014	237	1028	0.884	21.86	1.884	0.281	-4.734	-4.848	2014	238	028	0.778	20.19	4.088	0.276	0.873	0.624
2014	237	1029	0.882	21.83	1.88	0.284	-4.818	-4.812	2014	238	029	0.884	20.27	4.073	0.285	1.081	0.788
2014	237	1030	0.872	21.83	1.888	0.283	-4.781	-4.888	2014	238	030	0.887	20.27	4.073	0.285	1.083	0.803
2014	237	1031	0.888	21.47	1.88	0.278	-4.782	-4.887	2014	238	031	0.887	20.27	4.073	0.285	1.225	0.823
2014	237	1032	0.787	21.87	1.888	0.28	-4.888	-4.878	2014	238	032	0.788	20.28	4.073	0.278	1.088	0.824
2014	237	1033	0.882	21.81	1.88	0.288	-4.882	-4.888	2014	238	033	0.784	20.31	4.083	0.272	1.184	0.882
2014	237	1034	0.784	21.88	1.88	0.284	-4.824	-4.888	2014	238	034	0.718	20.32	4.071	0.274	1.118	0.844
2014	237	1035	0.781	21.88	1.23	0.281	-4.888	-4.827	2014	238	035	0.843	20.43	4.728	0.274	1.08	0.808
2014	237	1036	0.882	21.48	1.88	0.281	-4.828	-4.821	2014	238	036	0.848	20.43	4.884	0.281	0.878	0.74
2014	237	1037	0.884	21.48	1.888	0.281	-4.828	-4.821	2014	238	037	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1038	0.884	21.48	1.888	0.281	-4.828	-4.821	2014	238	038	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1039	0.884	21.48	1.888	0.281	-4.828	-4.821	2014	238	039	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1040	0.884	21.48	1.888	0.281	-4.828	-4.821	2014	238	040	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1041	0.781	21.83	1.88	0.28	-4.828	-4.828	2014	238	041	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1042	0.778	21.88	1.88	0.28	-4.828	-4.828	2014	238	042	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1043	0.754	21.72	1.888	0.281	-4.828	-4.828	2014	238	043	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1044	0.771	21.72	1.88	0.287	-4.828	-4.828	2014	238	044	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1045	0.788	21.7	1.88	0.287	-4.828	-4.828	2014	238	045	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1046	0.788	21.7	1.88	0.287	-4.828	-4.828	2014	238	046	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1047	0.884	21.8	1.88	0.284	-4.828	-4.828	2014	238	047	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1048	0.878	21.48	1.88	0.283	-4.828	-4.828	2014	238	048	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1049	0.882	21.47	1.88	0.288	-4.828	-4.828	2014	238	049	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1050	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	050	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1051	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	051	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1052	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	052	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1053	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	053	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1054	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	054	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1055	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	055	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1056	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	056	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1057	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	057	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1058	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	058	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1059	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	059	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1060	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	060	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1061	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	061	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1062	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	062	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1063	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	063	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1064	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	064	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1065	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	065	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1066	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	066	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1067	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	067	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1068	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	068	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1069	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	069	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1070	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	070	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1071	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	071	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1072	0.882	21.47	1.888	0.284	-4.828	-4.828	2014	238	072	0.848	20.43	4.884	0.281	1.022	0.848
2014	237	1073	0.882	21.47	1.88												

Client: Northern Plains
Project No.: 121511273
Stock Line 1014
Test No.:

Client: Northern Plains
Project No.: 121511273
Stock Line 1014
Test No.:

Year	Day	Hour	O ₂	CO ₂	CO	SO ₂	NO _x + TSP	TSP
	(Date)		(%)	(%)	(ppm)	(ppm)	(ppm)	(ppm)
2014	227	1803	8.11	21.11	1.13	0.308	-0.008	-0.714
2014	227	1801	8.08	21.07	1.00	0.304	-0.008	-0.714
2014	227	1802	8.10	21.08	1.00	0.304	-0.008	-0.714
2014	227	1803	8.03	20.88	1.00	0.304	-0.008	-0.714
2014	227	1804	8.04	21.01	1.00	0.304	-0.008	-0.714
2014	227	1805	8.05	21.04	1.00	0.304	-0.008	-0.714
2014	227	1806	8.06	21.07	1.00	0.304	-0.008	-0.714
2014	227	1807	8.13	21.09	1.00	0.304	-0.008	-0.714
2014	227	1808	8.11	21.12	1.00	0.304	-0.008	-0.714
2014	227	1809	8.08	21.10	1.00	0.304	-0.008	-0.714
2014	227	1810	8.05	21.08	1.00	0.304	-0.008	-0.714
2014	227	1811	8.02	21.06	1.00	0.304	-0.008	-0.714
2014	227	1812	8.00	21.04	1.00	0.304	-0.008	-0.714
2014	227	1813	8.00	21.02	1.00	0.304	-0.008	-0.714
2014	227	1814	8.00	21.00	1.00	0.304	-0.008	-0.714
2014	227	1815	8.00	20.98	1.00	0.304	-0.008	-0.714
2014	227	1816	8.00	20.96	1.00	0.304	-0.008	-0.714
2014	227	1817	8.00	20.94	1.00	0.304	-0.008	-0.714
2014	227	1818	8.00	20.92	1.00	0.304	-0.008	-0.714
2014	227	1819	8.00	20.90	1.00	0.304	-0.008	-0.714
2014	227	1820	8.00	20.88	1.00	0.304	-0.008	-0.714
2014	227	1821	8.00	20.86	1.00	0.304	-0.008	-0.714
2014	227	1822	8.00	20.84	1.00	0.304	-0.008	-0.714
2014	227	1823	8.00	20.82	1.00	0.304	-0.008	-0.714
2014	227	1824	8.00	20.80	1.00	0.304	-0.008	-0.714
2014	227	1825	8.00	20.78	1.00	0.304	-0.008	-0.714
2014	227	1826	8.00	20.76	1.00	0.304	-0.008	-0.714
2014	227	1827	8.00	20.74	1.00	0.304	-0.008	-0.714
2014	227	1828	8.00	20.72	1.00	0.304	-0.008	-0.714
2014	227	1829	8.00	20.70	1.00	0.304	-0.008	-0.714
2014	227	1830	8.00	20.68	1.00	0.304	-0.008	-0.714
2014	227	1831	8.00	20.66	1.00	0.304	-0.008	-0.714
2014	227	1832	8.00	20.64	1.00	0.304	-0.008	-0.714
2014	227	1833	8.00	20.62	1.00	0.304	-0.008	-0.714
2014	227	1834	8.00	20.60	1.00	0.304	-0.008	-0.714
2014	227	1835	8.00	20.58	1.00	0.304	-0.008	-0.714
2014	227	1836	8.00	20.56	1.00	0.304	-0.008	-0.714
2014	227	1837	8.00	20.54	1.00	0.304	-0.008	-0.714
2014	227	1838	8.00	20.52	1.00	0.304	-0.008	-0.714
2014	227	1839	8.00	20.50	1.00	0.304	-0.008	-0.714
2014	227	1840	8.00	20.48	1.00	0.304	-0.008	-0.714
2014	227	1841	8.00	20.46	1.00	0.304	-0.008	-0.714
2014	227	1842	8.00	20.44	1.00	0.304	-0.008	-0.714
2014	227	1843	8.00	20.42	1.00	0.304	-0.008	-0.714
2014	227							

Summary of RAW DATA

Client: Northern Poly
 Project No.: 131815004
 Basic: Lime Kiln
 Test No.: 1

Year	Day	Hour	O ₂ (%)	CO ₂ (%)	CO (ppm)	NO _x (ppm)	SO ₂ + TSS (ppm)	TSS (ppm)
2014	207	21:26	4.816	21.26	1.888	0.288	-1.90	-1.628
2014	207	21:28	4.891	21.44	1.88	0.302	-3.888	-1.671
2014	207	21:30	6.008	21.27	1.88	0.304	-3.888	-1.923
2014	207	21:32	6.079	21.25	1.88	0.308	-3.18	-1.891
2014	207	21:34	6.01	21.28	2.025	0.303	-3.025	-3.833
2014	207	21:40	6.016	21.31	1.88	0.308	-3.7	-3.988
2014	207	21:41	6.021	21.29	1.53	0.301	-3.677	-3.971
2014	207	21:42	6.038	21.22	2.025	0.303	-3.671	-3.984
2014	207	21:43	6.102	21.21	1.888	0.288	-3.488	-3.984
2014	207	21:45	6.01	21.2	1.888	0.284	-3.505	-3.628
2014	207	21:46	6.038	21.27	1.888	0.308	-3.678	-3.622
2014	207	21:48	6.094	21.19	1.888	0.387	-3.432	-3.728
2014	207	21:49	6.094	21.27	1.888	0.308	-3.584	-3.887
2014	207	21:50	6.124	21.17	1.888	0.288	-3.548	-3.94
2014	207	21:51	6.117	21.2	1.888	0.304	-3.482	-3.971
2014	207	21:52	6.042	21.28	1.888	0.308	-3.472	-3.778
2014	207	21:53	6.201	21.27	1.3	0.304	-3.928	-3.88
2014	207	21:54	6.173	21.45	1.88	0.308	-3.484	-3.928
2014	207	21:55	6.173	21.29	1.88	0.308	-3.482	-3.741
2014	207	21:56	6.091	21.27	1.888	0.314	-3.488	-3.778
2014	207	21:57	6.085	21.38	2.013	0.308	-3.488	-3.724
2014	207	21:58	6.085	21.34	2.013	0.304	-3.47	-3.784
2014	207	21:59	6.027	21.31	2.005	0.321	-3.501	-3.622
2014	207	22:00	6.028	21.3	1.238	0.318	-3.381	-3.708
2014	207	22:01	6.027	21.24	2.008	0.314	-3.128	-3.447
2014	207	22:02	6.028	21.2	2.005	0.31	-3.428	-3.723
2014	207	22:03	6.028	21.21	2.013	0.318	-3.388	-3.701
2014	207	22:04	6.028	21.28	2.013	0.312	-3.379	-3.671
2014	207	22:05	6.024	21.37	1.88	0.318	-3.353	-3.671
2014	207	22:06	6.013	21.38	1.88	0.322	-3.418	-3.742
2014	207	22:07	6.008	21.46	1.88	0.322	-3.488	-3.782
2014	207	22:08	6.008	21.48	1.3	0.322	-3.388	-3.671
2014	207	22:09	6.008	21.48	1.88	0.321	-3.488	-3.788
2014	207	22:10	6.008	21.48	1.88	0.328	-3.327	-3.628
2014	207	22:11	6.021	21.43	1.888	0.317	-3.317	-3.624
2014	207	22:12	6.008	21.44	1.88	0.323	-3.318	-3.72
2014	207	22:13	6.008	21.43	1.88	0.321	-3.308	-3.718
2014	207	22:14	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:15	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:16	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:17	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:18	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:19	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:20	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:21	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:22	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:23	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:24	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:25	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:26	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:27	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:28	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:29	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:30	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:31	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:32	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:33	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:34	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:35	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:36	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:37	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:38	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:39	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:40	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:41	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:42	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:43	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:44	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:45	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:46	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:47	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:48	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:49	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:50	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:51	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:52	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:53	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:54	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:55	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:56	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:57	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:58	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	22:59	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:00	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:01	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:02	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:03	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:04	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:05	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:06	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:07	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:08	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:09	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:10	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:11	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:12	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:13	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:14	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:15	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:16	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:17	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:18	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:19	6.008	21.43	1.88	0.321	-3.31	-3.621
2014	207	23:20	6.008	21.43	1.88	0.321	-3.31	-3.621

Client: Northern Pulp
Project No.: 121811280
Sheet: Line KM
Tool No.: 1

Year	Day	Hour	O ₂	CO ₂	CO	SO ₂	SO ₂ + TSS	TSS	Year	Day	Hour	O ₂	CO ₂	CO	SO ₂	SO ₂ + TSS	TSS
(Y)	(Jahr)		(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(Y)	(Jahr)		(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)
2014	237	2332	0.325	20.57	2.03	0.328	-1.81	-2.879	2014	238	1129	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2331	0.347	20.67	1.88	0.328	-1.81	-2.879	2014	238	1130	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2330	0.322	20.59	2.025	0.328	-1.81	-2.879	2014	238	1131	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2329	0.347	20.56	1.877	0.312	-1.458	-2.879	2014	238	1132	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2328	0.326	20.56	2.012	0.324	-1.452	-2.879	2014	238	1133	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2327	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1134	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2326	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1135	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2325	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1136	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2324	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1137	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2323	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1138	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2322	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1139	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2321	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1140	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2320	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1141	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2319	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1142	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2318	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1143	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2317	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1144	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2316	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1145	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2315	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1146	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2314	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1147	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2313	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1148	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2312	0.327	20.56	2.025	0.32	-1.871	-2.881	2014	238	1149	0.325	20.529	2.022	0.327	0.329	0.126
2014	237	2311	0.327	20.56	2.025	0.32	-1.87										

Summary of RAW DATA

Client: Northern Pulse
 Project No.: 101011263
 Asset: Live Kite
 Test No.: 1

Year	Day	Hour	O ₂ [ppm]	CO ₂ [%]	CO [ppm]	SO ₂ [ppm]	SO ₂ + TSP [ppm]	TSP [ppm]	Year	Day	Hour	O ₂ [ppm]	CO ₂ [%]	CO [ppm]	SO ₂ [ppm]	SO ₂ + TSP [ppm]	TSP [ppm]
2014	208	103	8.413	20.71	3.218	0.377	-1.730	-2.108	2014	208	1305	8.843	18.73	1.13	0.378	-1.272	-1.848
2014	208	104	8.43	20.69	3.217	0.378	-1.328	-2.010	2014	208	1306	8.821	18.71	1.09	0.379	-1.402	-1.774
2014	208	107	8.38	20.72	3.201	0.377	-1.485	-1.882	2014	208	1307	8.813	18.73	1.09	0.372	-1.217	-1.88
2014	208	109	8.276	20.62	3.228	0.368	-1.488	-1.371	2014	208	1308	8.84	18.81	1.09	0.382	-1.477	-1.858
2014	208	110	8.33	20.8	3.28	0.378	-1.871	-1.548	2014	208	1309	8.848	18.8	1.09	0.383	-1.48	-1.848
2014	208	111	8.384	20.82	3.227	0.384	-1.728	-1.11	2014	208	1310	8.888	18.81	1.09	0.388	-1.317	-1.703
2014	208	112	8.371	20.82	3.35	0.378	-1.722	-1.1	2014	208	1311	8.888	18.81	1.072	0.389	-1.388	-1.748
2014	208	113	8.314	20.89	3.771	0.385	-1.578	-1.882	2014	208	1312	8.88	18.83	1.09	0.391	-1.287	-1.778
2014	208	114	8.338	20.89	3.722	0.38	-1.888	-1.888	2014	208	1313	8.883	18.85	1.09	0.377	-1.388	-1.773
2014	208	115	8.28	20.85	3.788	0.391	-1.819	-2.009	2014	208	1314	8.828	18.83	1.09	0.378	-1.488	-1.734
2014	208	118	8.378	20.81	3.723	0.38	-1.821	-2.221	2014	208	1315	8.845	18.86	1.08	0.383	-1.418	-1.854
2014	208	117	8.388	20.87	3.738	0.383	-1.491	-1.384	2014	208	1316	8.848	18.8	1.08	0.385	-1.481	-1.853
2014	208	118	8.182	20.86	3.788	0.387	-1.883	-1.9	2014	208	1317	8.83	18.83	1.08	0.382	-1.444	-1.828
2014	208	119	8.338	20.8	3.738	0.408	-1.543	-1.881	2014	208	1318	8.791	18.82	1.072	0.387	-1.478	-1.882
2014	208	120	8.388	20.78	3.73	0.388	-1.887	-1.888	2014	208	1319	8.823	18.81	1.08	0.38	-1.488	-1.878
2014	208	121	8.388	20.78	3.788	0.401	-1.488	-1.388	2014	208	1320	8.884	18.88	1.08	0.381	-1.448	-1.83
2014	208	122	8.382	20.73	3.771	0.391	-1.481	-1.872	2014	208	1321	8.888	18.91	1.08	0.381	-1.488	-1.873
2014	208	123	8.338	20.78	3.78	0.385	-1.491	-1.384	2014	208	1322	8.848	18.88	1.13	0.383	-1.488	-1.873
2014	208	124	8.4	20.72	3.884	0.408	-1.491	-1.107	2014	208	1323	8.888	18.8	1.08	0.379	-1.518	-1.884
2014	208	125	8.382	20.8	3.888	0.388	-1.488	-1.888	2014	208	1324	8.888	18.85	1.08	0.388	-1.528	-1.888
2014	208	126	8.33	20.82	3.887	0.4	-1.477	-1.877	2014	208	1325	8.882	18.9	1.072	0.38	-1.477	-1.887
2014	208	127	8.271	20.88	3.785	0.387	-1.45	-1.547	2014	208	1326	8.838	18.87	1.08	0.382	-1.488	-1.887
2014	208	128	8.374	20.74	3.713	0.388	-1.48	-1.888	2014	208	1327	8.888	18.88	1.13	0.377	-1.514	-1.884
2014	208	129	8.432	20.7	3.755	0.383	-1.484	-1.882	2014	208	1328	8.888	18.88	1.13	0.377	-1.514	-1.884
2014	208	130	8.418	20.88	3.813	0.385	-1.887	-1.882	2014	208	1329	8.817	20.83	1.083	0.388	-1.581	-1.85
2014	208	131	8.388	20.71	3.746	0.382	-1.43	-1.322	2014	208	1330	8.883	20.81	1.08	0.371	-1.521	-1.882
2014	208	132	8.381	20.74	3.829	0.388	-1.388	-1.381	2014	208	1331	8.811	18.88	1.13	0.373	-1.543	-1.818
2014	208	133	8.378	20.78	3.713	0.388	-1.488	-1.888	2014	208	1332	8.888	18.77	1.08	0.371	-1.514	-1.888
2014	208	134	8.418	20.73	3.785	0.388	-1.371	-1.788	2014	208	1333	8.884	18.88	1.08	0.379	-1.581	-1.882
2014	208	135	8.38	20.83	3.779	0.403	-1.478	-1.879	2014	208	1334	8.888	18.88	1.08	0.373	-1.581	-1.814
2014	208	136	8.378	20.84	3.788	0.388	-1.488	-1.887	2014	208	1335	8.888	18.88	1.08	0.373	-1.581	-1.814
2014	208	137	8.388	20.85	3.887	0.472	-1.388	-1.778	2014	208	1336	8.888	18.88	1.08	0.373	-1.581	-1.814
2014	208	138	8.311	20.84	3.888	0.411	-1.488	-1.888	2014	208	1337	8.888	18.7	1.08	0.372	-1.588	-1.878
2014	208	139	8.388	20.88	3.779	0.408	-1.4	-1.888	2014	208	1338	8.888	18.77	1.08	0.371	-1.788	-2.127
2014	208	140	8.388	20.88	3.779	0.408	-1.4	-1.888	2014	208	1339	8.888	18.74	1.08	0.373	-1.578	-1.848
2014	208	141	8.374	20.87	3.888	0.413	-1.488	-1.788	2014	208	1340	8.888	18.88	1.08	0.363	-1.588	-2.081
2014	208	142	8.371	20.88	3.888	0.414	-1.388	-1.888	2014	208	1341	8.888	18.88	1.08	0.373	-1.588	-1.878
2014	208	143	8.378	20.84	3.888	0.388	-1.377	-1.773	2014	208	1342	8.888	18.8	1.13	0.371	-1.778	-2.148
2014	208	144	8.387	20.81	3.888	0.404	-1.388	-1.8	2014	208	1343	8.888	18.8	1.088	0.385	-1.888	-2.048
2014	208	145	8.438	20.46	3.888	0.403	-1.48	-1.883	2014	208	1344	8.887	18.82	1.072	0.388	-1.788	-2.127
2014	208	146	8.438	20.84	3.888	0.412	-1.488	-1.887	2014	208	1345	8.887	18.83	1.083	0.384	-1.781	-2.118
2014	208	147	8.438	20.87	3.888	0.403	-1.388	-1.784	2014	208	1346	8.887	18.83	1.083	0.388	-1.887	-2.118
2014	208	148	8.438	20.8	3.888	0.403	-1.388	-1.784	2014	208	1347	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	149	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1348	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	150	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1349	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	151	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1350	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	152	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1351	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	153	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1352	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	154	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1353	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	155	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1354	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	156	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1355	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	157	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1356	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	158	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1357	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	159	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1358	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	160	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1359	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	161	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1360	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	162	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1361	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	163	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1362	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	164	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1363	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	165	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1364	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	166	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1365	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	167	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1366	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	168	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1367	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	169	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1368	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	170	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1369	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	171	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1370	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	172	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1371	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	173	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1372	8.887	18.88	1.088	0.388	-1.887	-2.118
2014	208	174	8.438	20.82	3.888	0.403	-1.388	-1.784	2014	208	1373	8.887	18.88</				

Client:	Northern Poly
Project No.:	121011200
Client:	Line KB
Test No.:	1

[illegible]

Summary of CORRECTED DATA

Client: Northern Poly
 Project No.: 121611010
 Block: Line K01
 Test No.: 1

Year	Day	Hour	O ₂	CO ₂	SO ₂	NO _x	PM ₁₀	PM _{2.5}	THS	THS 4 hour rolling average	Year	Day	Hour	O ₂	CO ₂	SO ₂	NO _x	PM ₁₀	PM _{2.5}	THS	THS 4 hour rolling average
2014	1004	1004	4.88	21.75	1.98	0.26	0.40	0.26			2014	1004	1004	4.88	21.75	1.98	0.26	0.40	0.26		
2014	1005	1005	4.89	21.70	2.00	0.28	0.43	0.27			2014	1005	1005	4.89	21.70	2.00	0.28	0.43	0.27		
2014	1006	1006	4.90	21.65	2.02	0.30	0.45	0.29			2014	1006	1006	4.90	21.65	2.02	0.30	0.45	0.29		
2014	1007	1007	4.91	21.60	2.04	0.32	0.47	0.31			2014	1007	1007	4.91	21.60	2.04	0.32	0.47	0.31		
2014	1008	1008	4.92	21.55	2.06	0.34	0.49	0.33			2014	1008	1008	4.92	21.55	2.06	0.34	0.49	0.33		
2014	1009	1009	4.93	21.50	2.08	0.36	0.51	0.35			2014	1009	1009	4.93	21.50	2.08	0.36	0.51	0.35		
2014	1010	1010	4.94	21.45	2.10	0.38	0.53	0.37			2014	1010	1010	4.94	21.45	2.10	0.38	0.53	0.37		
2014	1011	1011	4.95	21.40	2.12	0.40	0.55	0.39			2014	1011	1011	4.95	21.40	2.12	0.40	0.55	0.39		
2014	1012	1012	4.96	21.35	2.14	0.42	0.57	0.41			2014	1012	1012	4.96	21.35	2.14	0.42	0.57	0.41		
2014	1013	1013	4.97	21.30	2.16	0.44	0.59	0.43			2014	1013	1013	4.97	21.30	2.16	0.44	0.59	0.43		
2014	1014	1014	4.98	21.25	2.18	0.46	0.61	0.45			2014	1014	1014	4.98	21.25	2.18	0.46	0.61	0.45		
2014	1015	1015	4.99	21.20	2.20	0.48	0.63	0.47			2014	1015	1015	4.99	21.20	2.20	0.48	0.63	0.47		
2014	1016	1016	5.00	21.15	2.22	0.50	0.65	0.49			2014	1016	1016	5.00	21.15	2.22	0.50	0.65	0.49		
2014	1017	1017	5.01	21.10	2.24	0.52	0.67	0.51			2014	1017	1017	5.01	21.10	2.24	0.52	0.67	0.51		
2014	1018	1018	5.02	21.05	2.26	0.54	0.69	0.53			2014	1018	1018	5.02	21.05	2.26	0.54	0.69	0.53		
2014	1019	1019	5.03	21.00	2.28	0.56	0.71	0.55			2014	1019	1019	5.03	21.00	2.28	0.56	0.71	0.55		
2014	1020	1020	5.04	20.95	2.30	0.58	0.73	0.57			2014	1020	1020	5.04	20.95	2.30	0.58	0.73	0.57		
2014	1021	1021	5.05	20.90	2.32	0.60	0.75	0.59			2014	1021	1021	5.05	20.90	2.32	0.60	0.75	0.59		
2014	1022	1022	5.06	20.85	2.34	0.62	0.77	0.61			2014	1022	1022	5.06	20.85	2.34	0.62	0.77	0.61		
2014	1023	1023	5.07	20.80	2.36	0.64	0.79	0.63			2014	1023	1023	5.07	20.80	2.36	0.64	0.79	0.63		
2014	1024	1024	5.08	20.75	2.38	0.66	0.81	0.65			2014	1024	1024	5.08	20.75	2.38	0.66	0.81	0.65		
2014	1025	1025	5.09	20.70	2.40	0.68	0.83	0.67			2014	1025	1025	5.09	20.70	2.40	0.68	0.83	0.67		
2014	1026	1026	5.10	20.65	2.42	0.70	0.85	0.69			2014	1026	1026	5.10	20.65	2.42	0.70	0.85	0.69		
2014	1027	1027	5.11	20.60	2.44	0.72	0.87	0.71			2014	1027	1027	5.11	20.60	2.44	0.72	0.87	0.71		
2014	1028	1028	5.12	20.55	2.46	0.74	0.89	0.73			2014	1028	1028	5.12	20.55	2.46	0.74	0.89	0.73		
2014	1029	1029	5.13	20.50	2.48	0.76	0.91	0.75			2014	1029	1029	5.13	20.50	2.48	0.76	0.91	0.75		
2014	1030	1030	5.14	20.45	2.50	0.78	0.93	0.77			2014	1030	1030	5.14	20.45	2.50	0.78	0.93	0.77		
2014	1031	1031	5.15	20.40	2.52	0.80	0.95	0.79			2014	1031	1031	5.15	20.40	2.52	0.80	0.95	0.79		
2014	1032	1032	5.16	20.35	2.54	0.82	0.97	0.81			2014	1032	1032	5.16	20.35	2.54	0.82	0.97	0.81		
2014	1033	1033	5.17	20.30	2.56	0.84	0.99	0.83			2014	1033	1033	5.17	20.30	2.56	0.84	0.99	0.83		
2014	1034	1034	5.18	20.25	2.58	0.86	1.01	0.85			2014	1034	1034	5.18	20.25	2.58	0.86	1.01	0.85		
2014	1035	1035	5.19	20.20	2.60	0.88	1.03	0.87			2014	1035	1035	5.19	20.20	2.60	0.88	1.03	0.87		
2014	1036	1036	5.20	20.15	2.62	0.90	1.05	0.89			2014	1036	1036	5.20	20.15	2.62	0.90	1.05	0.89		
2014	1037	1037	5.21	20.10	2.64	0.92	1.07	0.91			2014	1037	1037	5.21	20.10	2.64	0.92	1.07	0.91		
2014	1038	1038	5.22	20.05	2.66	0.94	1.09	0.93			2014	1038	1038	5.22	20.05	2.66	0.94	1.09	0.93		
2014	1039	1039	5.23	20.00	2.68	0.96	1.11	0.95			2014	1039	1039	5.23	20.00	2.68	0.96	1.11	0.95		
2014	1040	1040	5.24	19.95	2.70	0.98	1.13	0.97			2014	1040	1040	5.24	19.95	2.70	0.98	1.13	0.97		
2014	1041	1041	5.25	19.90	2.72	1.00	1.15	0.99			2014	1041	1041	5.25	19.90	2.72	1.00	1.15	0.99		
2014	1042	1042	5.26	19.85	2.74	1.02	1.17	1.01			2014	1042	1042	5.26	19.85	2.74	1.02	1.17	1.01		
2014	1043	1043	5.27	19.80	2.76	1.04	1.19	1.03			2014	1043	1043	5.27	19.80	2.76	1.04	1.19	1.03		
2014	1044	1044	5.28	19.75	2.78	1.06	1.21	1.05			2014	1044	1044	5.28	19.75	2.78	1.06	1.21	1.05		
2014	1045	1045	5.29	19.70	2.80	1.08	1.23	1.07			2014	1045	1045	5.29	19.70	2.80	1.08	1.23	1.07		
2014	1046	1046	5.30	19.65	2.82	1.10	1.25	1.09			2014	1046	1046	5.30	19.65	2.82	1.10	1.25	1.09		
2014	1047	1047	5.31	19.60	2.84	1.12	1.27	1.11			2014	1047	1047	5.31	19.60	2.84	1.12	1.27	1.11		
2014	1048	1048	5.32	19.55	2.86	1.14	1.29	1.13			2014	1048	1048	5.32	19.55	2.86	1.14	1.29	1.13		
2014	1049	1049	5.33	19.50	2.88	1.16	1.31	1.15			2014	1049	1049	5.33	19.50	2.88	1.16	1.31	1.15		
2014	1050	1050	5.34	19.45	2.90	1.18	1.33	1.17			2014	1050	1050	5.34	19.45	2.90	1.18	1.33	1.17		
2014	1051	1051	5.35	19.40	2.92	1.20	1.35	1.19			2014	1051	1051	5.35	19.40	2.92	1.20	1.35	1.19		
2014	1052	1052	5.36	19.35	2.94	1.22	1.37	1.21			2014	1052	1052	5.36	19.35	2.94	1.22	1.37	1.21		
2014	1053	1053	5.37	19.30	2.96	1.24	1.39	1.23			2014	1053	1053	5.37	19.30	2.96	1.24	1.39	1.23		
2014	1054	1054	5.38	19.25	2.98	1.26	1.41	1.25			2014	1054	1054	5.38	19.25	2.98	1.26	1.41	1.25		
2014	1055	1055	5.39	19.20	3.00	1.28	1.43	1.27			2014	1055	1055	5.39	19.20	3.00	1.28	1.43	1.27		
2014	1056	1056	5.40	19.15	3.02	1.30	1.45	1.29			2014	1056	1056	5.40	19.15	3.02	1.30	1.45	1.29		
2014	1057	1057	5.41	19.10	3.04	1.32	1.47	1.31			2014	1057	1057	5.41	19.10	3.04	1.32	1.47	1.31		
2014	1058	1058	5.42	19.05	3.06	1.34	1.49	1.33			2014	1058	1058	5.42	19.05	3.06	1.34	1.49	1.33		
2014	1059	1059	5.43	19.00	3.08	1.36	1.51	1.35			2014	1059	1059	5.43	19.00	3.08	1.36	1.51	1.35		
2014	1060	1060	5.44	18.95	3.10	1.38	1.53	1.37			2014	1060	1060	5.44	18.95	3.10	1.38	1.53	1.37		
2014	1061	1061	5.45	18.90	3.12	1.40	1.55	1.39			2014	1061	1061	5.45	18.90	3.12	1.40	1.55	1.39		
2014	1062	1062	5.46	18.85	3.14	1.42	1.57	1.41			2014	1062	1062	5.46	18.85	3.14	1.42	1.57	1.41		
2014	1063	1063	5.47	18.80	3.16	1.44	1.59	1.43			2014	1063	1063	5.47	18.80	3.16	1.44	1.59	1.43		
2014	1064	1064	5.48	18.75	3.18	1.46	1.61	1.45			2014	1064	1064	5.48	18.75	3.18	1.46	1.61	1.45		
2014	1065	1065	5.49	18.70	3.20	1.48	1.63	1.47			2014	1065	1065	5.49	18.70	3.20	1.48	1.63	1.47		
2014	1066	1066	5.50	18.65	3.22	1.50	1.65	1.49			2014	1066	1066	5.50	18.65	3.22	1.50	1.65	1.49		
2014	1067	1067	5.51	18.60	3.24	1.52	1.67	1.51			2014	1067	1067	5.51	18.60	3.24	1.52	1.67	1.51		
2014	1068	1068	5.52	18.55	3.26	1.54	1.69	1.53			2014	1068	1068	5.52	18.55	3.26	1.54	1.69			

Summary of CORRECTED DATA

Case: Northern Poly
Project (No.): 12101229
Sheet: Line 122
Total No.: 1

Year	Day	Hour	Q ₁	Q ₂	Q ₃	Q ₄	Q ₅	Q ₆	Q ₇	Q ₈	Q ₉	Q ₁₀	Q ₁₁	Q ₁₂	Q ₁₃	Q ₁₄	Q ₁₅	Q ₁₆	Q ₁₇	Q ₁₈	Q ₁₉	Q ₂₀	Q ₂₁	Q ₂₂	Q ₂₃	Q ₂₄	Q ₂₅	Q ₂₆	Q ₂₇	Q ₂₈	Q ₂₉	Q ₃₀	Q ₃₁	Q ₃₂	Q ₃₃	Q ₃₄	Q ₃₅	Q ₃₆	Q ₃₇	Q ₃₈	Q ₃₉	Q ₄₀	Q ₄₁	Q ₄₂	Q ₄₃	Q ₄₄	Q ₄₅	Q ₄₆	Q ₄₇	Q ₄₈	Q ₄₉	Q ₅₀	Q ₅₁	Q ₅₂	Q ₅₃	Q ₅₄	Q ₅₅	Q ₅₆	Q ₅₇	Q ₅₈	Q ₅₉	Q ₆₀	Q ₆₁	Q ₆₂	Q ₆₃	Q ₆₄	Q ₆₅	Q ₆₆	Q ₆₇	Q ₆₈	Q ₆₉	Q ₇₀	Q ₇₁	Q ₇₂	Q ₇₃	Q ₇₄	Q ₇₅	Q ₇₆	Q ₇₇	Q ₇₈	Q ₇₉	Q ₈₀	Q ₈₁	Q ₈₂	Q ₈₃	Q ₈₄	Q ₈₅	Q ₈₆	Q ₈₇	Q ₈₈	Q ₈₉	Q ₉₀	Q ₉₁	Q ₉₂	Q ₉₃	Q ₉₄	Q ₉₅	Q ₉₆	Q ₉₇	Q ₉₈	Q ₉₉	Q ₁₀₀	Q ₁₀₁	Q ₁₀₂	Q ₁₀₃	Q ₁₀₄	Q ₁₀₅	Q ₁₀₆	Q ₁₀₇	Q ₁₀₈	Q ₁₀₉	Q ₁₁₀	Q ₁₁₁	Q ₁₁₂	Q ₁₁₃	Q ₁₁₄	Q ₁₁₅	Q ₁₁₆	Q ₁₁₇	Q ₁₁₈	Q ₁₁₉	Q ₁₂₀	Q ₁₂₁	Q ₁₂₂	Q ₁₂₃	Q ₁₂₄	Q ₁₂₅	Q ₁₂₆	Q ₁₂₇	Q ₁₂₈	Q ₁₂₉	Q ₁₃₀	Q ₁₃₁	Q ₁₃₂	Q ₁₃₃	Q ₁₃₄	Q ₁₃₅	Q ₁₃₆	Q ₁₃₇	Q ₁₃₈	Q ₁₃₉	Q ₁₄₀	Q ₁₄₁	Q ₁₄₂	Q ₁₄₃	Q ₁₄₄	Q ₁₄₅	Q ₁₄₆	Q ₁₄₇	Q ₁₄₈	Q ₁₄₉	Q ₁₅₀	Q ₁₅₁	Q ₁₅₂	Q ₁₅₃	Q ₁₅₄	Q ₁₅₅	Q ₁₅₆	Q ₁₅₇	Q ₁₅₈	Q ₁₅₉	Q ₁₆₀	Q ₁₆₁	Q ₁₆₂	Q ₁₆₃	Q ₁₆₄	Q ₁₆₅	Q ₁₆₆	Q ₁₆₇	Q ₁₆₈	Q ₁₆₉	Q ₁₇₀	Q ₁₇₁	Q ₁₇₂	Q ₁₇₃	Q ₁₇₄	Q ₁₇₅	Q ₁₇₆	Q ₁₇₇	Q ₁₇₈	Q ₁₇₉	Q ₁₈₀	Q ₁₈₁	Q ₁₈₂	Q ₁₈₃	Q ₁₈₄	Q ₁₈₅	Q ₁₈₆	Q ₁₈₇	Q ₁₈₈	Q ₁₈₉	Q ₁₉₀	Q ₁₉₁	Q ₁₉₂	Q ₁₉₃	Q ₁₉₄	Q ₁₉₅	Q ₁₉₆	Q ₁₉₇	Q ₁₉₈	Q ₁₉₉	Q ₂₀₀	Q ₂₀₁	Q ₂₀₂	Q ₂₀₃	Q ₂₀₄	Q ₂₀₅	Q ₂₀₆	Q ₂₀₇	Q ₂₀₈	Q ₂₀₉	Q ₂₁₀	Q ₂₁₁	Q ₂₁₂	Q ₂₁₃	Q ₂₁₄	Q ₂₁₅	Q ₂₁₆	Q ₂₁₇	Q ₂₁₈	Q ₂₁₉	Q ₂₂₀	Q ₂₂₁	Q ₂₂₂	Q ₂₂₃	Q ₂₂₄	Q ₂₂₅	Q ₂₂₆	Q ₂₂₇	Q ₂₂₈	Q ₂₂₉	Q ₂₃₀	Q ₂₃₁	Q ₂₃₂	Q ₂₃₃	Q ₂₃₄	Q ₂₃₅	Q ₂₃₆	Q ₂₃₇	Q ₂₃₈	Q ₂₃₉	Q ₂₄₀	Q ₂₄₁	Q ₂₄₂	Q ₂₄₃	Q ₂₄₄	Q ₂₄₅	Q ₂₄₆	Q ₂₄₇	Q ₂₄₈	Q ₂₄₉	Q ₂₅₀	Q ₂₅₁	Q ₂₅₂	Q ₂₅₃	Q ₂₅₄	Q ₂₅₅	Q ₂₅₆	Q ₂₅₇	Q ₂₅₈	Q ₂₅₉	Q ₂₆₀	Q ₂₆₁	Q ₂₆₂	Q ₂₆₃	Q ₂₆₄	Q ₂₆₅	Q ₂₆₆	Q ₂₆₇	Q ₂₆₈	Q ₂₆₉	Q ₂₇₀	Q ₂₇₁	Q ₂₇₂	Q ₂₇₃	Q ₂₇₄	Q ₂₇₅	Q ₂₇₆	Q ₂₇₇	Q ₂₇₈	Q ₂₇₉	Q ₂₈₀	Q ₂₈₁	Q ₂₈₂	Q ₂₈₃	Q ₂₈₄	Q ₂₈₅	Q ₂₈₆	Q ₂₈₇	Q ₂₈₈	Q ₂₈₉	Q ₂₉₀	Q ₂₉₁	Q ₂₉₂	Q ₂₉₃	Q ₂₉₄	Q ₂₉₅	Q ₂₉₆	Q ₂₉₇	Q ₂₉₈	Q ₂₉₉	Q ₃₀₀	Q ₃₀₁	Q ₃₀₂	Q ₃₀₃	Q ₃₀₄	Q ₃₀₅	Q ₃₀₆	Q ₃₀₇	Q ₃₀₈	Q ₃₀₉	Q ₃₁₀	Q ₃₁₁	Q ₃₁₂	Q ₃₁₃	Q ₃₁₄	Q ₃₁₅	Q ₃₁₆	Q ₃₁₇	Q ₃₁₈	Q ₃₁₉	Q ₃₂₀	Q ₃₂₁	Q ₃₂₂	Q ₃₂₃	Q ₃₂₄	Q ₃₂₅	Q ₃₂₆	Q ₃₂₇	Q ₃₂₈	Q ₃₂₉	Q ₃₃₀	Q ₃₃₁	Q ₃₃₂	Q ₃₃₃	Q ₃₃₄	Q ₃₃₅	Q ₃₃₆	Q ₃₃₇	Q ₃₃₈	Q ₃₃₉	Q ₃₄₀	Q ₃₄₁	Q ₃₄₂	Q ₃₄₃	Q ₃₄₄	Q ₃₄₅	Q ₃₄₆	Q ₃₄₇	Q ₃₄₈	Q ₃₄₉	Q ₃₅₀	Q ₃₅₁	Q ₃₅₂	Q ₃₅₃	Q ₃₅₄	Q ₃₅₅	Q ₃₅₆	Q ₃₅₇	Q ₃₅₈	Q ₃₅₉	Q ₃₆₀	Q ₃₆₁	Q ₃₆₂	Q ₃₆₃	Q ₃₆₄	Q ₃₆₅	Q ₃₆₆	Q ₃₆₇	Q ₃₆₈	Q ₃₆₉	Q ₃₇₀	Q ₃₇₁	Q ₃₇₂	Q ₃₇₃	Q ₃₇₄	Q ₃₇₅	Q ₃₇₆	Q ₃₇₇	Q ₃₇₈	Q ₃₇₉	Q ₃₈₀	Q ₃₈₁	Q ₃₈₂	Q ₃₈₃	Q ₃₈₄	Q ₃₈₅	Q ₃₈₆	Q ₃₈₇	Q ₃₈₈	Q ₃₈₉	Q ₃₉₀	Q ₃₉₁	Q ₃₉₂	Q ₃₉₃	Q ₃₉₄	Q ₃₉₅	Q ₃₉₆	Q ₃₉₇	Q ₃₉₈	Q ₃₉₉	Q ₄₀₀	Q ₄₀₁	Q ₄₀₂	Q ₄₀₃	Q ₄₀₄	Q ₄₀₅	Q ₄₀₆	Q ₄₀₇	Q ₄₀₈	Q ₄₀₉	Q ₄₁₀	Q ₄₁₁	Q ₄₁₂	Q ₄₁₃	Q ₄₁₄	Q ₄₁₅	Q ₄₁₆	Q ₄₁₇	Q ₄₁₈	Q ₄₁₉	Q ₄₂₀	Q ₄₂₁	Q ₄₂₂	Q ₄₂₃	Q ₄₂₄	Q ₄₂₅	Q ₄₂₆	Q ₄₂₇	Q ₄₂₈	Q ₄₂₉	Q ₄₃₀	Q ₄₃₁	Q ₄₃₂	Q ₄₃₃	Q ₄₃₄	Q ₄₃₅	Q ₄₃₆	Q ₄₃₇	Q ₄₃₈	Q ₄₃₉	Q ₄₄₀	Q ₄₄₁	Q ₄₄₂	Q ₄₄₃	Q ₄₄₄	Q ₄₄₅	Q ₄₄₆	Q ₄₄₇	Q ₄₄₈	Q ₄₄₉	Q ₄₅₀	Q ₄₅₁	Q ₄₅₂	Q ₄₅₃	Q ₄₅₄	Q ₄₅₅	Q ₄₅₆	Q ₄₅₇	Q ₄₅₈	Q ₄₅₉	Q ₄₆₀	Q ₄₆₁	Q ₄₆₂	Q ₄₆₃	Q ₄₆₄	Q ₄₆₅	Q ₄₆₆	Q ₄₆₇	Q ₄₆₈	Q ₄₆₉	Q ₄₇₀	Q ₄₇₁	Q ₄₇₂	Q ₄₇₃	Q ₄₇₄	Q ₄₇₅	Q ₄₇₆	Q ₄₇₇	Q ₄₇₈	Q ₄₇₉	Q ₄₈₀	Q ₄₈₁	Q ₄₈₂	Q ₄₈₃	Q ₄₈₄	Q ₄₈₅	Q ₄₈₆	Q ₄₈₇	Q ₄₈₈	Q ₄₈₉	Q ₄₉₀	Q ₄₉₁	Q ₄₉₂	Q ₄₉₃	Q ₄₉₄	Q ₄₉₅	Q ₄₉₆	Q ₄₉₇	Q ₄₉₈	Q ₄₉₉	Q ₅₀₀	Q ₅₀₁	Q ₅₀₂	Q ₅₀₃	Q ₅₀₄	Q ₅₀₅	Q ₅₀₆	Q ₅₀₇	Q ₅₀₈	Q ₅₀₉	Q ₅₁₀	Q ₅₁₁	Q ₅₁₂	Q ₅₁₃	Q ₅₁₄	Q ₅₁₅	Q ₅₁₆	Q ₅₁₇	Q ₅₁₈	Q ₅₁₉	Q ₅₂₀	Q ₅₂₁	Q ₅₂₂	Q ₅₂₃	Q ₅₂₄	Q ₅₂₅	Q ₅₂₆	Q ₅₂₇	Q ₅₂₈	Q ₅₂₉	Q ₅₃₀	Q ₅₃₁	Q ₅₃₂	Q ₅₃₃	Q ₅₃₄	Q ₅₃₅	Q ₅₃₆	Q ₅₃₇	Q ₅₃₈	Q ₅₃₉	Q ₅₄₀	Q ₅₄₁	Q ₅₄₂	Q ₅₄₃	Q ₅₄₄	Q ₅₄₅	Q ₅₄₆	Q ₅₄₇	Q ₅₄₈	Q ₅₄₉	Q ₅₅₀	Q ₅₅₁	Q ₅₅₂	Q ₅₅₃	Q ₅₅₄	Q ₅₅₅	Q ₅₅₆	Q ₅₅₇	Q ₅₅₈	Q ₅₅₉	Q ₅₆₀	Q ₅₆₁	Q ₅₆₂	Q ₅₆₃	Q ₅₆₄	Q ₅₆₅	Q ₅₆₆	Q ₅₆₇	Q ₅₆₈	Q ₅₆₉	Q ₅₇₀	Q ₅₇₁	Q ₅₇₂	Q ₅₇₃	Q ₅₇₄	Q ₅₇₅	Q ₅₇₆	Q ₅₇₇	Q ₅₇₈	Q ₅₇₉	Q ₅₈₀	Q ₅₈₁	Q ₅₈₂	Q ₅₈₃	Q ₅₈₄	Q ₅₈₅	Q ₅₈₆	Q ₅₈₇	Q ₅₈₈	Q ₅₈₉	Q ₅₉₀	Q ₅₉₁	Q ₅₉₂	Q ₅₉₃	Q ₅₉₄	Q ₅₉₅	Q ₅₉₆	Q ₅₉₇	Q ₅₉₈	Q ₅₉₉	Q ₆₀₀	Q ₆₀₁	Q ₆₀₂	Q ₆₀₃	Q ₆₀₄	Q ₆₀₅	Q ₆₀₆	Q ₆₀₇	Q ₆₀₈	Q ₆₀₉	Q ₆₁₀	Q ₆₁₁	Q ₆₁₂	Q ₆₁₃	Q ₆₁₄	Q ₆₁₅	Q ₆₁₆	Q ₆₁₇	Q ₆₁₈	Q ₆₁₉	Q ₆₂₀	Q ₆₂₁	Q ₆₂₂	Q ₆₂₃	Q ₆₂₄	Q ₆₂₅	Q ₆₂₆	Q ₆₂₇	Q ₆₂₈	Q ₆₂₉	Q ₆₃₀	Q ₆₃₁	Q ₆₃₂	Q ₆₃₃	Q ₆₃₄	Q ₆₃₅	Q ₆₃₆	Q ₆₃₇	Q ₆₃₈	Q ₆₃₉	Q ₆₄₀	Q ₆₄₁	Q ₆₄₂	Q ₆₄₃	Q ₆₄₄	Q ₆₄₅	Q ₆₄₆	Q ₆₄₇	Q ₆₄₈	Q ₆₄₉	Q ₆₅₀	Q ₆₅₁	Q ₆₅₂	Q ₆₅₃	Q ₆₅₄	Q ₆₅₅	Q ₆₅₆	Q ₆₅₇	Q ₆₅₈	Q ₆₅₉	Q ₆₆₀	Q ₆₆₁	Q ₆₆₂	Q ₆₆₃	Q ₆₆₄	Q ₆₆₅	Q ₆₆₆	Q ₆₆₇	Q ₆₆₈	Q ₆₆₉	Q ₆₇₀	Q ₆₇₁	Q ₆₇₂	Q ₆₇₃	Q ₆₇₄	Q ₆₇₅	Q ₆₇₆	Q ₆₇₇	Q ₆₇₈	Q ₆₇₉	Q ₆₈₀	Q ₆₈₁	Q ₆₈₂	Q ₆₈₃	Q ₆₈₄	Q ₆₈₅	Q ₆₈₆	Q ₆₈₇	Q ₆₈₈	Q ₆₈₉	Q ₆₉₀	Q ₆₉₁	Q ₆₉₂	Q ₆₉₃	Q ₆₉₄	Q ₆₉₅	Q ₆₉₆	Q ₆₉₇	Q ₆₉₈	Q ₆₉₉	Q ₇₀₀	Q ₇₀₁	Q ₇₀₂	Q ₇₀₃	Q ₇₀₄	Q ₇₀₅	Q ₇₀₆	Q ₇₀₇	Q ₇₀₈	Q ₇₀₉	Q ₇₁₀	Q ₇₁₁	Q ₇₁₂	Q ₇₁₃	Q ₇₁₄	Q ₇₁₅	Q ₇₁₆	Q ₇₁₇	Q ₇₁₈	Q ₇₁₉	Q ₇₂₀	Q ₇₂₁	Q ₇₂₂	Q ₇₂₃	Q ₇₂₄	Q ₇₂₅	Q ₇₂₆	Q ₇₂₇	Q ₇₂₈	Q ₇₂₉	Q ₇₃₀	Q ₇₃₁	Q ₇₃₂	Q ₇₃₃	Q ₇₃₄	Q ₇₃₅	Q ₇₃₆	Q ₇₃₇	Q ₇₃₈	Q ₇₃₉	Q ₇₄₀	Q ₇₄₁	Q ₇₄₂	Q ₇₄₃	Q ₇₄₄	Q ₇₄₅	Q ₇₄₆	Q ₇₄₇	Q ₇₄₈	Q ₇₄₉	Q ₇₅₀	Q ₇₅₁	Q ₇₅₂	Q ₇₅₃	Q ₇₅₄	Q ₇₅₅	Q ₇₅₆	Q ₇₅₇	Q ₇₅₈	Q ₇₅₉	Q ₇₆₀	Q ₇₆₁	Q ₇₆₂	Q ₇₆₃	Q ₇₆₄	Q ₇₆₅	Q ₇₆₆	Q ₇₆₇	Q ₇₆₈	Q ₇₆₉	Q ₇₇₀	Q ₇₇₁	Q ₇₇₂	Q ₇₇₃	Q ₇₇₄	Q ₇₇₅	Q ₇₇₆	Q ₇₇₇	Q ₇₇₈	Q ₇₇₉	Q ₇₈₀	Q ₇₈₁	Q ₇₈₂	Q ₇₈₃	Q ₇₈₄	Q ₇₈₅	Q ₇₈₆	Q ₇₈₇	Q ₇₈₈	Q ₇₈₉	Q ₇₉₀	Q ₇₉₁	Q ₇₉₂	Q ₇₉₃	Q ₇₉₄	Q ₇₉₅	Q ₇₉₆	Q ₇₉₇	Q ₇₉₈	Q ₇₉₉	Q ₈₀₀	Q ₈₀₁	Q ₈₀₂	Q ₈₀₃	Q ₈₀₄	Q ₈₀₅	Q ₈₀₆	Q ₈₀₇	Q ₈₀₈	Q ₈₀₉	Q ₈₁₀	Q ₈₁₁	Q ₈₁₂	Q ₈₁₃	Q ₈₁₄	Q ₈₁₅	Q ₈₁₆	Q ₈₁₇	Q ₈₁₈	Q ₈₁₉	Q ₈₂₀	Q ₈₂₁	Q ₈₂₂	Q ₈₂₃	Q ₈₂₄	Q ₈₂₅	Q ₈₂₆	Q ₈₂₇	Q ₈₂₈	Q ₈₂₉	Q ₈₃₀	Q ₈₃₁	Q ₈₃₂	Q ₈₃₃	Q ₈₃₄	Q ₈₃₅	Q ₈₃₆	Q ₈₃₇	Q ₈₃₈	Q ₈₃₉	Q ₈₄₀	Q ₈₄₁	Q ₈₄₂	Q ₈₄₃	Q ₈₄₄	Q ₈₄₅	Q ₈₄₆	Q ₈₄₇	Q ₈₄₈	Q ₈₄₉	Q ₈₅₀	Q ₈₅₁	Q ₈₅₂	Q ₈₅₃	Q ₈₅₄	Q ₈₅₅	Q ₈₅₆	Q ₈₅₇	Q ₈₅₈	Q ₈₅₉	Q ₈₆₀	Q ₈₆₁	Q ₈₆₂	Q ₈₆₃	Q ₈₆₄	Q ₈₆₅	Q ₈₆₆	Q ₈₆₇	Q ₈₆₈	Q ₈₆₉	Q ₈₇₀	Q ₈₇₁	Q ₈₇₂	Q ₈₇₃	Q ₈₇₄	Q ₈₇₅	Q ₈₇₆	Q ₈₇₇	Q ₈₇₈	Q ₈₇₉	Q ₈₈₀	Q ₈₈₁
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Summary of CORRECTED DATA

Client: Matthews Pkg
Project No.: 121611288
Sheet: L1000 F01
Task No.: 1

Year	Day	Hour	Q ₁	Q ₂	Q ₃	Q ₄	Q ₅ + T ₅₀	T ₅₀	T ₅₀ 4 hour rolling average	Year	Day	Hour	Q ₁	Q ₂	Q ₃	Q ₄	Q ₅ + T ₅₀	T ₅₀	T ₅₀ 4 hour rolling average
2014	Monday	05:00	0.51	0.76	0.99	1.20	1.30	1.30	1.30	2014	Monday	05:00	0.51	0.76	0.99	1.20	1.30	1.30	1.30
2014	05:05	0.52	0.77	1.00	1.21	1.31	1.31	1.31	1.31	2014	05:05	0.52	0.77	1.00	1.21	1.31	1.31	1.31	
2014	05:10	0.53	0.78	1.01	1.22	1.32	1.32	1.32	1.32	2014	05:10	0.53	0.78	1.01	1.22	1.32	1.32	1.32	
2014	05:15	0.54	0.79	1.02	1.23	1.33	1.33	1.33	1.33	2014	05:15	0.54	0.79	1.02	1.23	1.33	1.33	1.33	
2014	05:20	0.55	0.80	1.03	1.24	1.34	1.34	1.34	1.34	2014	05:20	0.55	0.80	1.03	1.24	1.34	1.34	1.34	
2014	05:25	0.56	0.81	1.04	1.25	1.35	1.35	1.35	1.35	2014	05:25	0.56	0.81	1.04	1.25	1.35	1.35	1.35	
2014	05:30	0.57	0.82	1.05	1.26	1.36	1.36	1.36	1.36	2014	05:30	0.57	0.82	1.05	1.26	1.36	1.36	1.36	
2014	05:35	0.58	0.83	1.06	1.27	1.37	1.37	1.37	1.37	2014	05:35	0.58	0.83	1.06	1.27	1.37	1.37	1.37	
2014	05:40	0.59	0.84	1.07	1.28	1.38	1.38	1.38	1.38	2014	05:40	0.59	0.84	1.07	1.28	1.38	1.38	1.38	
2014	05:45	0.60	0.85	1.08	1.29	1.39	1.39	1.39	1.39	2014	05:45	0.60	0.85	1.08	1.29	1.39	1.39	1.39	
2014	05:50	0.61	0.86	1.09	1.30	1.40	1.40	1.40	1.40	2014	05:50	0.61	0.86	1.09	1.30	1.40	1.40	1.40	
2014	05:55	0.62	0.87	1.10	1.31	1.41	1.41	1.41	1.41	2014	05:55	0.62	0.87	1.10	1.31	1.41	1.41	1.41	
2014	06:00	0.63	0.88	1.11	1.32	1.42	1.42	1.42	1.42	2014	06:00	0.63	0.88	1.11	1.32	1.42	1.42	1.42	
2014	06:05	0.64	0.89	1.12	1.33	1.43	1.43	1.43	1.43	2014	06:05	0.64	0.89	1.12	1.33	1.43	1.43	1.43	
2014	06:10	0.65	0.90	1.13	1.34	1.44	1.44	1.44	1.44	2014	06:10	0.65	0.90	1.13	1.34	1.44	1.44	1.44	
2014	06:15	0.66	0.91	1.14	1.35	1.45	1.45	1.45	1.45	2014	06:15	0.66	0.91	1.14	1.35	1.45	1.45	1.45	
2014	06:20	0.67	0.92	1.15	1.36	1.46	1.46	1.46	1.46	2014	06:20	0.67	0.92	1.15	1.36	1.46	1.46	1.46	
2014	06:25	0.68	0.93	1.16	1.37	1.47	1.47	1.47	1.47	2014	06:25	0.68	0.93	1.16	1.37	1.47	1.47	1.47	
2014	06:30	0.69	0.94	1.17	1.38	1.48	1.48	1.48	1.48	2014	06:30	0.69	0.94	1.17	1.38	1.48	1.48	1.48	
2014	06:35	0.70	0.95	1.18	1.39	1.49	1.49	1.49	1.49	2014	06:35	0.70	0.95	1.18	1.39	1.49	1.49	1.49	
2014	06:40	0.71	0.96	1.19	1.40	1.50	1.50	1.50	1.50	2014	06:40	0.71	0.96	1.19	1.40	1.50	1.50	1.50	
2014	06:45	0.72	0.97	1.20	1.41	1.51	1.51	1.51	1.51	2014	06:45	0.72	0.97	1.20	1.41	1.51	1.51	1.51	
2014	06:50	0.73	0.98	1.21	1.42	1.52	1.52	1.52	1.52	2014	06:50	0.73	0.98	1.21	1.42	1.52	1.52	1.52	
2014	06:55	0.74	0.99	1.22	1.43	1.53	1.53	1.53	1.53	2014	06:55	0.74	0.99	1.22	1.43	1.53	1.53	1.53	
2014	07:00	0.75	1.00	1.23	1.44	1.54	1.54	1.54	1.54	2014	07:00	0.75	1.00	1.23	1.44	1.54	1.54	1.54	
2014	07:05	0.76	1.01	1.24	1.45	1.55	1.55	1.55	1.55	2014	07:05	0.76	1.01	1.24	1.45	1.55	1.55	1.55	
2014	07:10	0.77	1.02	1.25	1.46	1.56	1.56	1.56	1.56	2014	07:10	0.77	1.02	1.25	1.46	1.56	1.56	1.56	
2014	07:15	0.78	1.03	1.26	1.47	1.57	1.57	1.57	1.57	2014	07:15	0.78	1.03	1.26	1.47	1.57	1.57	1.57	
2014	07:20	0.79	1.04	1.27	1.48	1.58	1.58	1.58	1.58	2014	07:20	0.79	1.04	1.27	1.48	1.58	1.58	1.58	
2014	07:25	0.80	1.05	1.28	1.49	1.59	1.59	1.59	1.59	2014	07:25	0.80	1.05	1.28	1.49	1.59	1.59	1.59	
2014	07:30	0.81	1.06	1.29	1.50	1.60	1.60	1.60	1.60	2014	07:30	0.81	1.06	1.29	1.50	1.60	1.60	1.60	
2014	07:35	0.82	1.07	1.30	1.51	1.61	1.61	1.61	1.61	2014	07:35	0.82	1.07	1.30	1.51	1.61	1.61	1.61	
2014	07:40	0.83	1.08	1.31	1.52	1.62	1.62	1.62	1.62	2014	07:40	0.83	1.08	1.31	1.52	1.62	1.62	1.62	
2014	07:45	0.84	1.09	1.32	1.53	1.63	1.63	1.63	1.63	2014	07:45	0.84	1.09	1.32	1.53	1.63	1.63	1.63	
2014	07:50	0.85	1.10	1.33	1.54	1.64	1.64	1.64	1.64	2014	07:50	0.85	1.10	1.33	1.54	1.64	1.64	1.64	
2014	07:55	0.86	1.11	1.34	1.55	1.65	1.65	1.65	1.65	2014	07:55	0.86	1.11	1.34	1.55	1.65	1.65	1.65	
2014	08:00	0.87	1.12	1.35	1.56	1.66	1.66	1.66	1.66	2014	08:00	0.87	1.12	1.35	1.56	1.66	1.66	1.66	
2014	08:05	0.88	1.13	1.36	1.57	1.67	1.67	1.67	1.67	2014	08:05	0.88	1.13	1.36	1.57	1.67	1.67	1.67	
2014	08:10	0.89	1.14	1.37	1.58	1.68	1.68	1.68	1.68	2014	08:10	0.89	1.14	1.37	1.58	1.68	1.68	1.68	
2014	08:15	0.90	1.15	1.38	1.59	1.69	1.69	1.69	1.69	2014	08:15	0.90	1.15	1.38	1.59	1.69	1.69	1.69	
2014	08:20	0.91	1.16	1.39	1.60	1.70	1.70	1.70	1.70	2014	08:20	0.91	1.16	1.39	1.60	1.70	1.70	1.70	
2014	08:25	0.92	1.17	1.40	1.61	1.71	1.71	1.71	1.71	2014	08:25	0.92	1.17	1.40	1.61	1.71	1.71	1.71	
2014	08:30	0.93	1.18	1.41	1.62	1.72	1.72	1.72	1.72	2014	08:30	0.93	1.18	1.41	1.62	1.72	1.72	1.72	
2014	08:35	0.94	1.19	1.42	1.63	1.73	1.73	1.73	1.73	2014	08:35	0.94	1.19	1.42	1.63	1.73	1.73	1.73	
2014	08:40	0.95	1.20	1.43	1.64	1.74	1.74	1.74	1.74	2014	08:40	0.95	1.20	1.43	1.64	1.74	1.74	1.74	
2014	08:45	0.96	1.21	1.44	1.65	1.75	1.75	1.75	1.75	2014	08:45	0.96	1.21	1.44	1.65	1.75	1.75	1.75	
2014	08:50	0.97	1.22	1.45	1.66	1.76	1.76	1.76	1.76	2014	08:50	0.97	1.22	1.45	1.66	1.76	1.76	1.76	
2014	08:55	0.98	1.23	1.46	1.67	1.77	1.77	1.77	1.77	2014	08:55	0.98	1.23	1.46	1.67	1.77	1.77	1.77	
2014	09:00	0.99	1.24	1.47	1.68	1.78	1.78	1.78	1.78	2014	09:00	0.99	1.24	1.47	1.68	1.78	1.78	1.78	
2014	09:05	1.00	1.25	1.48	1.69	1.79	1.79	1.79	1.79	2014	09:05	1.00	1.25	1.48	1.69	1.79	1.79	1.79	
2014	09:10	1.01	1.26	1.49	1.70	1.80	1.80	1.80	1.80	2014	09:10	1.01	1.26	1.49	1.70	1.80	1.80	1.80	
2014	09:15	1.02	1.27	1.50	1.71	1.81	1.81	1.81	1.81	2014	09:15	1.02	1.27	1.50	1.71	1.81	1.81	1.81	
2014	09:20	1.03	1.28	1.51	1.72	1.82	1.82	1.82	1.82	2014	09:20	1.03	1.28	1.51	1.72	1.82	1.82	1.82	
2014	09:25	1.04	1.29	1.52	1.73	1.83	1.83	1.83	1.83	2014	09:25	1.04	1.29	1.52	1.73	1.83	1.83	1.83	
2014	09:30	1.05	1.30	1.53	1.74	1.84	1.84	1.84	1.84	2014	09:30	1.05	1.30	1.53	1.74	1.84	1.84	1.84	
2014	09:35	1.06	1.31	1.54	1.75	1.85	1.85	1.85	1.85	2014	09:35	1.06	1.31	1.54	1.75	1.85	1.85	1.85	
2014	09:40	1.07	1.32	1.55	1.76	1.86	1.86	1.86	1.86	2014	09:40	1.07	1.32	1.55	1.76	1.86	1.86	1.86	
2014	09:45	1.08	1.33	1.56	1.77	1.87	1.87	1.87	1.87	2014	09:45	1.08	1.33	1.56	1.77	1.87	1.87	1.87	
2014	09:50	1.09	1.34	1.57	1.78	1.88	1.88	1.88	1.88	2014	09:50	1.09	1.34	1.57	1.78	1.88	1.88	1.88	
2014	09:55	1.10	1.35	1.58	1.79	1.89	1.89	1.89	1.89	2014	09:55	1.10	1.35	1.58	1.79	1.89	1.89	1.89	
2014	10:00	1.11	1.36	1.59	1.80	1.90	1.90	1.90	1.90	2014	10:00	1.11	1.36	1.59	1.80	1.90	1.90	1.90	
2014	10:05	1.12	1.37	1.60	1.81	1.91	1.91	1.91	1.91	2014	10:05	1.12	1.37	1.60	1.81	1.91	1.91	1.91	
2014	10:10	1.13	1.38	1.61	1.82	1.92	1.92	1.92	1.92	2014	10:10	1.13	1.38	1.61	1.82	1.92	1.92	1.92	
2014	10:15	1.14	1.39	1.62	1.83	1.93	1.93	1.93	1.93	2014	10:15	1.14	1.39	1.62	1.83	1.93	1.93	1.93	
2014	10:20	1.15	1.40	1.63	1.84	1.94	1.94	1.94	1.94	2014	10:20	1.15	1.40	1.63	1.84	1.94	1.94	1.94	
2014	10:25	1.16	1.41	1.64	1.85	1.95	1.95	1.95	1.95	2014	10:25	1.16	1.41	1.64	1.85	1.95	1.95	1.95	
2014	10:30	1.17	1.42	1.65	1.86	1.96	1.96	1.96	1.96	2014	10:30	1.17	1.42	1.65	1.86	1.96	1.96	1.96	

Client:	Northern Pulse
Project No.:	021011309
Block:	Line 375
Test No.:	1

[illegible]

Client: Northern Pulp
Project No.: 121811269
Sheet: Line 104
Text No.: 1

[illegible]

Summary of collected data

Client: Northern Poly
Project No.: 12131270
Block: Line Kilo
Test No.: 1

Year	Day	Mon	Tu	We	Th	Fr	Sat + Sun	YTD	TOT 6 hour	Year	Day	Mon	Tu	We	Th	Sat + Sun	TOT	TOT 6 hour
	(Julian)								(approx)		(Julian)							(approx)
2014	201	129	6.16	20.70	4.78	0.00	0.00	0.00	0.00	2014	230	130	6.04	20.69	38.20	2.00	0.00	38.20
2014	202	130	6.20	20.70	4.82	0.00	0.00	0.00	0.00	2014	231	131	6.09	20.70	38.20	2.00	0.00	38.20
2014	203	131	6.25	20.70	4.77	0.00	0.00	0.00	0.00	2014	232	132	6.14	20.71	38.20	2.00	0.00	38.20
2014	204	132	6.16	20.70	4.69	0.00	0.00	0.00	0.00	2014	233	133	6.19	20.71	38.20	2.00	0.00	38.20
2014	205	133	6.25	20.70	4.72	0.00	0.00	0.00	0.00	2014	234	134	6.24	20.72	38.20	2.00	0.00	38.20
2014	206	134	6.17	20.70	4.72	0.00	0.00	0.00	0.00	2014	235	135	6.29	20.73	38.20	2.00	0.00	38.20
2014	207	135	6.25	20.70	4.69	0.00	0.00	0.00	0.00	2014	236	136	6.34	20.74	38.20	2.00	0.00	38.20
2014	208	136	6.10	20.70	4.62	0.00	0.00	0.00	0.00	2014	237	137	6.39	20.75	38.20	2.00	0.00	38.20
2014	209	137	6.00	20.69	4.72	0.00	0.00	0.00	0.00	2014	238	138	6.44	20.76	38.20	2.00	0.00	38.20
2014	210	138	6.09	21.05	4.68	0.00	0.00	0.00	0.00	2014	239	139	6.49	20.77	38.20	2.00	0.00	38.20
2014	211	139	6.10	20.99	4.67	0.00	0.00	0.00	0.00	2014	240	140	6.54	20.78	38.20	2.00	0.00	38.20
2014	212	140	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	241	141	6.59	20.79	38.20	2.00	0.00	38.20
2014	213	141	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	242	142	6.64	20.80	38.20	2.00	0.00	38.20
2014	214	142	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	243	143	6.69	20.81	38.20	2.00	0.00	38.20
2014	215	143	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	244	144	6.74	20.82	38.20	2.00	0.00	38.20
2014	216	144	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	245	145	6.79	20.83	38.20	2.00	0.00	38.20
2014	217	145	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	246	146	6.84	20.84	38.20	2.00	0.00	38.20
2014	218	146	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	247	147	6.89	20.85	38.20	2.00	0.00	38.20
2014	219	147	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	248	148	6.94	20.86	38.20	2.00	0.00	38.20
2014	220	148	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	249	149	6.99	20.87	38.20	2.00	0.00	38.20
2014	221	149	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	250	150	7.04	20.88	38.20	2.00	0.00	38.20
2014	222	150	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	251	151	7.09	20.89	38.20	2.00	0.00	38.20
2014	223	151	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	252	152	7.14	20.90	38.20	2.00	0.00	38.20
2014	224	152	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	253	153	7.19	20.91	38.20	2.00	0.00	38.20
2014	225	153	6.16	20.99	4.64	0.00	0.00	0.00	0.00	2014	254	154	7.24	20.92	38.20	2.00	0.00	38.20
2014	226	154	6.17	20.99	4.63	0.00	0.00	0.00	0.00	2014	255	155	7.29	20.93	38.20	2.00	0.00	38.20
2014	227	155	6.25	20.99	4.60	0.00	0.00	0.00	0.00	2014	256	156	7.34	20.94	38.20	2.00	0.00	38.20
2014	228	156	6.10	20.99	4.53	0.00	0.00	0.00	0.00	2014	257	157	7.39	20.95	38.20	2.00	0.00	38.20
2014	229	157	6.00	20.98	4.67	0.00	0.00	0.00	0.00	2014	258	158	7.44	20.96	38.20	2.00	0.00	38.20
2014	230	158	6.09	21.04	4.63	0.00	0.00	0.00	0.00	2014	259	159	7.49	20.97	38.20	2.00	0.00	38.20
2014	231	159	6.10	20.98	4.62	0.00	0.00	0.00	0.00	2014	260	160	7.54	20.98	38.20	2.00	0.00	38.20
2014	232	160	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	261	161	7.59	20.99	38.20	2.00	0.00	38.20
2014	233	161	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	262	162	7.64	21.00	38.20	2.00	0.00	38.20
2014	234	162	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	263	163	7.69	21.01	38.20	2.00	0.00	38.20
2014	235	163	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	264	164	7.74	21.02	38.20	2.00	0.00	38.20
2014	236	164	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	265	165	7.79	21.03	38.20	2.00	0.00	38.20
2014	237	165	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	266	166	7.84	21.04	38.20	2.00	0.00	38.20
2014	238	166	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	267	167	7.89	21.05	38.20	2.00	0.00	38.20
2014	239	167	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	268	168	7.94	21.06	38.20	2.00	0.00	38.20
2014	240	168	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	269	169	7.99	21.07	38.20	2.00	0.00	38.20
2014	241	169	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	270	170	8.04	21.08	38.20	2.00	0.00	38.20
2014	242	170	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	271	171	8.09	21.09	38.20	2.00	0.00	38.20
2014	243	171	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	272	172	8.14	21.10	38.20	2.00	0.00	38.20
2014	244	172	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	273	173	8.19	21.11	38.20	2.00	0.00	38.20
2014	245	173	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	274	174	8.24	21.12	38.20	2.00	0.00	38.20
2014	246	174	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	275	175	8.29	21.13	38.20	2.00	0.00	38.20
2014	247	175	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	276	176	8.34	21.14	38.20	2.00	0.00	38.20
2014	248	176	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	277	177	8.39	21.15	38.20	2.00	0.00	38.20
2014	249	177	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	278	178	8.44	21.16	38.20	2.00	0.00	38.20
2014	250	178	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	279	179	8.49	21.17	38.20	2.00	0.00	38.20
2014	251	179	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	280	180	8.54	21.18	38.20	2.00	0.00	38.20
2014	252	180	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	281	181	8.59	21.19	38.20	2.00	0.00	38.20
2014	253	181	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	282	182	8.64	21.20	38.20	2.00	0.00	38.20
2014	254	182	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	283	183	8.69	21.21	38.20	2.00	0.00	38.20
2014	255	183	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	284	184	8.74	21.22	38.20	2.00	0.00	38.20
2014	256	184	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	285	185	8.79	21.23	38.20	2.00	0.00	38.20
2014	257	185	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	286	186	8.84	21.24	38.20	2.00	0.00	38.20
2014	258	186	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	287	187	8.89	21.25	38.20	2.00	0.00	38.20
2014	259	187	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	288	188	8.94	21.26	38.20	2.00	0.00	38.20
2014	260	188	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	289	189	8.99	21.27	38.20	2.00	0.00	38.20
2014	261	189	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	290	190	9.04	21.28	38.20	2.00	0.00	38.20
2014	262	190	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	291	191	9.09	21.29	38.20	2.00	0.00	38.20
2014	263	191	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	292	192	9.14	21.30	38.20	2.00	0.00	38.20
2014	264	192	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	293	193	9.19	21.31	38.20	2.00	0.00	38.20
2014	265	193	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	294	194	9.24	21.32	38.20	2.00	0.00	38.20
2014	266	194	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	295	195	9.29	21.33	38.20	2.00	0.00	38.20
2014	267	195	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	296	196	9.34	21.34	38.20	2.00	0.00	38.20
2014	268	196	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	297	197	9.39	21.35	38.20	2.00	0.00	38.20
2014	269	197	6.16	20.98	4.59	0.00	0.00	0.00	0.00	2014	298	198	9.44	21.36	38.20	2.00	0.00	38.20
2014	270	198	6.16	20.98	4.59	0.00	0.00	0.00	0.00									

AVERAGE	4.29	21.37	3.33	6.34	8.18	8.34	2.40
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Test Data for Northern Pulp Summer Source Testing
Test #1

Client: Northern Pulp
Job Number: 171511253
Plant: Pulp
Location: Recovery Boiler
Test: 17-1
Date: 15-Apr-14
Parameter: T Bluff
Test Start: 11:10 AM
Test Finish: 1:10 PM

Parameters
Barometric Pressure, Pbar (in. Hg)
Stack Static Pressure, Pstatic (in. H2O)
Ambient Temp, T_a (°F)
ISO Volume Collected, V_{sc} (mL)
Total ISO Sampling Points
Sampling Time per Point, t_{sp} (min)
Resulting Total Error — min
Regulatory Agency

Implinger No.
1
2
3
4

Implinger Contents
100 mL H2O
100 mL H2O
Blank
200g Silica Gel

Final Weight (g)
907.9
874.0
802.6
1091.8

Total Weight (g)
628.7
737.3
722.0
1367.7

Weight of Moisture (g)
28.1
28.1
30.6
33.1

Total Weight Gain (g)
581.8
581.8

Stack Diameter, (in.)
Stack Area, (sq. in.)
Probe Length, (in.)
Nozzle Diameter, (in.)
Flow Coefficient, (CF)
Geometry, meter constant
Port length (in.)

One Meter Temp
Inlet (°F)
Outlet (°F)

Gas Meter
Volume (cu. ft.)

Office
data H (in. H2O)

5-Step Plot
data P (in. H2O)

Stack Gas
Temp, T_g (°F)

Time
(min)

Transverse
Point

Transverse 1	1-1	2.5	154	8.61	8.91	478.123	61	72
	1-2	7.5	129	8.78	8.99	471.420	62	73
	1-3	10	115	8.85	8.94	471.789	63	74
	1-4	12.5	117	8.70	8.99	471.940	64	75
	1-5	15	118	8.91	8.94	473.249	65	76
	1-6	17.5	118	8.63	8.94	476.450	66	77
	1-7	20	117	8.61	8.87	477.676	67	78
	1-8	22.5	117	8.61	8.99	478.718	68	79
	1-9	25	117	8.61	8.91	481.140	69	80
	1-10	27.5	117	8.64	8.91	483.309	70	81
	1-11	30	116	8.61	8.87	483.690	71	82
	1-12	32.5	117	8.67	8.85	481.678	72	83
	1-13	35	116	8.64	8.87	483.100	73	84
	1-14	37.5	116	8.63	8.92	487.684	74	85
	1-15	40	116	8.63	8.99	488.086	75	86
	1-16	42.5	116	8.63	8.94	491.318	76	87
	1-17	45	115	8.63	8.91	492.590	77	88
	1-18	47.5	115	8.61	8.92	492.590	78	89
	1-19	50	117	8.64	8.91	495.203	79	90
	1-20	52.5	117	8.63	8.91	497.720	80	91
	1-21	55	117	8.63	8.88	498.590	81	92
	1-22	57.5	116	8.63	8.94	500.128	82	93
	1-23	60	116	8.67	8.94	500.418	83	94
	1-24	62.5	116	8.67	8.91	502.700	84	95
	1-25	65	116	8.67	8.94	504.008	85	96
	1-26	67.5	116	8.63	8.94	505.770	86	97
	1-27	70	116	8.63	8.94	506.600	87	98
	1-28	72.5	116	8.61	8.91	507.800	88	99
	1-29	75	116	8.61	8.91	509.000	89	100
	1-30	77.5	116	8.61	8.91	510.200	90	101
	1-31	80	117	8.61	8.91	511.400	91	102
	1-32	82.5	117	8.61	8.91	512.600	92	103
	1-33	85	117	8.61	8.91	513.800	93	104
	1-34	87.5	117	8.61	8.91	515.000	94	105
	1-35	90	117	8.61	8.91	516.200	95	106
	1-36	92.5	117	8.61	8.91	517.400	96	107
	1-37	95	117	8.61	8.91	518.600	97	108
	1-38	97.5	117	8.61	8.91	519.800	98	109
	1-39	100	117	8.61	8.91	521.000	99	110
	1-40	102.5	117	8.61	8.91	522.200	100	111
	1-41	105	117	8.61	8.91	523.400	101	112
	1-42	107.5	117	8.61	8.91	524.600	102	113
	1-43	110	117	8.61	8.91	525.800	103	114
	1-44	112.5	117	8.61	8.91	527.000	104	115
	1-45	115	117	8.61	8.91	528.200	105	116
	1-46	117.5	117	8.61	8.91	529.400	106	117
	1-47	120	117	8.61	8.91	530.600	107	118

Calculations for Northern Pipe Company Square Tasting
Test #1

Client: Northern Pipe
Job Number: 17151250
Plant: Picher
Location: Recovery Huber
Test: PM-1
Date: 10-Aug-14
Personnel: T BH/PS

Calculated Parameters

Stack Gas Pressure, Ps (in-Hg) 35.08
Stack Gas Molecular Weight, Dry Basis, M_d (lb-lbmol) 30.00
Volume of Water Vapor Collected, V_w (cc) 27.97
Stack Gas Molecular Weight, Wet Basis, M_w (lb-lbmol) 0.304
Stack Gas Molecular Weight, Wet Basis, M_w (lb-lbmol) 20.36

Isokineticity Checks

Check average Within Criteria

Transverse Point	Time (min)	Stack Gas Temp, T _s (°C)	B-type Pitot, Gage P (in. H ₂ O)	Orifice Gage H (in. H ₂ O)	Stack Gas Velocity, V _s (ft/s)	Meter Press., P _m (in. Hg)	Avg. Temp, T _m (°C)	Gas Meter V _m (sc. ft.)	Vel. @ Ref. V _{ref} (sc. ft.)	Isokinetics I (%)
Traverse 1	2.5	614	0.64	0.91	50.34	30.07	522	1.250	1.344	98.10
	5	619	0.70	0.86	52.86	30.07	522	1.270	1.360	98.78
	7.5	617	0.66	0.94	61.26	30.07	524	1.280	1.340	98.85
	10	617	0.70	0.90	52.78	30.07	524	1.260	1.361	94.51
	12.5	617	0.66	0.93	60.86	30.07	524	1.240	1.326	98.52
	15	618	0.63	0.90	50.11	30.07	523	1.220	1.306	98.44
	17.5	618	0.61	0.87	48.23	30.06	525	1.240	1.327	97.94
	20	617	0.63	0.90	50.07	30.07	525	1.240	1.324	98.96
	22.5	617	0.64	0.91	50.47	30.07	528	1.260	1.378	100.00
	25	617	0.64	0.91	50.47	30.07	528	1.260	1.378	98.24
	27.5	617	0.61	0.87	48.27	30.06	528	1.180	1.270	97.47
	30	618	0.62	0.86	50.06	30.06	527	1.230	1.311	97.47
Traverse 2	32.5	617	0.61	0.87	48.27	30.06	528	1.230	1.327	99.57
	35	620	0.64	0.92	60.98	30.06	529	1.250	1.327	97.45
	37.5	620	0.63	0.90	50.18	30.07	529	1.250	1.327	99.22
	40	620	0.63	0.90	50.18	30.07	530	1.240	1.314	97.25
	42.5	620	0.62	0.89	48.79	30.07	530	1.220	1.293	98.45
	45	620	0.65	0.93	60.98	30.07	530	1.260	1.378	100.38
	47.5	616	0.64	0.92	50.43	30.07	531	1.290	1.366	99.87
	50	617	0.66	0.96	61.26	30.07	531	1.270	1.342	98.51
	52.5	617	0.64	0.93	50.47	30.07	532	1.290	1.404	102.06
	55	617	0.63	0.91	50.07	30.06	532	1.220	1.278	99.87
	57.5	618	0.61	0.86	48.23	30.06	532	1.210	1.255	94.71
	60	614	0.60	0.87	44.75	30.06	532	1.180	1.255	98.97
Traverse 3	62.5	619	0.65	0.94	50.94	30.07	535	1.290	1.380	100.51
	65	618	0.66	0.96	60.94	30.07	534	1.310	1.381	98.02
	67.5	618	0.65	0.94	50.19	30.07	534	1.290	1.347	98.06
	70	620	0.63	0.91	50.19	30.07	534	1.270	1.358	101.77
	72.5	619	0.66	0.94	60.90	30.07	534	1.300	1.360	94.81
	75	618	0.63	0.93	50.11	30.07	534	1.280	1.383	94.76
	77.5	618	0.64	0.93	50.51	30.07	534	1.290	1.393	98.97
	80	617	0.61	0.90	48.27	30.06	536	1.290	1.299	94.52
	82.5	617	0.62	0.90	48.27	30.07	536	1.210	1.299	100.08
	85	617	0.64	0.93	50.47	30.07	536	1.310	1.374	100.05
	87.5	617	0.64	0.93	50.47	30.07	536	1.280	1.342	98.82
	90	618	0.62	0.92	50.43	30.07	536	1.250	1.321	98.54
Traverse 4	92.5	621	0.64	0.93	50.85	30.07	536	1.270	1.331	97.80
	95	621	0.65	0.95	60.90	30.07	536	1.300	1.363	98.10
	97.5	618	0.65	0.90	48.78	30.07	536	1.240	1.298	98.76
	100	619	0.62	0.94	51.07	30.07	536	1.300	1.361	98.33
	102.5	622	0.66	0.94	60.93	30.07	537	1.300	1.329	97.82
	105	621	0.64	0.93	48.78	30.07	537	1.270	1.287	95.89
	107.5	619	0.62	0.90	50.74	30.07	537	1.300	1.290	100.43
	110	618	0.65	0.95	51.29	30.07	537	1.330	1.391	97.74
	112.5	618	0.66	0.96	60.34	30.07	537	1.290	1.338	95.30
	115	614	0.64	0.93	50.34	30.07	537	1.260	1.318	100.18
	117.5	614	0.64	0.94	50.34	30.07	537	1.260	1.318	100.18
	120	615	0.65	0.95	50.78	30.07	537	1.320	1.381	Average
Total	120	Average 616	Average 0.64	Average 0.92	Average 50.35	Average 30.07	Average 531	Total 60.670	Total 63.897	Average 97.91

Combustion Gas Data for: Northern Pulp

Client: Northern Pulp
Job Number: 121511289

Plant: Pictou
Location: Recovery Boiler
Test: PM-1
Date: 18-Aug-14
Personnel: T B/FS

Test Start: 12:15 PM
Test Finish: 12:45 PM

Time (min)	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
0	5.90	11.20	2465	15	63
5	5.70	11.28	1139	17	68
10	5.19	11.00	1638	16	54
15	5.90	11.16	1271	24	50
20	5.60	10.80	1313	18	48
25	5.56	10.79	1310	21	50
30	5.50	10.90	1200	21	51
Average:	5.1	11.0	1470	19	62

Raw Data For Northern Pulp Summer Source Testing
Test #2

Client: Northern Pulp
Job Number: 121811 gm

Plant: Pulp
Location: Recovery Bay
Test: PM₁₀
Date: 15-Aug-14
Personnel: JRU/PS
Test Start: 9:40 PM
Test Finish: 5:14 PM

Parameters
Barometric Pressure, Pbar (in. Hg)
Stack Bottle Pressure, Pstck (in. H₂O)
Ambient Temp, (°F)
H₂O Volume Collected, Vw (mL)
Total # Sampling Points
Sampling Time per Point, (min)
Reading Time Every ___ min
Regulatory Agency

Transverse Point	Time (min)	Stack Gas Temp, T _s (°F)	Stack Gas P (in. H ₂ O)	CO ₂ (%)	CO (%)	NO _x (ppm)	SO ₂ (ppm)	Gas Meter Volume (cu. ft.)	Gas Meter Temp Inlet (°F)	Gas Meter Temp Outlet (°F)	Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)	Total Weight Gain (g)	Moisture Volume (mL)
Transverse 1	2.5	157	0.0	0.0	0.0	0.0	0.0	230.90	73	73	1	100 mL H ₂ O	918.2	482.6	298.7	600.4	128
	5	157	0.0	0.0	0.0	0.0	0.0	232.56	73	73	2	100 mL H ₂ O	918.2	482.6	298.7	600.4	103.77
	7.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73	3	Blank	918.2	482.6	298.7	600.4	3
	10	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73	4	200g Silica Gel	918.2	482.6	298.7	600.4	0.233
	12.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	0.031
	15	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	1.04
	17.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	20	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	22.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	25	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
Transverse 2	27.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	30	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	32.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	35	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	37.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	40	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	42.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	45	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	47.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	50	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
Transverse 3	52.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	55	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	57.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	60	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	62.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	65	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	67.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	70	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	72.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	75	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
Transverse 4	77.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	80	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	82.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	85	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	87.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	90	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	92.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	95	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	97.5	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	
	100	157	0.0	0.0	0.0	0.0	0.0	231.08	73	73			918.2	482.6	298.7	600.4	

Transverse Point	Time (min)	Stack Gas Temp., T _s (°F)	S-type Pilot, inches P (in. H ₂ O)	Oxides, inches H (in. H ₂ O)	Stack Gas Velocity, U _s (ft/s)	Master Pressure, P _m (in. Hg)	Avg. Temp., T _m (°F)	Gas Meter Volume, V _m (cu. ft.)	Vol. @ Red., V _{red} (cu. ft.)	Isokinetic (%)
Transverse 1	1-1	517	0.61	0.80	49.20	30.21	536	1,280	1,349	102.55
	5	517	0.64	0.84	50.40	30.21	537	1,250	1,314	97.53
	1-3	516	0.82	0.90	49.50	30.21	536	1,180	1,254	94.17
	1-5	518	0.80	0.87	50.64	30.21	535	1,230	1,298	103.46
	1-7	517	0.64	0.83	50.44	30.21	535	1,270	1,303	103.46
	1-9	517	0.80	0.97	48.80	30.21	536	1,210	1,277	96.51
	2-1	517	0.63	0.82	50.00	30.21	535	1,170	1,244	94.82
	2-3	516	0.61	0.88	50.00	30.21	535	1,270	1,340	100.25
	2-5	515	0.81	0.96	49.18	30.21	535	1,240	1,308	99.20
	2-7	517	0.60	0.87	49.12	30.21	536	1,220	1,285	97.85
Transverse 2	2-1	518	0.60	0.87	48.80	30.21	535	1,220	1,285	97.85
	2-3	517	0.82	0.90	48.64	30.21	536	1,210	1,274	97.67
	2-5	518	0.81	0.89	48.16	30.21	535	1,250	1,316	99.35
	2-7	517	0.68	0.86	47.98	30.21	535	1,230	1,298	98.48
	2-9	514	0.61	0.90	49.05	30.21	535	1,230	1,298	98.48
	3-1	517	0.68	0.86	48.36	30.21	537	1,200	1,268	96.67
	3-3	517	0.60	0.85	48.36	30.21	537	1,200	1,260	95.67
	3-5	518	0.60	0.73	49.80	30.21	535	1,140	1,203	92.97
	3-7	517	0.83	0.87	49.80	30.21	535	1,180	1,222	102.72
	3-9	520	0.80	0.87	49.80	30.21	535	1,180	1,222	102.72
Transverse 3	3-1	517	0.80	0.87	49.80	30.21	535	1,180	1,222	102.72
	3-3	517	0.80	0.87	49.80	30.21	535	1,180	1,222	102.72
	3-5	516	0.81	0.86	49.24	30.21	535	1,170	1,244	94.53
	3-7	520	0.82	0.90	48.72	30.21	535	1,250	1,328	101.05
	3-9	519	0.64	0.90	50.48	30.21	537	1,250	1,329	101.05
	4-1	517	0.87	0.93	51.57	30.21	535	1,250	1,316	96.03
	4-3	518	0.64	0.84	50.48	30.21	535	1,300	1,371	98.43
	4-5	519	0.68	0.99	52.53	30.21	535	1,240	1,307	97.18
	4-7	519	0.70	1.00	52.70	30.21	535	1,300	1,371	98.65
	4-9	520	0.60	0.99	52.08	30.21	536	1,310	1,378	99.00
Transverse 4	4-1	519	0.67	0.87	50.87	30.21	537	1,290	1,357	97.99
	4-3	519	0.60	0.84	48.88	30.21	537	1,290	1,358	93.88
	4-5	518	0.60	0.87	48.84	30.21	537	1,290	1,358	93.88
	4-7	518	0.63	0.82	48.96	30.21	537	1,200	1,268	92.72
	4-9	518	0.62	0.91	48.64	30.21	537	1,150	1,208	92.72
	5-1	518	0.61	0.88	48.28	30.21	537	1,230	1,292	96.56
	5-3	518	0.81	0.89	48.34	30.21	535	1,300	1,364	102.94
	5-5	518	0.81	0.89	48.28	30.21	537	1,230	1,290	96.27
	5-7	518	0.82	0.91	48.64	30.21	537	1,250	1,292	96.28
	5-9	519	0.83	0.91	48.64	30.21	537	1,260	1,313	98.66
Transverse 5	5-1	519	0.83	0.91	48.64	30.21	537	1,260	1,313	98.66
	5-3	519	0.83	0.91	48.64	30.21	537	1,260	1,313	98.66
	5-5	519	0.83	0.91	48.64	30.21	537	1,260	1,313	98.66
	5-7	519	0.83	0.91	48.64	30.21	537	1,260	1,313	98.66
	5-9	519	0.83	0.91	48.64	30.21	537	1,260	1,313	98.66
	6-1	519	0.83	0.91	48.64	30.21	537	1,260	1,313	98.66
	6-3	519	0.83	0.91	48.64	30.21	537	1,260	1,313	98.66
	6-5	519	0.83	0.91	48.64	30.21	537	1,260	1,313	98.66
	6-7	519	0.83	0.91	48.64	30.21	537	1,260	1,313	98.66
	6-9	519	0.83	0.91	48.64	30.21	537	1,260	1,313	98.66
Total	120	Average 518	Average 0.82	Average 0.90	Average 49.52	Average 30.21	Average 536	Total 59,450	Total 62,965	Average 98.59

Combustion Gas Data for: Northern Pulp

Client: Northern Pulp
Job Number: 121511208

Plant: Pictou
Location: Recovery Boiler
Test: PM-2
Date: 18-Aug-14
Personnel: TBM/FS

Test Start: 4:30 PM
Test Finish: 5:00 PM

Time (min)	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	NO _x (ppm)
0	4.44	12.28	128	50	86
5	4.69	12.10	148	38	96
10	4.70	12.16	118	57	86
15	4.40	12.20	192	61	88
20	4.76	12.10	177	83	85
25	4.80	12.28	130	87	85
30	4.36	12.10	159	85	86
Average:	4.50	12.14	131	60	88

Calculations for Northern Pulp Wet Air Emissions Testing

Client: Northern Pulp
Job Number: 12181700
Plant: Pulp
Location: Recovery Boiler
Test: PM-3
Date: 20-Aug-14
Parameter: Emissions

Calculated Parameters

Stack Gas Pressure, P_g (kPa)
Stack Gas Molecular Weight, Dry Basis, M_d (lb/lbmole)
Volume of Water Vapor Collected, V_w (cc/L)
Stack Gas Molecular Weight, Wet Basis, M_w (lb/lbmole)
Stack Gas Molecular Weight, Wet Basis, M_w (lb/lbmole)

Isokinetic Checks

Check average Within Criteria

Transverse	Transverse Point	Time (min)	Stack Gas Temp, T _g (°F)	g-Type Pitot, delta P (in. H ₂ O)	Orifice delta H (in. H ₂ O)	Stack Gas Velocity, U _g (ft/s)	Meter Press., P _m (in. Hg)	Avg. Temp, T _m (°F)	Gas Meter Volume, V _m (cu. ft.)	Vol. @ Ref. Press. (cu. ft.)	Isokinetic %
Transverse 1	1-1	2.5	619	0.65	0.93	50.97	30.07	544	1.260	1.260	97.90
	1-2	7.5	620	0.64	0.92	50.82	30.07	545	1.260	1.260	98.30
	1-3	10	618	0.66	0.94	50.83	30.07	546	1.260	1.260	98.31
	1-4	12.5	619	0.68	0.95	51.32	30.07	548	1.270	1.270	97.58
	1-5	15	618	0.61	0.88	49.38	30.08	546	1.220	1.264	97.48
	1-6	17.5	620	0.63	0.94	50.87	30.07	547	1.280	1.264	98.77
	1-7	20	619	0.67	0.91	50.22	30.07	548	1.240	1.271	97.31
	1-8	22.5	618	0.60	0.89	49.32	30.07	548	1.220	1.261	97.21
	1-9	25	619	0.60	0.87	48.85	30.07	548	1.220	1.258	98.44
	1-10	27.5	618	0.64	0.93	50.84	30.08	548	1.280	1.249	97.85
Transverse 2	2-1	30	618	0.62	0.90	49.74	30.06	549	1.280	1.270	100.07
	2-2	32.5	619	0.64	0.93	50.83	30.07	549	1.280	1.270	98.72
	2-3	35	618	0.66	0.95	51.32	30.07	549	1.280	1.277	98.99
	2-4	37.5	617	0.62	0.87	48.83	30.06	549	1.270	1.277	98.07
	2-5	40	618	0.66	0.95	51.32	30.07	549	1.270	1.266	97.44
	2-6	42.5	617	0.62	0.90	48.74	30.07	549	1.270	1.266	97.41
	2-7	45	618	0.63	0.92	50.15	30.07	549	1.270	1.262	98.57
	2-8	47.5	617	0.65	0.95	51.32	30.07	549	1.270	1.262	97.25
	2-9	50	618	0.62	0.91	49.74	30.07	549	1.260	1.262	98.44
	2-10	52.5	619	0.64	0.94	50.84	30.07	549	1.260	1.260	98.34
Transverse 3	3-1	55	618	0.63	0.92	50.16	30.07	549	1.260	1.270	97.14
	3-2	57.5	619	0.65	0.95	51.32	30.07	549	1.260	1.270	98.29
	3-3	60	618	0.61	0.89	48.38	30.07	549	1.260	1.270	97.79
	3-4	62.5	619	0.64	0.93	50.83	30.07	549	1.260	1.269	98.31
	3-5	65	620	0.66	0.95	51.32	30.07	549	1.260	1.269	98.29
	3-6	67.5	618	0.63	0.92	50.16	30.07	549	1.260	1.269	98.31
	3-7	70	619	0.65	0.95	51.32	30.07	549	1.260	1.269	98.29
	3-8	72.5	620	0.64	0.93	50.83	30.07	549	1.260	1.269	98.29
	3-9	75	618	0.62	0.90	48.38	30.07	549	1.260	1.269	98.29
	3-10	77.5	619	0.64	0.93	50.83	30.07	549	1.260	1.269	98.29
Transverse 4	4-1	80	619	0.65	0.95	51.32	30.07	549	1.260	1.269	98.29
	4-2	82.5	618	0.63	0.92	50.16	30.07	549	1.260	1.269	98.29
	4-3	85	620	0.66	0.95	51.32	30.07	549	1.260	1.269	98.29
	4-4	87.5	618	0.64	0.93	50.83	30.07	549	1.260	1.269	98.29
	4-5	90	619	0.65	0.95	51.32	30.07	549	1.260	1.269	98.29
	4-6	92.5	618	0.63	0.92	50.16	30.07	549	1.260	1.269	98.29
	4-7	95	620	0.66	0.95	51.32	30.07	549	1.260	1.269	98.29
	4-8	97.5	618	0.64	0.93	50.83	30.07	549	1.260	1.269	98.29
	4-9	100	619	0.65	0.95	51.32	30.07	549	1.260	1.269	98.29
	4-10	102.5	618	0.63	0.92	50.16	30.07	549	1.260	1.269	98.29
Total		120	Average	0.64	0.92	50.38	Average	542	Total	61.314	Average
									60.270		97.23

Combustion Gas Data for: Northern Pulp Summer Source Testing

Client: Northern Pulp
 Job Number: 121511259
 Plant: Piclou
 Location: Recovery Boiler
 Test: PM-3
 Date: 20-Aug-14
 Personnel: TBH/FS
 Test Start: 1:18 AM
 Test Finish: 1:40 AM

Time (min)	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
0	5.50	13.40	75	5	34
5	5.50	13.40	118	5	34
10	5.20	13.80	83	7	34
15	5.30	13.70	194	7	35
20	5.60	13.50	318	8	35
25	5.70	13.50	440	8	35
30	5.50	13.40	285	8	35
Average:	5.46	13.48	212	7	35

DATA ENTRY
 Northern Pulp
 Recovery Boiler
 Operating Conditions: Normal
 Emission Control Equipment: Multicyclones
 Stack Diameter: 3.5 m

Reference Temperature, Tref (F): 75
 (K): 298
 Reference Pressure, Pref (in.Hg): 30.0
 (Bar): 1.0

Parameter	Symbol	Units	Test 1	Test 2	Test 3	Average
Test ID						
Date						
Start Time			PM-1	PM-2	PM-3	
End Time			19-Aug-14	19-Aug-14	20-Aug-14	
Total Sampling Time			11:10 AM	3:00 PM	1:10 PM	n/a
			1:30 PM	5:15 PM	3:20 PM	n/a
		min	120	120	120	120
Stack Diameter	D	in.				
Average Stack Gas Temperature	Ts	F	138	138	138	138
Average Dry Gas Meter Temperature	Tm	F	158	158	158	158
Barometric Pressure	Pbar	in.Hg	71	75	82	80
Stack Static Pressure	Pstatic	in.H2O	30.0	30.1	30.0	30.0
Average Pressure Drop (Head)	dP	in.H2O	1.10	1.10	1.10	1.10
Average delta H Orifice	dH	in.H2O	0.84	0.82	0.64	0.63
Average Meter Temperature	Tm	F	0.92	0.90	0.92	0.91
Gas Sample Volume	Vm	cu.ft	71	78	82	80
Average Isokinetics	I	%	80.57	88.45	80.27	80.10
			97.9	98.8	97.2	97.9
Nozzle Diameter	Dn	in.				
PIOT Coefficient	Cp	-	0.233	0.233	0.233	0.233
Gamma, meter constant	y	-	0.838	0.838	0.838	0.838
			1.040	1.040	1.040	1.040
Reference Temperature	Tref	R				
Reference Pressure	Pref	in.Hg	537	537	537	537
			29.92	29.92	29.92	29.92
Stack Gas Oxygen Content	Co2	%				
Stack Gas Carbon Dioxide Content	Cco2	%	6.1	4.5	5.5	5.4
Stack Gas Nitrogen Content	Cn2	%	11.0	12.1	13.6	12.2
Stack Gas Sulphur Dioxide Content	Cso2	ppm	82.9	83.4	81.1	82.4
Stack Gas Nitrogen Oxides Content	Cnox	ppm	19	80	7	29
Stack Gas Carbon Monoxide Content	Cco	ppm	52	86	35	51
			1478	131	212	807
Volume of Water Collected	Vw	mL				
Particulate Collected from Filter	-	mg	582	800	822	801
Particulate Collected from Probe Wash	-	mg	828	885	1244	865
Particulate Collected from Impinger Wash	-	mg	423	378	758	519
Total Particulate Collected (excluding Impingers)	Σp	mg	5.23	3.44	3.72	4.13
			1,249	1,282	2,001	1,504

Legend: F - degrees Fahrenheit
 K - degrees Kelvin
 Bar - bars
 in.Hg - inches of mercury
 in. - inches

in.H2O - inches of water
 cu.ft - cubic feet
 R - degrees Rankin
 NOx - as NO2

CALCULATIONS
 Northern Pulp
 Recovery Boiler
 Operating Conditions: Normal
 Emission Control Equipment: Multicyclones
 Stack Diameter: 3.5 m

Variable	Symbol	Units	Calculation	Test 1	Test 2	Test 3	Average
Stack Area	As	sq.ft sq.m	$A_s = \pi \times (D/12)^2 \times 4$ $A_s \text{ (sq.m)} = A_s \text{ (sq.ft)} \times 0.0929$	103.87 9.65	103.87 9.65	103.87 9.65	103.87 9.65
Barometric Pressure	Pbar	hPa	$P_{bar} \text{ (hPa)} = P_{bar} \text{ (hPa)} \times 1.325$	101.8	102.1	101.8	101.7
Stack Static Pressure	Pstatic	hPa	$P_{static} \text{ (hPa)} = P_{static} \text{ (hPa)} \times 0.248$	0.27	0.27	0.27	0.27
Avg. Stack Temperature	Ts	R	$T_s \text{ (R)} = T_s \text{ (F)} + 459$	618	618	618	618
Avg. Meter Temperature	Tm	R	$T_m \text{ (R)} = T_m \text{ (F)} + 459$	531	536	552	540
Nozzle Diameter	Dn	mm	$D_n \text{ (mm)} = D_n \text{ (in.)} \times 25.4$	8	8	8	8
Gas Meter Pressure	Pm	in.Hg mm.Hg	$P_m = P_{bar} + (P_n / 13.6)$	30.1	30.2	30.1	30.1
Sample Volume at Ref Cond	Vms	cu.ft cu.m	$V_{ms} = T_{ref} P_{ref} / (P_m \times T_m) \times V_m$	94.0	82.8	81.3	82.8
Volume of Water Vapour	Vws	cu.ft	$V_{ws} = 0.0458 \times V_m$	1.81	1.77	1.74	1.77
Water Fraction	Wws		$W_{ws} = V_{ws} / (V_{ws} + V_{ms})$	27.9	28.8	28.8	28.8
Molecular Weight, Dry	Md	lb/lb-mol	$M_d = 0.44 \text{ (CO}_2\text{)} + 0.32 \text{ (CO)} + 0.28 \text{ (O}_2\text{)}$	30.0	30.1	30.4	30.2
Molecular Weight, Wet	Mw	lb/lb-mol	$M_w = M_d (1 - W_{ws}) + (18 \times W_{ws})$	28.4	28.3	28.3	28.3
Stack Pressure	Ps	in.Hg	$P_s = P_{bar} + (P_{static} / 13.6)$	30.1	30.2	30.1	30.1
Stack Gas Velocity	Vs	ft/s m/s	$V_s = 44.72 \times C_p \times (P/P_{ref}) \times (T_{ref}/T_s) \times V_{ref}$	80.4	46.9	80.4	80.1
Actual Stack Gas Flow Rate	Q	acfm	$Q = 60 \times V_s \times A_s$	313,981	304,834	313,970	312,184
Dry Stack Gas Flow Rate	Qd	acfm Nm³/s	$Q_d = Q \times (1 - W_{ws}) \times (P_{ref}/P_s) \times (T_s/T_{ref})$ $Q_d \text{ (Nm³/s)} = 0.000472 \times Q \text{ (acfm)}$	181,101 80.2	185,573 87.8	184,353 87.0	187,009 86.8
Sulphur Dioxide - SO2	SO2	ppm	Measurement from Flue Gas Analyser	18.71	88.29	7.14	28.7
SO2 Measured Concentration	SO2	mg/ft³	$SO_2 \text{ (mg/ft³)} = SO_2 \text{ (ppm)} \times 2.83$	49.03	157.95	18.71	76.2
SO2 Emission Rate	ERSO2	g/s kg/hr	$ER_{SO_2} = SO_2 / 1000 \times Q_d$ $ER_{SO_2} \text{ (kg/hr)} = 2.8 \times ER_{SO_2} \text{ (g/s)}$	4.42 15.92	13.83 49.81	1.83 6.88	8.8 24
SO2 Concentration	SO2	mg/ft³	$SO_2 \text{ (11% O}_2\text{)} = SO_2 \text{ (mg/ft³)} \times (20.9 - 11) / (20.9 - CO_2)$	32.9	95.3	12.0	46.7
Corrected to 11% O2	SO2	mg/ft³	$SO_2 \text{ (3% O}_2\text{)} = SO_2 \text{ (mg/ft³)} \times (20.9 - 3) / (20.9 - CO_2)$	58	172	22	85
Corrected to 12% CO2	SO2	mg/ft³	$SO_2 \text{ (12% CO}_2\text{)} = SO_2 \text{ (mg/ft³)} \times (13/CO_2)$	53.7	158.1	16.7	75.5
Nitrogen Oxides - NOx	NOx	ppm	Measurement from Flue Gas Analyser	81.7	64.8	34.8	50.7
NOx Measured Concentration	NOx	mg/ft³	$NO_x \text{ (mg/ft³)} = NO_x \text{ (ppm)} \times 1.63$	97.3	123	68	95
NOx Emission Rate	ERNOx	g/s kg/hr	$ER_{NO_x} = NO_x / 1000 \times Q_d$ $ER_{NO_x} \text{ (kg/hr)} = 2.8 \times ER_{NO_x} \text{ (g/s)}$	9.78 21.6	10.81 38.9	5.71 20.5	11.42 30.4
NOx Concentration	NOx	mg/ft³	$NO_x \text{ (11% O}_2\text{)} = NO_x \text{ (mg/ft³)} \times (20.9 - 11) / (20.9 - CO_2)$	65.3	74.5	42.1	60.8
Corrected to 11% O2	NOx	mg/ft³	$NO_x \text{ (3% O}_2\text{)} = NO_x \text{ (mg/ft³)} \times (20.9 - 3) / (20.9 - CO_2)$	118	135	70	110
Corrected to 12% CO2	NOx	mg/ft³	$NO_x \text{ (12% CO}_2\text{)} = NO_x \text{ (mg/ft³)} \times (13/CO_2)$	109.8	122.0	88.4	95.8
Carbon Monoxide - CO	CO	ppm	Measurement from Flue Gas Analyser	1,478	131	212	607
CO Measured Concentration	CO	mg/ft³	$CO \text{ (mg/ft³)} = CO \text{ (ppm)} \times 1.146$	1,694	160	243	665
CO Emission Rate	ERCO	g/s kg/hr	$ER_{CO} = CO / 1000 \times Q_d$ $ER_{CO} \text{ (kg/hr)} = 2.8 \times ER_{CO} \text{ (g/s)}$	152.8 550	13.1 47	21.1 78	62.3 224
CO Concentration	CO	mg/ft³	$CO \text{ (11% O}_2\text{)} = CO \text{ (mg/ft³)} \times (20.9 - 11) / (20.9 - CO_2)$	1,138	90	150	481
Corrected to 11% O2	CO	mg/ft³	$CO \text{ (3% O}_2\text{)} = CO \text{ (mg/ft³)} \times (20.9 - 3) / (20.9 - CO_2)$	4,050	588	785	2,169
Corrected to 12% CO2	CO	mg/ft³	$CO \text{ (12% CO}_2\text{)} = CO \text{ (mg/ft³)} \times (13/CO_2)$	1,855	148	218	743
Particulate Concentration	Ca	mg/ft³	$C_a = M_p / V_{ms}$	889	712	1,182	651
Particulate Emission Rate	ERp	g/s kg/hr	$ER_p = C_a / 1000 \times Q_d$ $ER_p \text{ (kg/hr)} = 2.8 \times ER_p \text{ (g/s)}$	82.1 224	82.4 229	100.3 361	74.6 270
Particulate Concentration	Ca	mg/ft³	$Ca \text{ (11% O}_2\text{)} = Ca \times (20.9 - 11) / (20.9 - CO_2)$	482	430	739	544
Corrected to 11% O2	Ca	mg/ft³	$Ca \text{ (3% O}_2\text{)} = Ca \times (20.9 - 3) / (20.9 - CO_2)$	836	777	1,335	985
Corrected to 12% CO2	Ca	mg/ft³	$Ca \text{ (12% CO}_2\text{)} = Ca \times (13/CO_2)$	755	704	1,225	828

Legend: sq.ft - square feet
 sq.m - square metres
 ft - 1.143
 R - degrees Rankin

acfm - actual cubic feet per minute
 RRef - dry reference cubic feet per minute
 RRef - dry reference cubic metres per second
 ppm - parts per million
 cu.ft - cubic metres
 Ref Cond - reference temperature and pressure (25 C and 101.3 kPa)

in.Hg - inches of mercury
 cu.ft - cubic feet
 mg/ft³ - milligrams per dry reference cubic metre
 g/s - grams per second
 NOx - as NO2

OFFICIAL STACK TESTING RESULTS

Northern Pulp

Recovery Boiler

Operating Conditions: Normal

Emission Control Equipment: Multicyclones

Stack Diameter: 3.5 m

Parameter	Test 1	Test 2	Test 3	Average	NSENV Limits
Test ID	PM-1	PM-2	PM-3		
Test Date	19-Aug-14	19-Aug-14	20-Aug-14		
Stack Gas Temperature (C)	70	70	70	70	-
Moisture Content (%)	30.4	31.5	32.7	31.5	-
Velocity (m/s)	15.4	15.1	15.4	15.3	-
Volumetric Flow (Rcms)	90.2	87.6	87.0	88.3	-
Oxygen - O2 (%)	8.14	4.50	5.5	5.37	-
Carbon Dioxide - CO2 (%)	10.96	12.1	13.49	12.20	-
Sulphur Dioxide - SO2					
SO2 Measured Concentration (ppm)	18.7	60.3	7.14	28.7	-
Uncorrected at Ref Cond (mg/Rcm)	49.0	158	18.7	75.2	-
Emission Rate (kg/hr)	15.9	49.8	5.86	23.9	-
Nitrogen Oxides - NOx					
NOx Measured Concentration (ppm)	51.7	65.6	34.9	50.7	-
Uncorrected at Ref Cond (mg/Rcm)	97.3	123.4	65.6	95.4	-
Emission Rate (kg/hr)	31.6	38.9	20.5	30.4	-
Carbon Monoxide - CO					
CO Measured Concentration (ppm)	1,479	131	212	607	-
Uncorrected at Ref Cond (mg/Rcm)	1,694	150	243	895	-
Emission Rate (kg/hr)	550	47.2	76.0	224	-
Particulate Matter - PM					
Uncorrected at Ref Cond (mg/Rcm)	689	712	1,152	851	-
PM - Corrected to 11% O2 (mg/Rcm)	482	430	739	544	-
Particulate Emission Rate (kg/hr)	224	225	381	270	375

Legend: C - degrees Celsius
m/s - metres per second
Rcms - dry reference cubic metres per second
ppm - parts per million

Ref Cond - reference temperature and pressure (25 C and
mg/Rcm - milligrams per dry reference cubic metre
NOx - as NO2

Portugalia Reservoir, Sampling Cabin, Pinalo Wash, 1 Mile SW

Client: Northern Pip
 Facility: Pinalo
 Location: Recovery Boiler
 Job Number: 121511228

REPROCESS CATCH

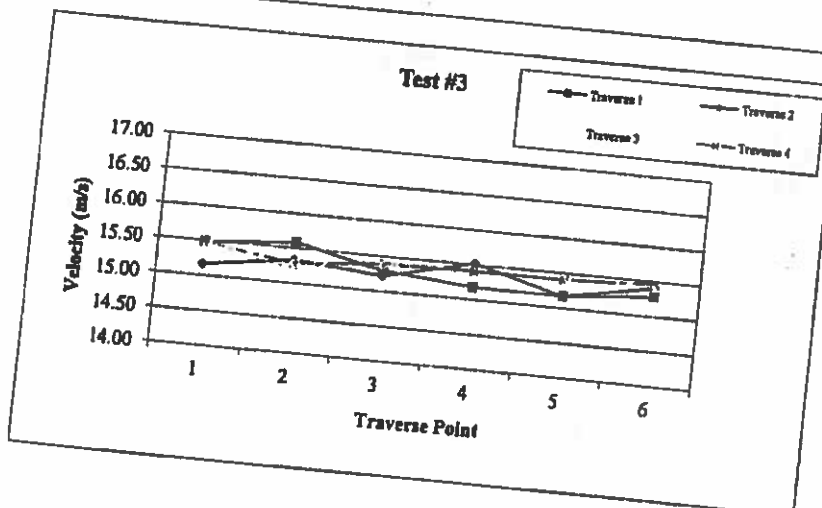
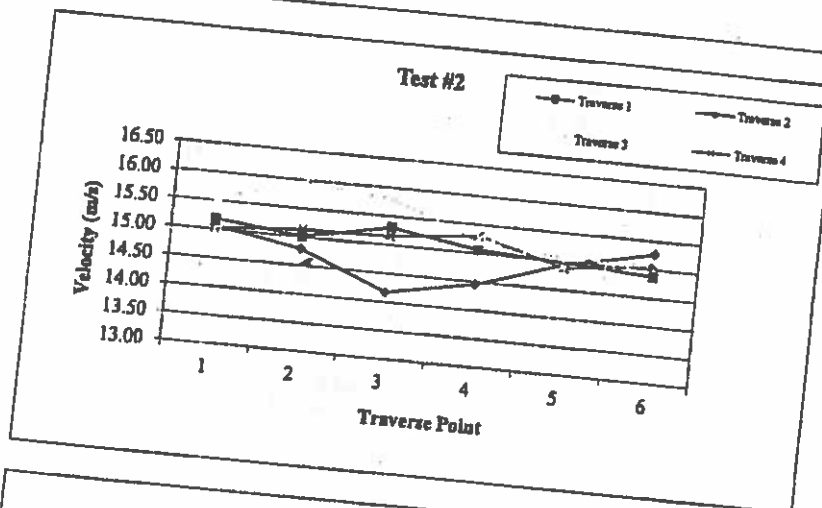
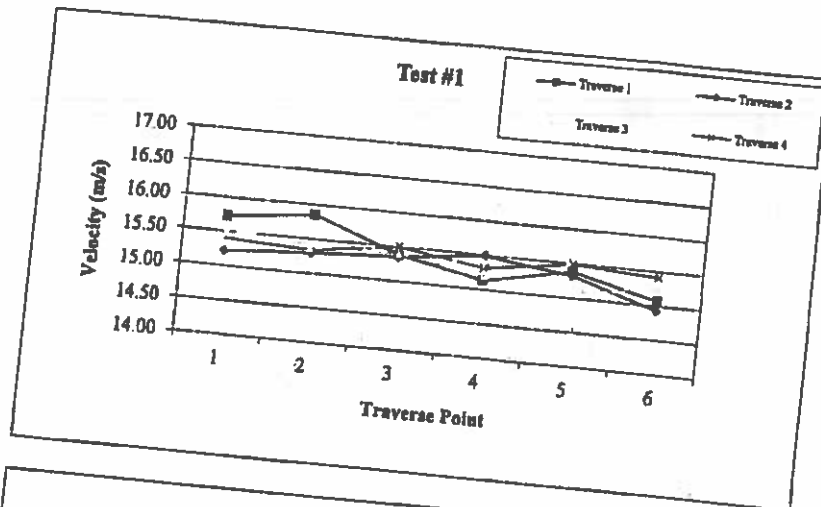
Container ID	Sample ID				Sample ID				Sample ID				Sample ID				Sample ID			
	Trail 1	Trail 2	Trail 3	Average	Trail 1	Trail 2	Trail 3	Average	Trail 1	Trail 2	Trail 3	Average	Trail 1	Trail 2	Trail 3	Average	Trail 1	Trail 2	Trail 3	Average
T1	114.7325	114.7323		114.7324	P6-1				1076.4	778.0	19.5	11.8	114.7971	114.7876		114.7977	114.7971	114.7876		114.7977
C3	113.2769	113.2764		113.2767	P6-2				1058.7	777.8	16.5	18.4	113.2801	113.2802		113.2802	113.2801	113.2802		113.2802
A3	110.3980	110.3987		110.3980	P6-3				1072.5	780.9	23.1	23.1	110.3177	110.3178		110.3178	110.3177	110.3178		110.3178
S6	108.0487	108.0482		108.0485	W9				632.7	777.4	279.2	279.2	108.0492	108.0488		108.0484	108.0492	108.0488		108.0492
																				0.0000
																				0.0000

Container ID	Sample ID				Sample ID				Sample ID				Sample ID				Sample ID			
	Trail 1	Trail 2	Trail 3	Average	Trail 1	Trail 2	Trail 3	Average	Trail 1	Trail 2	Trail 3	Average	Trail 1	Trail 2	Trail 3	Average	Trail 1	Trail 2	Trail 3	Average
L1	109.1345	109.1345		109.1345	P6-1				479.3	308.2	19.5	23.1	108.8172	108.8173		108.8173	108.8172	108.8173		108.8173
V1	111.8257	111.8257		111.8257	P6-2				493.1	308.5	174.8	31.6	113.2873	113.2873		113.2873	113.2873	113.2873		113.2873
O1	111.9756	111.9756		111.9756	P6-3				777.8	283.2	31.6	31.6	112.7288	112.7288		112.7288	112.7288	112.7288		112.7288
V7	109.1243	109.1244		109.1244	A8				477.7	778.7	101.0	101.0	101.1741	101.1741		101.1741	101.1741	101.1741		101.1741
																				0.0000
																				0.0000

REPROCESS CATCH

Filter ID	Sample ID				Sample ID				Sample ID				Sample ID				Sample ID			
	Trail 1	Trail 2	Trail 3	Average	Trail 1	Trail 2	Trail 3	Average	Trail 1	Trail 2	Trail 3	Average	Trail 1	Trail 2	Trail 3	Average	Trail 1	Trail 2	Trail 3	Average
0123-14	0.3168	0.3168		0.3168	P6-1				1.1570	1.1577	1.1577	1.1577	1.1570	1.1577		1.1577	1.1570	1.1577		1.1577
0126-17	0.3051	0.3050		0.3051	P6-2				1.1895	1.1896	1.1896	1.1896	1.1895	1.1896		1.1896	1.1895	1.1896		1.1896
0316-20	0.3315	0.3317		0.3316	P6-3				1.1990	1.1990	1.1990	1.1990	1.1990	1.1990		1.1990	1.1990	1.1990		1.1990

Stack Gas Velocity Profiles
Recovery Boiler



Raw Data for Northern Pulp Summer Source Testing

Test #1 Client: Northern Pulp
Job Number: 21081524

Plant: Pulp
Location: Unloading Tank
Test: PM₁₀
Date: 7/9 Aug-11
Personnel: C/M/M/N
Test Start: 1:50 PM
Test Finish: 4:00 PM

Parameters
Barometric Pressure, Pbar (in. Hg)
Stack Static Pressure, Pstatic (in. H2O)
Ambient Temp, (°F)
H2O Volume Collected, Vol (mL)
Total # Sampling Points
Sampling Time per Point, (min)
Readings Taken Every — min
Regulatory Agency

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H2O	1715.0	152.5	379.7
2	100 mL H2O	1422.6	899.2	523.4
3	Blank	793.1	821.4	97.7
4	200g Silica Gel	1013.1	1007.0	6.1
		Total Weight Gain (g)		808.9
		Moisture Volume (mL)		808.9

Stack Diameter, (in.)
Stack Area, (sq. ft.)
Probe Length, (ft.)
Probe Diameter, (in.)
Flow Calibration, (CFM)
Correction, enter constant
Port Height, (ft.)

48
12.57
5
0.311
0.856
1.091
6

C2-109

Particulates Collected from Filter (mg):
Particulates Collected from Probe Wash (mg):
Particulates Collected from Impinger Wash (mg):
Total Particulates Collected (mg):

600.8
234.7
64.2
970.7

O2 (%)
CO2 (%)
NO2 (%)
CO (ppm)
H2S (ppm)
SO2 (ppm)

30.00
-0.10
84
888.9
27
4
2.5
N/A

Transverse Point	Time (min)	Stack Gas Temp, (°F)	B-type Phot cell P (in. H2O)	Orifice delta H (in. H2O)	Gas Meter Volume (cu. ft.)	Gas Meter Temp (°F)	Orifice	Inlet (°F)	Outlet (°F)	Gas Meter Temp (°F)	Inlet (°F)	Outlet (°F)
Transverse 1	1	316	0.94	0.71	21234.0	38	0.71	38	37	37	38	37
	2	314	0.12	0.40	31534.0	38	0.40	38	37	37	38	37
	3	312	0.15	0.33	31977.0	38	0.33	38	37	37	38	37
	4	319	0.21	0.16	31600.0	38	0.16	38	37	37	38	37
	5	317	0.27	0.41	31500.0	38	0.41	38	37	37	38	37
	6	315	0.16	0.39	31670.0	38	0.39	38	37	37	38	37
	7	317	0.21	0.44	31720.0	38	0.44	38	37	37	38	37
	8	318	0.19	0.43	31600.0	38	0.43	38	37	37	38	37
	9	315	0.17	0.19	31900.0	38	0.19	38	37	37	38	37
	10	311	0.17	0.17	31610.0	38	0.17	38	37	37	38	37
Transverse 2	1	314	0.13	0.25	31534.0	38	0.25	38	37	37	38	37
	2	312	0.14	0.21	31534.0	38	0.21	38	37	37	38	37
	3	314	0.18	0.19	31770.0	38	0.19	38	37	37	38	37
	4	316	0.16	0.35	31600.0	38	0.35	38	37	37	38	37
	5	317	0.17	0.37	31600.0	38	0.37	38	37	37	38	37
	6	315	0.17	0.39	31670.0	38	0.39	38	37	37	38	37
	7	317	0.17	0.37	31720.0	38	0.37	38	37	37	38	37
	8	318	0.17	0.37	31600.0	38	0.37	38	37	37	38	37
	9	315	0.17	0.19	31900.0	38	0.19	38	37	37	38	37
	10	311	0.17	0.17	31610.0	38	0.17	38	37	37	38	37

Calculations for Northern Pip Summer Source Testing Test #1

Client: Northern Pip
Job Number: 1291250
Phase: Field
Location: Drilling Tank
Test: PPA
Date: 20-Aug-14
Permitted: California

Calculated Parameters

Static Gas Pressure, Ps (in.Hg)
Static Gas Molecular Weight, Dry Basis, M_d (lb/lb-mole)
Volume of Water Vapor Collected, V_w (cu.ft)
Static Gas Molecular Weight, Wet Basis, M_w (lb/lb-mole)
Static Gas Molecular Weight, Wet Basis, M_w (lb/lb-mole)

Isokinetic Checks

Check average Within Criteria

Transverse Point	Time (min)	Static Gas Temp, T _s (°F)	Static Gas Velocity, V _s (ft/min)	Orifice Dia, H (in. H ₂ O)	Static Gas Velocity, V _s (ft/min)	Static Gas Pressure, P _s (in. H ₂ O)	Avg. Temp, T _s (°F)	Gas Meter, V _m (cu. ft)	Vel. @ Ref., V _r (cu. ft)	Isokinetics (%)
Transverse 1	1	2.5	0.10	0.21	22.24	30.02	54.8	0.000	0.040	102.24
	2	5	0.10	0.40	30.58	30.02	54.8	0.000	0.044	102.24
	3	7.5	0.10	0.31	27.32	30.02	54.8	0.000	0.044	102.24
	4	12.5	0.21	0.44	32.50	30.02	54.8	0.000	0.044	102.24
	5	17.5	0.10	0.38	29.87	30.02	54.8	0.000	0.044	102.24
	6	22.5	0.21	0.44	32.55	30.02	54.8	0.000	0.044	102.24
	7	27.5	0.10	0.40	30.70	30.02	54.8	0.000	0.044	102.24
	8	32.5	0.10	0.38	29.89	30.02	54.8	0.000	0.044	102.24
	9	37.5	0.10	0.32	27.22	30.02	54.8	0.000	0.044	102.24
	10	42.5	0.10	0.28	24.96	30.02	54.8	0.000	0.044	102.24
Transverse 2	1	47.5	0.10	0.37	28.65	30.02	54.8	0.000	0.044	102.24
	2	52.5	0.10	0.40	30.31	30.02	54.8	0.000	0.044	102.24
	3	57.5	0.10	0.38	28.41	30.02	54.8	0.000	0.044	102.24
	4	62.5	0.10	0.27	25.32	30.02	54.8	0.000	0.044	102.24
	5	67.5	0.10	0.31	26.99	30.02	54.8	0.000	0.044	102.24
	6	72.5	0.10	0.35	27.71	30.02	54.8	0.000	0.044	102.24
	7	77.5	0.10	0.30	26.44	30.02	54.8	0.000	0.044	102.24
	8	82.5	0.10	0.37	28.76	30.02	54.8	0.000	0.044	102.24
	9	87.5	0.10	0.37	28.74	30.02	54.8	0.000	0.044	102.24
	10	92.5	0.10	0.37	28.76	30.02	54.8	0.000	0.044	102.24
Total		100	Average	0.38	28.51	Average	54.8	-Total	Total	Average
								37.100	35.797	102.16

Combustion Gas Data for: Northern Pulp

Client: Northern Pulp
Job Number: 12151289

Plant: Pictou
Location: Dissolving Tank
Test: PM-1
Date: 20-Aug-14
Personnel: CAMMM

Test Start: 3:49 PM
Test Finish: 3:50 PM

Time (min)	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
0	20.98	0.00	0.0	0.0	0
5	20.98	0.00	0.0	0.0	0
10	21.00	0.00	0.0	0.0	0
15	20.90	0.00	0.0	0.0	0
20	20.80	0.00	0.0	0.0	0
25	20.88	0.00	0.0	0.0	0
30	20.90	0.00	0.0	0.0	0
Average:	20.91	0.00	0.0	0	0

Raw Data for Northern Pip Summer Source Testing

Test #2

Client: Northern Pip
Job Number: 121612208

Plastic Pallet
Location: Delying Tank
Date: 23-Aug-11
Personnel: CMM/ML
Test Start: 8:30 AM
Test Finish: 10:30 AM

Parameters
Barometric Pressure, Pbar (in. Hg)
Static Static Pressure, Pstatic (in. H2O)
Ambient Temp, (°F)
H2O Volume Collected, Vw (mL)
Total P Sampling Points
Sampling Time per Point, (min)
Sampling Tube Entry — in/in
Regulatory Agency

Impinger No.	Impinger Comments	Fired Weight (g)	True Weight (g)	Weight of Moisture (g)
1	120 mL H2O	1754.4	1384.7	369.7
2	120 mL H2O	1653.4	717.5	516.1
3	Blank	791.8	822.4	79.2
4	200g silica Gel	1022.7	1016.8	7.7
Total Weight Gain (g)				801.7
Moisture Volume (mL)				801.7

Stack Diameter, (in.)
Stack Area, (sq. in.)
Probe Length, (ft.)
Nozzle Diameter, (in.)
Probe Condition, (C/F)
Oxygen, probe comment
Port length (in.)

CO₂ (%)
CO₂ (ppm)
NO₂ (%)
CO (ppm)
NOx (ppm)
SO₂ (ppm)

Gas Meter
Volume (cc. H₂)

S-type Flow
cells P
(in. H₂O)

Stack Gas
Temp, Tg
(°F)

Time
(min)

Transverse
Point

Transverse 1

Gas Meter Temp
Inlet (°F)

Gas Meter
Volume (cc. H₂)

S-type Flow
cells P
(in. H₂O)

Stack Gas
Temp, Tg
(°F)

Time
(min)

Transverse
Point

Transverse 2

Gas Meter Temp
Inlet (°F)

Gas Meter
Volume (cc. H₂)

S-type Flow
cells P
(in. H₂O)

Stack Gas
Temp, Tg
(°F)

Time
(min)

Transverse
Point

Client: Northern Pipe
Job Number: 121611208
Plant: Puton
Location: Dredging Test
Test Pkg: 2
Date: 21-Aug-14
Personnel: CASHMAN

Stock Gas Propanone, Pz (in Hg)
Stock Gas Molecular Weight, Dry Basis, Mol (N₂O=moles)
Volume of Water Vapour Collected, Vol (cu ft)
Stock Gas Moisture Content (% as decal)
Stock Gas Molecular Weight, Dry Basis, Mol (N₂O=moles)

Check average:

Traverse Point	Time (min)	Stack Gas Temp., T _s (°F)	S-Oxide Pres., delta P (in. H ₂ O)	Orifice delta H (in. H ₂ O)	Stack Gas Velocity, V _s (ft/s)	Moist. Pres., P _m (in. Hg)	Avg. Temp., T _m (°F)	Gas Meter Vol. (cu. ft.)	Vol. @ Ref., V _m (cu. ft.)	Vol. @ Ref., V _m (cu. ft.)	Leakhead, L (%)
Traverse 1	2.5	844	0.18	0.45	27.54	30.03	550	1.910	0.983	110.18	
	5	847	0.13	0.28	24.70	30.02	541	0.980	0.944	104.38	
	7.5	844	0.20	0.32	30.04	30.04	551	1.140	1.120	104.35	
	10	864	0.19	0.32	30.03	30.04	551	1.140	1.120	104.35	
	12.5	864	0.19	0.32	30.03	30.04	552	1.200	1.009	109.85	
	15	853	0.17	0.47	28.40	30.03	553	1.000	1.037	110.51	
	17.5	871	0.18	0.44	28.42	30.03	553	1.020	0.977	108.70	
	20	874	0.18	0.48	28.90	30.04	553	1.020	0.977	108.70	
	22.5	875	0.21	0.38	32.04	30.04	564	1.000	0.877	107.00	
	25	875	0.18	0.31	30.50	30.04	564	1.170	1.142	119.27	
Traverse 2	27.5	867	0.18	0.48	29.99	30.04	554	0.950	0.827	98.49	
	30	873	0.18	0.48	27.85	30.03	555	0.960	0.855	108.81	
	32.5	863	0.15	0.48	29.85	30.04	545	0.970	1.042	111.89	
	35	882	0.13	0.41	28.98	30.03	535	0.970	0.940	110.07	
	37.5	898	0.10	0.30	34.80	30.02	549	0.750	0.790	90.34	
	40	861	0.13	0.30	30.81	30.02	549	0.890	0.871	95.17	
	42.5	871	0.13	0.26	34.17	30.02	568	0.870	0.851	81.37	
	45	871	0.19	0.26	30.10	30.04	558	0.780	0.758	86.44	
	47.5	885	0.18	0.48	28.47	30.04	557	1.050	1.020	108.89	
	50	870	0.18	0.48	29.58	30.04	557	1.050	1.010	108.97	
Traverse 3	52.5	857	0.14	0.39	25.83	30.03	557	0.950	0.823	110.78	
	55	863	0.15	0.41	29.88	30.03	557	0.920	0.860	105.96	
	57.5	858	0.10	0.28	31.86	30.04	559	0.700	0.670	86.51	
	60	860	0.18	0.50	28.34	30.04	549	1.030	0.996	102.93	
	62.5	863	0.19	0.52	30.34	30.04	549	1.030	1.027	103.74	
	65	873	0.20	0.34	31.25	30.04	559	1.100	1.045	108.38	
	67.5	858	0.18	0.39	28.34	30.04	559	1.090	1.045	108.38	
	70	863	0.18	0.49	29.42	30.03	559	1.090	1.029	110.78	
	72.5	890	0.17	0.47	29.69	30.03	560	1.040	1.004	108.13	
	75	889	0.17	0.47	28.72	30.03	560	1.040	1.004	108.13	
Traverse 4	77.5	863	0.17	0.47	28.60	30.03	560	1.040	1.004	108.13	
	80	890	0.14	0.37	25.89	30.03	560	0.940	0.904	108.88	
	82.5	885	0.15	0.41	28.89	30.04	560	0.940	0.907	108.18	
	85	868	0.16	0.49	28.89	30.03	560	0.940	0.898	108.18	
	87.5	860	0.12	0.34	27.60	30.03	560	0.940	0.898	108.18	
	90	865	0.18	0.41	23.79	30.03	560	0.740	0.714	82.13	
	92.5	868	0.18	0.49	28.47	30.04	560	0.890	0.850	88.44	
	95	894	0.17	0.47	27.65	30.03	560	1.000	0.965	108.32	
	97.5	899	0.16	0.47	28.82	30.04	561	1.010	0.974	108.70	
	100	887	0.14	0.38	27.85	30.03	561	1.020	0.983	110.53	
Total 100	Average 862	Average 0.16	Average 0.43	Average 27.85	Average 30.03	Average 557	Total 39,236	Total 38,111	Average 102.36		

Combustion Gas Data for:

Northern Pulp

Client: Northern Pulp
Job Number: 121511288

Plant: Picou
Location: Dissolving Tank
Test: PM-2
Date: 21-Aug-14
Personnel: CAM/MIM

Test Start: 8:30 AM
Test Finish: 9:00 AM

Time (min)	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
0	20.89	0.00	0.0	0	0
5	20.90	0.00	0.0	0	0
10	20.88	0.00	0.0	0	0
15	20.89	0.00	0.0	0	0
20	21.00	0.00	0.0	0	0
25	20.90	0.00	0.0	0	0
30	20.90	0.00	0.0	0	0
Average:	20.91	0.00	0.0	0	0

Client: Northern Pulp
Job Number: 121911359

Plant: Futou
Location: Breeding Test
Test: P4-1
Date: 12-Aug-11
Personnel: CAM/DEM
Test Start: 6:10 AM
Test Finish: 10:00 AM

Parameters
Barometric Pressure, Pbar (in. Hg)
Static Static Pressure, Pstatic (in. H₂O)
Ambient Temp. (°F)
HCO Volume Collected, Vc (mL)
Total # Sampling Points,
Sampling Time per Point, (min)
Readings Taken Every — mins
Regulatory Agency

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
0	Blank	919.8	914.8	359.2
1	100 mL H ₂ O	1019.2	927.4	281.8
2	100 mL H ₂ O	983.4	715.6	264.8
3	Blank	678.6	622.9	24.1
4	200g Silica Gel	997.6	991.6	5.1
Total Weight Gain (g)				943.8
Moisture Volume (mL)				943.8

Particulate Collected from Filter (mg):
 Particulate Collected from Probe Wash (mg):
 Particulate Collected from Impinger Wash (mg):
 Total Particulate Collected (mg):

	CO ₂ (%)	CO ₂ (%)	H ₂ (%)	CO ₂ (ppm)	NO _x (ppm)	SO ₂ (ppm)
71.00	20.9					
-0.25	0.0					
20.00	78.1					
941.25	0.0					
20	0.0					
J	0.0					

Stack Diameter, (in.)
Stack Area, (sq. ft.)
Probe Length, (ft.)
Nozzle Diameter, (in.)
Pilot Coefficient, (Cp)
Gamma, meter constant
Port length (ft.)

(7) **Minimum Volume (ml)**
Total Weight Gals (lb)

Transverse Point	Time (min)	Black Gas Temp, T _g (°F)	S-Type Pilot delta P (in. H ₂ O)	Orifice delta H (in. H ₂ O)	Gas Meter Volume (cu. ft.)	Gas Meter Temp (°F)	Corrected (°F)
Transverse 1	1	2.5	70	0.71	348 810		
	2	9	152	0.12	363 760	55	53
	3	7.5	151	0.13	349 650	55	53
	4	10	161	0.16	354 550	54	51
	5	12.5	147	0.20	373 750	55	51
	6	16	145	0.22	359 660	55	51
	7	17.5	159	0.70	353 850	55	51
	8	20	144	0.47	351 850	55	51
	9	22.5	155	0.18	353 770	55	51
	10	25	153	0.15	356 750	56	54
	11	27.5	151	0.15	357 670	57	55
	12	30	169	0.16	358 510	56	54
	13	32.5	155	0.17	369 510	56	54
	14	36	160	0.18	410 560	56	54
	15	37.5	163	0.08	181 570	56	54
	16	40	145	0.17	404 550	56	54
	17	42.5	169	0.19	482 540	56	54
	18	45	165	0.19	491 510	56	54
	19	47.5	196	0.15	461 510	100	100
	20	50	191	0.18	485 600	100	100
Transverse 2	1	52.5	705	0.14	476 610		
	2	54	751	0.13	467 650	55	51
	3	57.5	761	0.11	468 450	100	100
	4	60	716	0.13	469 160	100	100
	5	62.5	799	0.15	418 640	101	101
	6	65	791	0.15	418 640	101	101
	7	67.5	764	0.15	411 640	101	101
	8	70	713	0.15	417 610	101	101
	9	72.5	751	0.19	415 500	101	101
	10	74	726	0.19	414 500	101	101
	11	76	711	0.19	413 540	101	101
	12	77.5	769	0.19	416 520	101	101
	13	80	825	0.19	437 530	101	101
	14	82.5	797	0.19	415 540	101	101
	15	85	780	0.17	413 610	101	101
	16	87.5	718	0.16	419 750	101	101
	17	90	715	0.18	410 570	101	101
	18	92.5	713	0.18	415 770	101	101
	19	95	764	0.19	415 770	101	101
	20	97.5	762	0.21	431 650	101	101
	21	100	759	0.21	434 560	101	101

Calculation for: Northern Pip Survey Scatter Testing Test #3

Client: Northern Pip
Job Number: 121511268
Plant: Pison
Location: Deepening Tank
Test: PM-J
Date: 22-Aug-14
Personnel: CAG/MS

Calculated Parameters

Stack Gas Pressure, Pa (m.Hg) 28.89
Stack Gas Molecular Weight, Dry Basis, M_d (lb/lb-mole) 28.85
Volume of Water Vapor Collected, Vol_w (cu.ft) 41.263
Stack Gas Molecular Content (N₂ as default) 0.287
Stack Gas Molecular Weight, Wet Basis, M_w (lb/lb-mole) 22.08

Isolenticity Checks

Check average Within Criteria

Transverse	Transverse Point	Time (min)	Stack Gas Temp, T _s (R)	Stack Gas P _s (m.Hg)	Orifice dia H (in. H ₂ O)	Stack Gas Velocity, U _s (ft/s)	Mass Flow Rate (lb/s)	Avg. Temp, T _m (R)	Gas Meter Volume, V _m (cu. ft)	Vol. @ Ref. Temp (cu. ft)	Isolenticity (%)
Transverse 1	1	2.5	653	0.13	0.28	24.20	30.02	583	0.770	0.752	105.87
	2	5	642	0.12	0.28	24.18	30.02	583	0.760	0.738	107.24
	3	7.5	645	0.13	0.28	24.04	30.02	564	0.800	0.781	108.22
	4	10	651	0.16	0.35	27.91	30.03	564	0.850	0.830	105.10
	5	15	667	0.18	0.41	30.58	30.03	554	0.800	0.781	111.12
	6	17.5	668	0.20	0.50	31.57	30.03	554	0.870	0.846	108.42
	7	20	668	0.17	0.37	31.40	30.03	555	0.880	0.855	108.86
	8	22.5	656	0.18	0.37	28.93	30.03	555	0.820	0.806	110.85
	9	25	653	0.18	0.34	28.77	30.03	556	0.860	0.824	110.84
	10	27.5	663	0.16	0.35	28.85	30.03	556	0.850	0.824	110.82
	11	30	669	0.18	0.34	28.17	30.03	556	0.910	0.863	113.04
	12	32.5	672	0.17	0.38	30.01	30.03	556	0.850	0.804	108.42
	13	35	669	0.18	0.38	29.25	30.03	557	0.860	0.835	108.78
	14	37.5	653	0.18	0.17	30.01	30.03	557	0.830	0.803	109.22
	15	40	659	0.19	0.41	18.82	30.03	557	0.830	0.811	110.43
	16	42.5	659	0.19	0.41	30.80	30.03	557	0.870	0.841	112.33
	17	45	658	0.19	0.41	30.53	30.03	558	1.000	0.941	109.98
	18	47.5	658	0.18	0.38	28.72	30.03	558	0.960	0.909	113.00
Transverse 2	1	50	682	0.18	0.38	28.86	30.03	558	0.960	0.901	114.83
	2	52.5	685	0.14	0.30	26.38	30.02	568	0.920	0.865	108.46
	3	55	681	0.13	0.28	25.33	30.02	568	0.830	0.805	110.08
	4	57.5	684	0.14	0.30	25.33	30.02	568	0.793	0.736	104.50
	5	60	676	0.18	0.38	26.37	30.02	568	0.737	0.713	87.50
	6	62.5	668	0.15	0.33	27.17	30.02	569	0.860	0.851	103.82
	7	65	665	0.18	0.33	27.11	30.02	569	0.820	0.782	104.15
	8	67.5	681	0.18	0.30	29.83	30.02	569	0.780	0.753	84.84
	9	70	673	0.20	0.43	31.73	30.03	569	0.770	0.744	83.49
	10	72.5	671	0.19	0.41	30.86	30.03	569	0.890	0.860	96.00
	11	75	671	0.19	0.41	30.86	30.03	569	0.890	0.860	96.00
	12	77.5	689	0.18	0.41	30.86	30.03	569	0.890	0.860	96.00
	13	80	678	0.18	0.41	30.86	30.03	569	0.890	0.860	96.00
	14	82.5	682	0.19	0.41	30.86	30.03	569	0.890	0.860	96.00
	15	85	680	0.19	0.41	30.86	30.03	569	0.890	0.860	96.00
	16	87.5	678	0.17	0.37	30.87	30.03	569	0.890	0.860	96.00
	17	90	674	0.18	0.38	30.21	30.03	569	0.890	0.860	96.00
	18	92.5	678	0.18	0.38	30.12	30.03	569	0.890	0.860	96.00
Total		100	Average 684	Average 0.17	Average 0.38	Average 28.11	Average 30.03	Average 558	Total 35.830	Total 34.530	Average 100.80

Combustion Gas Data for: Northern Pulp

Client: Northern Pulp
Job Number: 121511269

Plant: Fido
Location: Dissolving Tank
Test: PM-3
Date: 22-Aug-14
Personnel: CAMMM

Test Start: 5:30 AM
Test Finish: 9:18 AM

Time (min)	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
0	20.90	0.00	0.0	0	0
5	20.90	0.00	0.0	0	0
10	20.90	0.00	0.0	0	0
15	20.90	0.00	0.0	0	0
20	20.90	0.00	0.0	0	0
25	20.90	0.00	0.0	0	0
30	20.90	0.00	0.0	0	0
Average:	20.90	0.00	0.0	0	0

DATA ENTRY

Northern Pulp
Dissolving Tank

Operating Conditions: Normal
Stack Height from Grade: 51 m
Stack Diameter: 1.22 m

Reference Temperature, Tref (F): 77
(K): 298
Reference Pressure, Pref (in.Hg): 29.92
(Bar): 1.0

Parameter	Symbol	Units	Test 1	Test 2	Test 3	Average
Test ID	-	-	PM-1	PM-2	PM-3	-
Date	-	-	20-Aug-14	21-Aug-14	22-Aug-14	-
Start Time	-	-	2:50 PM	8:20 AM	8:10 AM	n/a
End Time	-	-	4:00 PM	10:20 AM	10:00 AM	n/a
Total Sampling Time	-	min	100	100	100	100
Stack Diameter	D	in.	48	48	48	48
Average Stack Gas Temperature	Ts	F	204	202	204	203
Average Dry Gas Meter Temperature	Tm	F	101	97	98	98
Barometric Pressure	Pbar	in.Hg	30.00	30.00	30.00	30.00
Stack Static Pressure	Pstatic	in.H2O	-0.20	-0.20	-0.20	-0.20
Average Pressure Drop (Head)	dP	in.H2O	0.17	0.16	0.17	0.17
Average deltaH Orifice	dH	in.H2O	0.36	0.43	0.38	0.39
Average Meter Temperature	Tm	F	101	97	98	98
Gas Sample Volume	Vm	cu.ft	37.10	39.23	35.63	37.32
Average Isokinetics	I	%	102.2	108.4	107	106
Nozzle Diameter	Dn	in.	0.311	0.311	0.311	0.311
Pitot Coefficient	Cp	-	0.836	0.836	0.836	0.836
Gamma, meter constant	y	-	1.003	1.003	1.003	1.003
Reference Temperature	Tref	R	537	537	537	537
Reference Pressure	Pref	in.Hg	29.92	29.92	29.92	29.92
Stack Gas Oxygen Content	Co2	%	20.9	20.9	20.9	20.9
Stack Gas Carbon Dioxide Content	Cco2	%	0.0	0.0	0.0	0.0
Stack Gas Nitrogen Content	Cn2	%	79.1	79.1	79.1	79.1
Stack Gas Sulphur Dioxide Content	Cso2	ppm	0.0	0.0	0.0	0.0
Stack Gas Nitrogen Oxides Content	Cnox	ppm	0.0	0.0	0.0	0.0
Stack Gas Carbon Monoxide Content	Cco	ppm	0.0	0.0	0.0	0.0
Volume of Water Collected	Vw	mL	809	802	944	851
Particulate Collected from Filter	-	mg	601	443	600	548
Particulate Collected from Probe Wash	-	mg	265	333	88.8	235
Particulate Collected from Impinger Wash	-	mg	85.2	65.5	74.4	75.0
Total Particulate Collected (excluding impingers)	Mp	mg	866	778	687	783

Legend: F - degrees Fahrenheit
K - degrees Kelvin
Bar - bars
in.Hg - inches of mercury
in. - inches

in.H2O - inches of water
cu.ft - cubic feet
R - degrees Rankin
NOx - as NO2

Northern Pulp
Dissolving Tank
Operating Conditions: Normal
Stack Height from Grade: 51 m
Stack Diameter: 1.22 m

Variable	Symbol	Units	Calculation	Test 1	Test 2	Test 3	Average
Stack Area	A_s	m^2 $sq.ft$	$A_s = \pi \times (D/2)^2 \times 4$ $A_s (sq.ft) = A_s (m^2) \times 10.764$	12.57 1.17	12.57 1.17	12.57 1.17	12.57 1.17
Barometric Pressure	P_{bar}	kPa	$P_{bar} (kPa) = P_{bar} (in.Hg) \times 3.386$	101.8	101.8	101.8	101.8
Stack Static Pressure	P_{static}	kPa	$P_{static} (kPa) = P_{static} (in.Hg) \times 3.386$	-0.05	-0.05	-0.05	-0.05
Avg. Stack Temperature	T_s	R	$T_s (R) = T_s (F) + 459.67$	564	564	564	564
Avg. Meter Temperature	T_m	R	$T_m (R) = T_m (F) + 459.67$	561	567	558	561.3
Nozzle Diameter	D_n	mm	$D_n (mm) = D_n (in.) \times 25.4$	8	8	8	8
Gas Meter Pressure	P_m	in.Hg	$P_m = P_{bar} + (dH / 13.6)$	30.03	30.03	30.03	30.03
Sample Volume at Ref Cond	V_{sc}	$cu.ft$ $cu.m$	$V_{sc} = T_{ref} \times P_{sc} \times (V_{sc} \times P_{sc} \times T_{sc}) / T_{sc}$ $V_{sc} (cu.m) = V_{sc} (cu.ft) \times 0.02832$	35.77 1.01	38.10 1.08	34.53 0.98	36.1 1.02
Volume of Water Vapour	V_{wc}	$cu.ft$	$V_{wc} = 0.0423 \times V_{sc}$	38.6	38.6	45.3	40.9
Water Fraction	B_{wc}	-	$B_{wc} = V_{wc} / (V_{wc} + V_{sc})$	0.52	0.50	0.57	0.53
Molecular Weight, Dry	M_d	lb/lb-mol	$M_d = 0.44 (CO_2) + 0.32 (CO) + 0.28 (N_2)$	28.8	28.8	28.8	28.8
Molecular Weight, Wet	M_w	lb/lb-mol	$M_w = M_d (1 - B_{wc}) + (18 \times B_{wc})$	23.2	23.4	22.7	23.1
Stack Pressure	P_s	in.Hg	$P_s = P_{bar} + P_{static} / 13.6$	30.0	30.0	30.0	30.0
Stack Gas Velocity	U_s	ft/s	$U_s = 85.33 \times C_p \times ((dP \times T_s) / (P_s \times M_d))^{0.5}$	28.5	27.9	29.1	28.5
Actual Stack Gas Flow Rate	Q	$scfm$	$Q = U_s \times A_s$	8.89	8.81	8.87	8.89
Dry Stack Gas Flow Rate	Q_d	$scfm$	$Q_d = Q \times (1 - B_{wc}) \times (T_{ref} / T_s) \times (P_{sc} / P_s)$	21,498	21,048	21,932	21,498
			$Q_d (Nm^3) = 1.359472 \times Q_d (scfm)$	8,363	8,510	7,702	8,188
				3.94	4.02	3.64	3.86
Sulphur Dioxide - SO ₂							
SO ₂ Measured Concentration	C_{SO2}	ppm	Measurement from Flow Gas Analyzer	ND	ND	ND	ND
Uncorrected @ Ref Cond	C_{SO2}	mg/Ram	$C_{SO2} (mg/Ram) = C_{SO2} (ppm) \times 2.63$	ND	ND	ND	ND
SO ₂ Emission Rate	ER_{SO2}	g/s kg/hr	$ER_{SO2} = C_{SO2} / 1000 \times Q_d$ $ER_{SO2} (kg/hr) = 3.6 \times ER_{SO2} (g/s)$	ND	ND	ND	ND
Nitrogen Oxides - NO _x							
NO _x Measured Concentration	C_{NOx}	ppm	Measurement from Flow Gas Analyzer	ND	ND	ND	ND
Uncorrected @ Ref Cond	C_{NOx}	mg/Ram	$C_{NOx} (mg/Ram) = C_{NOx} (ppm) \times 1.887$	ND	ND	ND	ND
NO _x Emission Rate	ER_{NOx}	g/s kg/hr	$ER_{NOx} = C_{NOx} / 1000 \times Q_d$ $ER_{NOx} (kg/hr) = 3.6 \times ER_{NOx} (g/s)$	ND	ND	ND	ND
Carbon Monoxide - CO							
CO Measured Concentration	C_{CO}	ppm	Measurement from Flow Gas Analyzer	ND	ND	ND	ND
Uncorrected @ Ref Cond	C_{CO}	mg/Ram	$C_{CO} (mg/Ram) = C_{CO} (ppm) \times 1.145$	ND	ND	ND	ND
CO Emission Rate	ER_{CO}	g/s kg/hr	$ER_{CO} = C_{CO} / 1000 \times Q_d$ $ER_{CO} (kg/hr) = 3.6 \times ER_{CO} (g/s)$	ND	ND	ND	ND
Particulate Concentration	C_p	mg/Ram	$C_p = M_p / V_{sc}$	874	720	702	765
Particulate Emission Rate	ER_p	g/s kg/hr	$ER_p = C_p / 1000 \times Q_d$ $ER_p (kg/hr) = 3.6 \times ER_p (g/s)$	3.45 12.41	2.89 10.40	2.55 9.18	2.96 10.67
Emission Metric		kg/tonne/day		868	890	831	830
Emission Metric		kg/tonne/day		0.31	0.38	0.27	0.31

Legend:
sq.ft - square feet
sq.m - square metres
PI - 3.142
R - degrees Rankin
ppm - parts per million

in.Hg - inches of mercury
cu.ft - cubic feet
cu.m - cubic metres
Ref Cond - reference temperature and pressure (25 C and 101.3 kPa)
Nm³ - dry reference cubic metres per second
Nm³ - dry reference cubic feet per minute

mg/Ram - milligrams per dry reference cubic metre
g/s - grams per second
NO_x - as NO₂
scfm - actual cubic feet per minute
scfm - air dried unheated metric tonnes

OFFICIAL STACK TESTING RESULTS

Northern Pulp

Dissolving Tank

Operating Conditions: Normal

Stack Height from Grade: 51 m

Stack Diameter: 1.22 m

Parameter	Test 1	Test 2	Test 3	Average	NSENV Limits
Test ID	PM-1	PM-2	PM-3	-	-
Test Date	20-Aug-14	21-Aug-14	22-Aug-14	-	-
Stack Gas Temperature (C)	96	95	95	95	-
Moisture Content (%)	52.1	50.2	56.7	53.0	-
Velocity (m/s)	8.69	8.51	8.87	8.69	-
Volumetric Flow (Rcms)	3.94	4.02	3.84	3.86	-
Oxygen - O2 (%)	20.9	20.9	20.9	20.9	-
Carbon Dioxide - CO2 (%)	0.0	0.0	0.0	0.0	-
Sulphur Dioxide - SO2					
SO2 Measured Concentration (ppm)	ND	ND	ND	ND	-
Uncorrected at Ref Cond (mg/Rcm)	ND	ND	ND	ND	-
Emission Rate (kg/hr)	ND	ND	ND	ND	-
Nitrogen Oxides - NOx					
NOx Measured Concentration (ppm)	ND	ND	ND	ND	-
Uncorrected at Ref Cond (mg/Rcm)	ND	ND	ND	ND	-
Emission Rate (kg/hr)	ND	ND	ND	ND	-
Carbon Monoxide - CO					
CO Measured Concentration (ppm)	ND	ND	ND	ND	-
Uncorrected at Ref Cond (mg/Rcm)	ND	ND	ND	ND	-
Emission Rate (kg/hr)	ND	ND	ND	ND	-
Particulate Matter - PM					
Particulate Concentration (mg/Rcm)	874	720	702	765	-
Particulate Emission Rate (kg/hr)	12.41	10.40	9.19	10.67	-
Particulate Emission Rate (kg/ADUBMT)	0.31	0.36	0.27	0.31	0.60

Legend: C - degrees Celsius
m/s - metres per second
Rcms - dry reference cubic metres per second
ppm - parts per million
ADUBMT - air dried unbleached metric tonnes

Ref Cond - reference temperature and pressure (25 C and 101.3 kPa)
mg/Rcm - milligrams per dry reference cubic metre
NOx - as NO2
ND - non-detectable

John Macomber, 721 6th Ave.

WINGER CATCH

[illegible]

HEAVEN JOURNAL

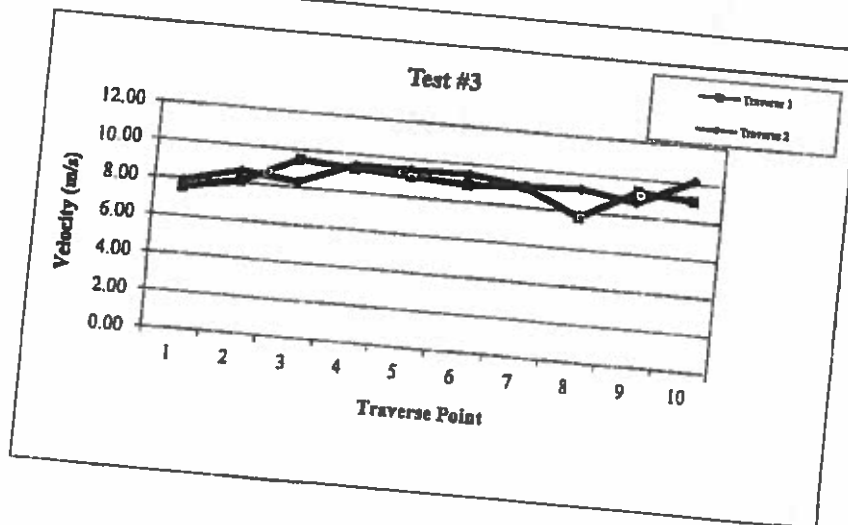
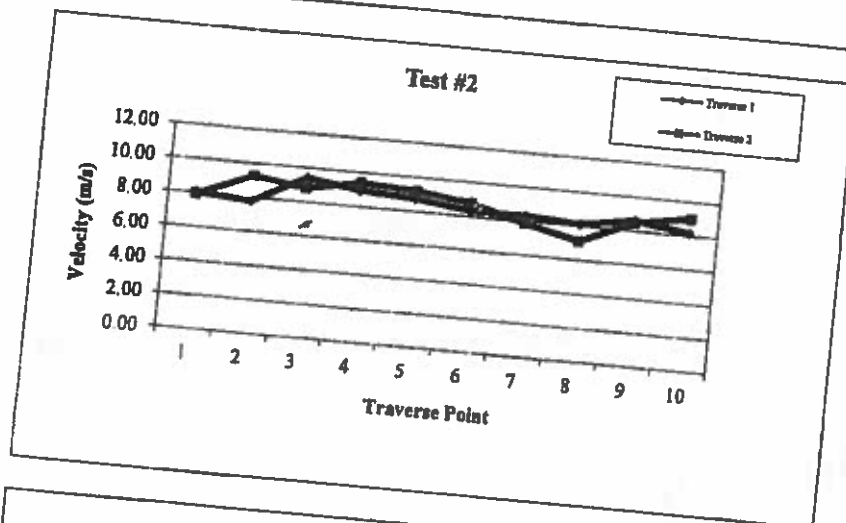
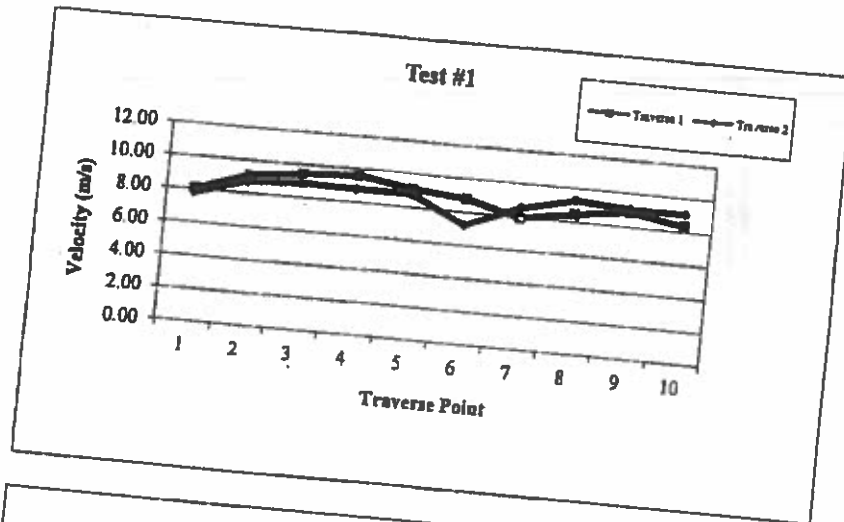
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University of Amsterdam

FILTER CATCH

1-Form ID	Pre-Tested 100				Sample ID	Post-Tested 100				Post-Tested Weighted Mean Factorial
	Pre-Tested by					Post-Tested by				
	Form 1	Form 2	Form 3	Form 4		Form 1	Form 2	Form 3	Form 4	
0518-18	0.5004	0.5004	0.5004	0.5004	PA-1	0.5004	0.5004	0.5004	0.5004	0.5004
0518-21	0.5004	0.5004	0.5004	0.5004	PA-2	0.5004	0.5004	0.5004	0.5004	0.5004
0518-7	0.5004	0.5004	0.5004	0.5004	PA-3	0.5004	0.5004	0.5004	0.5004	0.5004

Stack Gas Velocity Profiles
Dissolving Tank



Plant: PWRU
Location: Power Bldg
Tant: Pkg-1
Date: 18-Aug-14
Permitted: CALSWA

Calculated Parameters

Stock Gas Pressure, Ps (atm)
 Stock Gas Molecular Weight, Dry Basis, Md (N₂/H₂-mole)
 Volume of Water Vapor Collected, Vwc (cc)
 Stock Gas Mixture Content (% as defined)
 Stock Gas Molecular Weight, Wet Basis, Mw (N₂/H₂-mole)

石胡荽 蔓草 花紫 果白

Reliability Checks

Check coverage

Transverse Point	Time (min)	Shank Gun Temp., T _g (°C)	S-type Prod. Rate, P (lb. H ₂ O)	Orifice Depth, H (in. H ₂ O)	Shank Gun Velocity, U _g (ft/s)	Water Press., P _w (in. Hg)	Avg. Temp., T _m (°F)	Gas Meter Vol., V _m (cc. ft.)	Vol. @ Std. Press. (cc. ft.)	Refractometer I (%)	
Transverse 1	1	2.5	604	0.60	0.45	30.03	530	1.050	1.072	113.53	
	2	5	604	0.78	0.44	30.03	528	1.000	1.022	109.41	
	3	7.5	598	0.69	0.39	30.03	528	0.960	0.981	111.10	
	4	12.5	602	0.72	0.40	30.03	528	0.960	0.982	106.23	
	5	15	606	0.80	0.34	30.03	528	0.860	0.881	108.77	
	6	17.5	602	0.59	0.35	30.03	528	0.860	0.881	118.34	
	7	22.5	602	0.58	0.34	30.03	528	0.860	0.880	116.59	
	8	26	602	0.61	0.34	30.03	528	0.860	0.880	114.08	
	9	30	602	0.84	0.34	30.03	528	0.860	0.880	111.34	
	10	32.5	602	0.87	0.47	30.03	530	0.860	0.880	116.09	
	11	35	604	1.70	0.49	30.03	530	0.810	0.810	107.28	
	12	37.5	598	1.79	0.50	30.07	530	1.440	1.467	108.91	
Transverse 2	1	62.5	598	1.30	0.74	30.05	630	1.320	1.347	111.27	
	2	65	597	1.20	0.60	30.05	631	1.240	1.264	104.50	
	3	67.5	602	1.20	0.60	30.05	631	1.240	1.264	106.07	
	4	72.5	600	1.10	0.62	30.05	631	1.070	1.090	107.82	
	5	77.5	603	1.00	0.58	30.05	632	1.180	1.201	107.36	
	6	80	601	1.29	0.68	30.04	632	1.150	1.170	110.54	
	7	82.5	601	1.10	0.82	30.05	632	1.260	1.280	108.23	
	8	85	601	1.20	0.66	30.05	632	1.110	1.130	107.29	
	9	87.5	603	1.20	0.69	30.05	634	1.060	1.079	108.09	
	10	89.5	603	1.20	0.69	30.05	634	1.060	1.079	108.09	
	11	94	603	0.76	0.69	30.05	636	1.200	1.225	103.81	
	12	97.5	602	0.83	0.68	30.05	635	1.210	1.235	108.14	
Total	100		Average 602	Average 1.08	Average 0.60	Average 532	Total 54.560	Average 108.84			
	102.5										
	105										
	107.5										
	110										
	112.5										
	115										
	117.5										
	120										
	Total	120									

Combustion Gas Data for: Northern Pulp

Client: Northern Pulp
Job Number: 121511289

Plant: Picchu
Location: Power Boiler
Test: PM-1
Date: 19-Aug-14
Personnel: CAM/MM

Test Start: 4:00 PM
Test Finish: 4:30 PM

Time (min)	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
0	12.40	6.30	448	0	36
5	12.40	6.10	473	0	37
10	12.80	6.20	541	0	36
15	12.70	6.00	606	0	37
20	12.60	6.20	734	0	40
25	11.70	6.80	685	0	41
30	10.80	7.40	390	0	48
Average:	12.97	6.50	554	0	39

Raw Data for: Test #2

Client: Northern Pulp
Job Number: 121811289

Plant: Pulp
Location: Pulp Mill
Test: PM-1
Date: 12-Aug-11
Parameter: CUM-PM
Test Start: 1:00 PM
Test Finish: 1:05 PM

Parameters:
Barometric Pressure, Pbar (in. Hg)
Stack Static Pressure, Pstatic (in. H2O)
Ambient Temp, (°F)
H2O Volume Collected, Vw (mL)
Total # Sampling Points,
Sampling Time per Point, (min)
Readings Taken Every, min

Parameters:
Barometric Pressure, Pbar (in. Hg)
Stack Static Pressure, Pstatic (in. H2O)
Ambient Temp, (°F)
H2O Volume Collected, Vw (mL)
Total # Sampling Points,
Sampling Time per Point, (min)
Readings Taken Every, min

Parameters:
Barometric Pressure, Pbar (in. Hg)
Stack Static Pressure, Pstatic (in. H2O)
Ambient Temp, (°F)
H2O Volume Collected, Vw (mL)
Total # Sampling Points,
Sampling Time per Point, (min)
Readings Taken Every, min

Transverse 1

Time (min)

Shake Gas Temp, Tg (°F)

g-type Pstat delta P (in. H2O)

Orifice delta H (in. H2O)

Gas Meter Volume (cc. RL)

Inlet (°F)

Outlet (°F)

Stack Diameter (in.)

Stack Area (sq. in.)

Probe Length (ft.)

Nozzle Diameter (in.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

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Gasman, meter coefficient

Port length (ft.)

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Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Transverse 2

Time (min)

Shake Gas Temp, Tg (°F)

g-type Pstat delta P (in. H2O)

Orifice delta H (in. H2O)

Gas Meter Volume (cc. RL)

Inlet (°F)

Outlet (°F)

Stack Diameter (in.)

Stack Area (sq. in.)

Probe Length (ft.)

Nozzle Diameter (in.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Flow Coefficient, Kp

Gasman, meter coefficient

Port length (ft.)

Impinger No.
1
2
3
4

Impinger Contents
100 mL H2O
100 mL H2O
Blank
200g Silica Gel

Particulates Collected from Filter (mg)
Particulates Collected from Probe Head (mg)
Particulates Collected from Impinger Head (mg)
Total Particulates Collected (mg)

Particulates Collected from Filter (mg)
Particulates Collected from Probe Head (mg)
Particulates Collected from Impinger Head (mg)
Total Particulates Collected (mg)

Particulates Collected from Filter (mg)
Particulates Collected from Probe Head (mg)
Particulates Collected from Impinger Head (mg)
Total Particulates Collected (mg)

Pust Weight (g)
84.3
7.88
682.2
886.6

Tare Weight (g)
188.7
7.11
671.7
856.6

Total Weight Gain (g)
263.2
283.2

Moisture Volume (mL)
7.2
28.77
8
8.175
0.817
1.003
8

Moisture Volume (mL)
7.2
28.77
8
8.175
0.817
1.003
8

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1.003
8

Moisture Volume (mL)
7.2
28.77
8
8.175
0.817
1.003
8

Moisture Volume (mL)
7.2
28.77
8
8.175
0.817
1.003
8

Calculations for Northern Pip Buyer Source Trading
Test #2

Client: Northern Pip
Job Number: 11161139

Plant: Pibou
Location: Pibou Baker
Test: PMA-2
Date: 16 Aug-14
Personnel: CMM/M

Calculated Parameters

Stock Gas Pressure, Ps (gauge)
Stock Gas Molecular Weight, Dry Basis, M_d (lb/lb-mole)
Volume of Water Vapor Collected, V_w (cu ft)
Stock Gas Molecular Weight, Wet Basis, M_w (lb/lb-mole)

28.24
28.41
12.964
8.989
27.14

Isokinetic Checks

Check average: Within Criteria

Transverse Point	Time (min)	Stock Gas Temp, T _s (°F)	S-type Pitot static P (in. H ₂ O)	Orifice dia, H (in. H ₂ O)	Stock Gas Velocity, U _s (ft/s)	Molar Press., P _s (in. Hg)	Avg. Temp., T _m (°F)	Gas Meter Volume, V _m (cu. ft)	Vol. @ Ref. Press (cu. ft)	Isokinetic I (%)
Transverse 1	2.5	603	1.10	0.83	62.01	30.05	538	1.190	1.195	106.46
	5	603	1.00	0.87	59.88	30.04	538	1.140	1.146	106.16
	7.5	603	1.00	0.87	59.88	30.04	538	1.110	1.116	106.16
	10	602	0.99	0.83	59.88	30.05	538	1.080	1.087	106.02
	12.5	605	0.87	0.86	58.10	30.04	538	1.120	1.127	106.02
	15	604	0.85	0.84	58.51	30.04	538	1.080	1.086	106.09
	17.5	600	0.87	0.86	58.51	30.04	538	1.120	1.126	106.51
	20	601	0.87	0.86	58.51	30.04	538	1.120	1.126	106.51
	22.5	602	1.00	0.87	59.88	30.04	538	1.140	1.147	106.57
	25	600	0.87	0.86	58.51	30.04	538	1.120	1.127	106.57
	27.5	597	1.00	0.87	59.88	30.04	538	1.150	1.157	106.57
	30	604	0.86	0.86	58.51	30.04	538	1.130	1.136	110.41
Transverse 2	32.5	602	0.82	0.80	54.82	30.02	536	0.960	0.964	112.59
	35	602	0.82	0.80	54.82	30.02	536	0.960	0.964	112.59
	37.5	605	0.44	0.25	38.86	30.02	536	0.790	0.793	112.59
	40	605	0.44	0.25	38.86	30.02	536	0.790	0.793	112.59
	42.5	598	0.48	0.28	41.81	30.02	536	0.790	0.794	107.54
	45	591	0.48	0.28	41.82	30.02	536	0.790	0.794	107.54
	47.5	604	0.54	0.31	44.12	30.02	538	0.770	0.774	100.35
	50	603	0.54	0.31	44.08	30.02	538	0.760	0.764	100.35
	52.5	605	0.58	0.33	45.78	30.02	538	0.790	0.794	88.07
	55	604	0.58	0.34	46.11	30.02	538	0.790	0.794	88.07
	57.5	605	0.50	0.28	42.89	30.02	538	0.820	0.824	88.07
	60	604	0.50	0.28	42.86	30.02	538	0.810	0.814	106.70
Transverse 3	62.5	612	0.82	0.48	54.72	30.03	537	1.040	1.047	110.06
	65	612	0.85	0.48	55.71	30.04	538	1.090	1.096	110.06
	67.5	611	0.83	0.36	47.83	30.03	538	0.830	0.834	111.59
	70	611	0.83	0.36	47.83	30.03	538	0.830	0.834	111.59
	72.5	613	0.53	0.30	44.08	30.02	538	0.830	0.832	109.50
	75	616	0.58	0.31	45.37	30.02	538	0.830	0.832	109.50
	77.5	607	0.55	0.31	44.83	30.02	540	0.890	0.892	110.52
	80	607	0.55	0.31	44.83	30.02	540	0.890	0.892	110.52
	82.5	607	0.81	0.35	47.00	30.03	541	0.950	0.950	101.38
	85	604	0.80	0.34	46.11	30.03	541	0.900	0.900	110.78
	87.5	604	0.79	0.48	55.36	30.03	541	1.040	1.040	111.37
	90	607	0.80	0.48	55.36	30.03	541	1.040	1.040	111.37
Transverse 4	92.5	607	1.00	0.87	78.40	30.07	542	1.380	1.378	104.45
	95	606	1.00	0.87	78.40	30.07	542	1.380	1.378	104.45
	97.5	607	1.70	0.87	78.40	30.07	542	1.480	1.458	108.79
	100	607	1.70	0.87	78.40	30.07	542	1.480	1.458	108.79
	102.5	605	1.70	0.87	78.40	30.07	543	1.480	1.447	108.79
	105	605	1.70	0.86	78.40	30.07	543	1.480	1.447	108.79
	107.5	605	1.70	0.86	78.40	30.07	543	1.480	1.447	108.79
	110	607	1.70	0.86	78.40	30.07	543	1.480	1.447	108.79
	112.5	607	1.70	0.86	78.40	30.07	543	1.480	1.447	108.79
	115	607	1.70	0.86	78.40	30.07	543	1.480	1.447	108.79
	117.5	607	1.70	0.86	78.40	30.07	543	1.480	1.447	108.79
	120	605	1.30	0.74	68.88	30.05	544	1.320	1.314	110.13
Total	120	Average 605	Average 0.83	Average 0.54	Average 58.52	Average 30.04	Average 539	Total 50.730	Total 50.834	Average 107.45

Calculations for Northern Pip Summer Seals Testing Test #1

Client: Northern Pip
Job Number: 1215/1200
Plant Policy
Location: Young Bay
Track: PM-3
Date: 20-Aug-14
Permitted: CMMMM

Calculated Parameters

Stock Gas Pressure, P₁ (Pa)
Stock Gas Molecular Weight, Dry Basis, M_d (g/mole)
Volume of Water Vapor Collected, V_w (mL)
Stock Gas Molecular Weight, Wet Basis, M_w (g/mole)
Stock Gas Molecular Weight, Wet Basis, M_w (g/mole)

20.91
28.48
11.276
0.104
27.31

Inclinometer Checks

Check average

Within Criteria

Transverse Point	Time (min)	Stock Gas Temp, T ₁ (°C)	S-type Pk, delta P (m. H ₂ O)	Orifice delta P (m. H ₂ O)	Stock Gas Velocity, U _s (ft/s)	Water Pressure, P _w (m. Hg)	Avg. Temp, T ₁ (°C)	Gas Meter V ₁ (m. H ₂ O)	Vol. @ Std. Press (m. H ₂ O)	Inclinometer (°)
Transverse 1	1	2.5	0.04	0.37	44.82	30.03	533	0.950	0.993	111.20
	2	7.5	0.05	0.37	44.33	30.03	532	0.940	0.985	111.27
	3	12.5	0.05	0.37	45.33	30.02	533	0.980	0.982	112.40
	4	17.5	0.05	0.36	45.22	30.02	535	0.910	0.975	112.29
	5	22.5	0.05	0.36	46.00	30.02	533	0.870	0.972	112.74
	6	27.5	0.05	0.34	38.38	30.02	534	0.750	0.791	108.52
	7	32.5	0.05	0.28	40.86	30.02	534	0.810	0.789	111.43
	8	37.5	0.05	0.37	46.33	30.03	534	0.770	0.820	118.00
	9	42.5	0.05	0.37	46.33	30.03	534	0.830	0.840	107.81
	10	47.5	0.05	0.37	70.75	30.03	534	0.910	0.892	112.08
	11	52.5	0.05	0.40	70.75	30.03	535	0.910	0.921	112.03
	12	57.5	0.05	0.40	70.75	30.03	535	0.910	0.921	112.03
Transverse 2	1	62.5	0.05	0.57	59.85	30.04	537	1.220	1.220	115.51
	2	67.5	0.05	0.57	59.85	30.04	538	1.170	1.177	110.37
	3	72.5	0.05	0.57	59.85	30.04	538	1.150	1.157	102.59
	4	77.5	0.05	0.56	59.85	30.04	539	1.090	1.095	102.59
	5	82.5	0.05	0.56	59.25	30.04	539	1.120	1.065	102.59
	6	87.5	0.05	0.51	58.82	30.04	540	1.140	1.124	107.84
	7	92.5	0.05	0.55	58.46	30.04	540	1.100	1.144	108.34
	8	97.5	0.05	0.57	59.04	30.04	541	1.090	1.143	108.34
	9	102.5	0.05	0.55	59.45	30.04	541	1.150	1.081	108.34
	10	107.5	0.05	0.58	58.85	30.04	541	1.150	1.151	108.34
	11	112.5	0.05	0.58	48.85	30.03	541	1.140	1.141	108.34
	12	117.5	0.05	0.58	48.85	30.03	541	1.140	1.141	108.34
Total		120	Average 0.07	Average 0.48	Average 54.32	Average 30.04	Average 538	Total 48.730	Total 50.007	Average 108.34

Combustion Gas Data for: Northern Pulp

Client: Northern Pulp
Job Number: 121511259

Plant: Piclou
Location: Power Boiler
Test: PM-3

Date: 20-Aug-14
Personnel: CAM/MM

Test Start: 11:44 AM
Test Finish: 12:15 PM

Time (min)	O2 (%)	CO2 (%)	CO (ppm)	SO2 (ppm)	NOx (ppm)
0	12.40	5.60	727	0	30
5	13.59	5.50	1033	0	30
10	13.60	5.40	848	0	29
15	14.10	5.00	817	0	27
20	14.20	5.00	848	0	27
25	13.88	5.40	823	0	28
30	13.50	5.50	748	0	30
Average:	13.70	5.34	882	0	29

DATA ENTRY
Northern Pulp
Power Boiler
Fuel: Biomass
Operating Conditions: Normal
Emission Control Equipment: Scrubber
Stack Diameter: 1.83 m

Reference Temperature, Tref (F): 77
(K): 298
Reference Pressure, Pref (in.Hg): 29.92
(Bar): 1.0

Parameter	Symbol	Units	Test 1	Test 2	Test 3	Average
Test ID	-	-	PM-1	PM-2	PM-3	-
Date	-	-	18-Aug-14	19-Aug-14	20-Aug-14	-
Start Time	-	-	11:00 AM	3:00 PM	9:12 AM	n/a
End Time	-	-	1:00 PM	5:08 PM	11:20 AM	n/a
Total Sampling Time	-	min	120	120	120	120
Stack Diameter	D	in.	72	72	72	72
Average Stack Gas Temperature	Ta	F	142	145	144	144
Average Dry Gas Meter Temperature	Tm	F	72	79	78	78
Barometric Pressure	Pbar	in.Hg	30.00	30.00	30.00	30.00
Stack Static Pressure	Pstatic	in.H2O	0.20	0.20	0.20	0.20
Average Pressure Drop (Head)	dP	in.H2O	1.08	0.93	0.87	0.95
Average deltaH Orifice	dH	in.H2O	0.60	0.54	0.49	0.54
Average Meter Temperature	Tm	F	72	79	78	76
Gas Sample Volume	Vm	cu.ft	54.8	50.7	49.7	51.7
Average Isokinetics	I	%	108.8	107.5	108.4	108.2
Nozzle Diameter	Dn	in.	0.173	0.173	0.173	0.173
Pitot Coefficient	Cp	-	0.817	0.817	0.817	0.817
Gamma, meter constant	γ	-	1.003	1.003	1.003	1.003
Reference Temperature	Tref	R	537	537	537	537
Reference Pressure	Pref	in.Hg	29.92	29.92	29.92	29.92
Stack Gas Oxygen Content	Co2	%	12.1	13.8	13.7	13.2
Stack Gas Carbon Dioxide Content	Cco2	%	8.5	5.4	5.3	5.7
Stack Gas Nitrogen Content	Cn2	%	81.4	80.9	81.0	81.1
Stack Gas Sulphur Dioxide Content	Co2	ppm	0.0	0.0	0.0	0.0
Stack Gas Nitrogen Oxides Content	Cnox	ppm	39.0	30.4	28.7	32.7
Stack Gas Carbon Monoxide Content	Cco	ppm	584	938	882	801
Volume of Water Collected	Vw	mL	272	283	234.8	257
Particulate Collected from Filter	-	mg	215	288	248	250
Particulate Collected from Probe Wash	-	mg	14.85	8.50	18.6	13.8
Particulate Collected from Impinger Wash	-	mg	5.57	4.29	8.34	5.40
Total Particulate Collected (excluding impingers)	Mp	mg	230	294	288	284

Legend: F - degrees Fahrenheit
K - degrees Kelvin
Bar - bars
in.Hg - inches of mercury
in. - inches

in.H2O - inches of water
cu.ft - cubic feet
R - degrees Rankin
NOx - as NO2

CALCULATIONS
 Northern Pulp
 Power Boiler
 Fuel: Biomass
 Operating Conditions: Normal
 Emission Control Equipment: Scrubber
 Stack Diameter: 1.83 m

Variable	Symbol	Units	Calculation	Test 1	Test 2	Test 3	Average
Stack Area	A_s	sq ft sq.m	$A_s = \pi \times (D/12)^2 \times \pi / 4$ $A_s \text{ (sq.m)} = A_s \text{ (sq.ft)} \times 0.0929$	28.27 2.63	28.27 2.63	28.27 2.63	28.27 2.63
Barometric Pressure	P_{bar}	hPa	$P_{bar} \text{ (hPa)} = P_{bar} \text{ (in.Hg)} \times 3.386$	101.8	101.8	101.8	101.8
Stack Static Pressure	P_{static}	hPa	$P_{static} \text{ (hPa)} = P_{static} \text{ (in.Hg)} \times 3.386$	0.05	0.05	0.05	0.05
Avg. Stack Temperature	T_s	K	$T_s \text{ (K)} = T_s \text{ (°F)} + 459$	802	805	804	804
Avg. Meter Temperature	T_m	K	$T_m \text{ (K)} = T_m \text{ (°F)} + 459$	532	539	538	536
Nozzle Diameter	D_n	mm	$D_n \text{ (mm)} = D_n \text{ (in.)} \times 25.4$	4	4	4	4
Gas Meter Pressure	P_m	in.Hg	$P_m = P_{bar} + (dH / 13.6)$	30.04	30.04	30.04	30.04
Sample Volume at Ref Cond	V_{sc}	cu.ft	$V_{sc} = T_{ref} P_{ref} \times (V_m \times P_m \times \pi / T_m)$	53.48	50.86	48.89	52.1
Volume of Water Vapour	V_{wc}	cu.ft	$V_{wc} \text{ (cu.ft)} = 8.6231 \times V_{sc} \text{ (cu.ft)}$	1.57	1.44	1.42	1.48
Water Fraction	B_{wc}	-	$B_{wc} = V_{wc} / (V_{wc} + V_{sc})$	0.190	0.190	0.184	0.19
Molecular Weight, Dry	M_d	lb/lb-mol	$M_d = 0.44 \text{ (CO}_2\text{)} + 0.32 \text{ (CO)} + 0.20 \text{ (C}_2\text{H}_6\text{)}$	29.52	28.41	29.40	29.4
Molecular Weight, Wet	M_w	lb/lb-mol	$M_w = M_d (1 - B_{wc}) + (18 \times B_{wc})$	27.33	27.14	27.31	27.3
Stack Pressure	P_s	in.Hg	$P_s = P_{bar} + (P_{static} / 13.6)$	30.01	30.01	30.01	30.01
Stack Gas Velocity	U_s	ft/s m/s	$U_s = 85.33 \times C_p \times (dP \times T_{ref} / P_s \times M_d)^{0.5}$ $U_s \text{ (m/s)} = 0.3048 \times U_s \text{ (ft/s)}$	80.1 18.3	56.5 17.2	54.3 16.6	57.0 17.4
Actual Stack Gas Flow Rate	Q	acfm	$Q = U_s \times A_s$	102,008	95,878	92,144	96,877
Dry Stack Gas Flow Rate	Q_d	scfm	$Q_d = Q \times (1 - B_{wc}) \times (T_{ref} / T_s) \times (P_{ref} / P_s)$ $Q_d \text{ (scfm)} = 0.000472 \times Q \text{ (acfm)}$	73,884 34.9	68,361 32.3	67,022 31.9	69,758 32.8
Sulphur Dioxide - SO ₂							
SO ₂ Measured Concentration	C_{s2}	ppm	Measurement from Flue Gas Analyser	ND	ND	ND	ND
Uncorrected @ Ref Cond	C_{s2}	mg/lbm	$C_{s2} \text{ (mg/lbm)} = C_{s2} \text{ (ppm)} \times 1.67$	ND	ND	ND	ND
SO ₂ Emission Rate	ER_{s2}	g/s kg/hr	$ER_{s2} = C_{s2} / 1000 \times Q_d$ $ER_{s2} \text{ (kg/hr)} = 3.6 \times ER_{s2} \text{ (g/s)}$	ND	ND	ND	ND
SO ₂ Concentration							
Corrected to 11% O ₂	C_{s2}	mg/lbm	$C_{s2} \text{ (11% O}_2\text{)} = C_{s2} \text{ (mg/lbm)} \times (20.9 - 11) / (20.9 - C_{O2})$	ND	ND	ND	ND
Corrected to 3% O ₂	C_{s2}	mg/lbm	$C_{s2} \text{ (3% O}_2\text{)} = C_{s2} \text{ (mg/lbm)} \times (20.9 - 3) / (20.9 - C_{O2})$	ND	ND	ND	ND
Corrected to 12% CO ₂	C_{s2}	mg/lbm	$C_{s2} \text{ (12% CO}_2\text{)} = C_{s2} \text{ (mg/lbm)} \times (12 / C_{CO2})$	ND	ND	ND	ND
Nitrogen Oxides - NO _x							
NO _x Measured Concentration	C_{nox}	ppm	Measurement from Flue Gas Analyser	39.0	30.4	29.7	32.7
Uncorrected @ Ref Cond	C_{nox}	mg/lbm	$C_{nox} \text{ (mg/lbm)} = C_{nox} \text{ (ppm)} \times 1.67$	73	57	54	62
NO _x Emission Rate	ER_{nox}	g/s kg/hr	$ER_{nox} = C_{nox} / 1000 \times Q_d$ $ER_{nox} \text{ (kg/hr)} = 3.6 \times ER_{nox} \text{ (g/s)}$	2.58 9.2	1.85 6.7	1.71 6.2	2.04 7.3
NO _x Concentration							
Corrected to 11% O ₂	C_{nox}	mg/lbm	$C_{nox} \text{ (11% O}_2\text{)} = C_{nox} \text{ (mg/lbm)} \times (20.9 - 11) / (20.9 - C_{O2})$	82	79	74	78
Corrected to 3% O ₂	C_{nox}	mg/lbm	$C_{nox} \text{ (3% O}_2\text{)} = C_{nox} \text{ (mg/lbm)} \times (20.9 - 3) / (20.9 - C_{O2})$	148	143	134	142
Corrected to 12% CO ₂	C_{nox}	mg/lbm	$C_{nox} \text{ (12% CO}_2\text{)} = C_{nox} \text{ (mg/lbm)} \times (12 / C_{CO2})$	138	128	121	128
Carbon Monoxide - CO							
CO Measured Concentration	C_{co}	ppm	Measurement from Flue Gas Analyser	584	936	882	801
Uncorrected @ Ref Cond	C_{co}	mg/lbm	$C_{co} \text{ (mg/lbm)} = C_{co} \text{ (ppm)} \times 1.146$	689	1072	1010	917
CO Emission Rate	ER_{co}	g/s kg/hr	$ER_{co} = C_{co} / 1000 \times Q_d$ $ER_{co} \text{ (kg/hr)} = 3.6 \times ER_{co} \text{ (g/s)}$	23.3 83.9	34.59 124.5	31.98 115.0	30.0 107.8
CO Concentration							
Corrected to 11% O ₂	C_{co}	mg/lbm	$C_{co} \text{ (11% O}_2\text{)} = C_{co} \text{ (mg/lbm)} \times (20.9 - 11) / (20.9 - C_{O2})$	750	1485	1389	1208
Corrected to 3% O ₂	C_{co}	mg/lbm	$C_{co} \text{ (3% O}_2\text{)} = C_{co} \text{ (mg/lbm)} \times (20.9 - 3) / (20.9 - C_{O2})$	1355	2685	2512	2184
Corrected to 12% CO ₂	C_{co}	mg/lbm	$C_{co} \text{ (12% CO}_2\text{)} = C_{co} \text{ (mg/lbm)} \times (12 / C_{CO2})$	1234	2401	2289	1988
Particulate Concentration	C_p	mg/lbm	$C_p = M_p / V_{sc}$	146.2	204	189.0	179.8
Particulate Emission Rate	ER_p	g/s kg/hr	$ER_p = C_p / 1000 \times Q_d$ $ER_p \text{ (kg/hr)} = 3.6 \times ER_p \text{ (g/s)}$	5.10 18.3	6.59 23.7	5.98 21.5	5.89 21.2
Particulate Concentration							
Corrected to 11% O ₂	C_p	mg/lbm	$C_p \text{ (11% O}_2\text{)} = C_p \times (20.9 - 11) / (20.9 - C_{O2})$	184	283	259.9	236.8
Corrected to 3% O ₂	C_p	mg/lbm	$C_p \text{ (3% O}_2\text{)} = C_p \times (20.9 - 3) / (20.9 - C_{O2})$	298	512	470	428
Corrected to 12% CO ₂	C_p	mg/lbm	$C_p \text{ (12% CO}_2\text{)} = C_p \times (12 / C_{CO2})$	270	458	424	383.9

Legend:
 sq.ft - square feet
 sq.m - square metres
 °F - 1.142
 R - degrees Rankine
 ppm - parts per million

in.Hg - inches of mercury
 cu.ft - cubic feet
 scfm - cubic feet
 Ref Cond - reference temperature and pressure (25 °C and 101.3 kPa)
 acfm - dry reference cubic metres per second
 Rcfm - dry reference cubic feet per minute

mg/lbm - milligrams per dry reference cubic metre
 g/s - grams per second
 NO_x - as NO₂
 acfm - actual cubic feet per minute

OFFICIAL STACK TESTING RESULTS

Northern Pulp

Power Boiler

Fuel: Biomass

Operating Conditions: Normal

Emission Control Equipment: Scrubber

Stack Diameter: 1.83 m

Parameter	Test 1	Test 2	Test 3	Average	NSENV Limits
Test ID					
Test Date	PM-1 19-Aug-14	PM-2 19-Aug-14	PM-3 20-Aug-14	- -	- -
Stack Gas Temperature (C)					
Moisture Content (%)	81	63	82	82	-
Velocity (m/s)	19.0	19.9	18.40	19.1	-
Velumetric Flow (Rcms)	18.3	17.2	16.6	17.4	-
	34.9	32.3	31.8	32.9	-
Oxygen - O2 (%)					
Carbon Dioxide - CO2 (%)	12.1	13.8	13.7	13.2	-
	8.50	5.38	5.34	5.73	-
Sulphur Dioxide - SO2					
SO2 Measured Concentration (ppm)					
Uncorrected at Ref Cond (mg/Rcm)	ND	ND	ND	ND	-
Emission Rate (kg/hr)	ND	ND	ND	ND	-
	ND	ND	ND	ND	-
Nitrogen Oxides - NOx					
NOx Measured Concentration (ppm)					
Uncorrected at Ref Cond (mg/Rcm)	39.0	30.4	28.7	32.7	-
Emission Rate (kg/hr)	73.4	57.3	54.0	61.8	-
	9.21	6.85	6.15	7.34	-
Carbon Monoxide - CO					
CO Measured Concentration (ppm)					
Uncorrected at Ref Cond (mg/Rcm)	584	936	882	801	-
Emission Rate (kg/hr)	889	1072	1010	917	-
	83.9	125	115	108	-
Particulate Matter - PM					
Uncorrected at Ref Cond (mg/Rcm)					
PM - Corrected to 11% O2 (mg/Rcm)	148	204	189	180	-
Particulate Emission Rate (kg/hr)	164	283	260	238	-
	18.3	23.7	21.5	21.2	150

Legend: C - degrees Celsius
m/s - metres per second
Rcms - dry reference cubic metres per second
ppm - parts per million

Ref Cond - reference temperature and pressure (25 C and 101.3 kPa)
mg/Rcm - milligrams per dry reference cubic metre
NOx - as NO2
ND - non-detectable

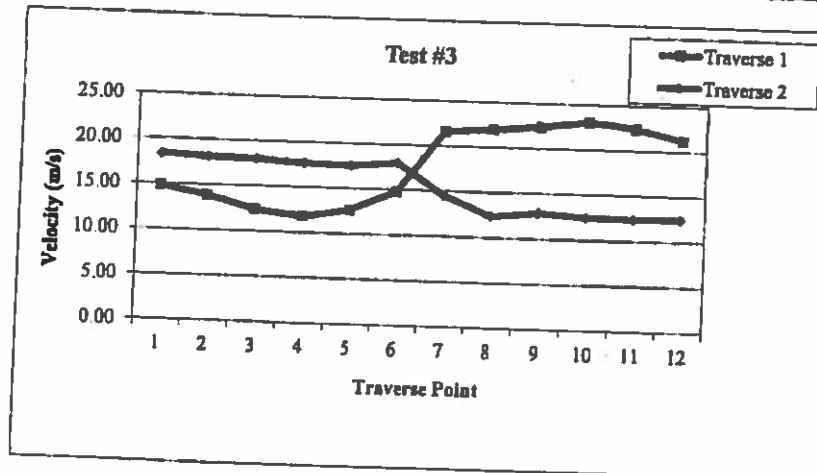
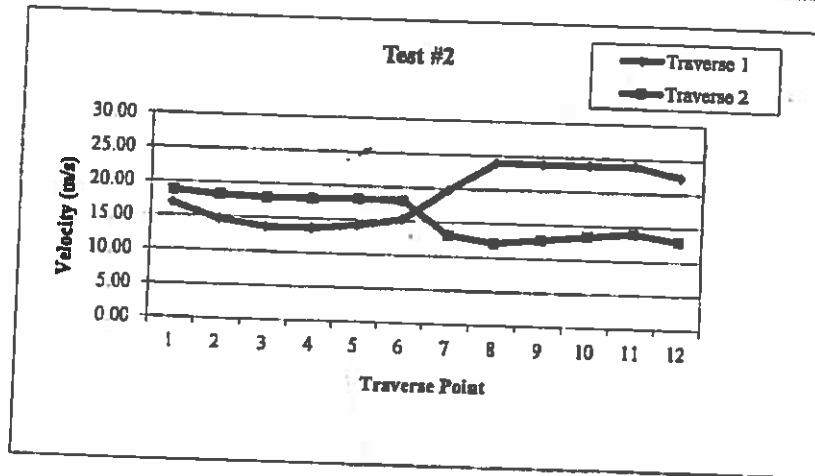
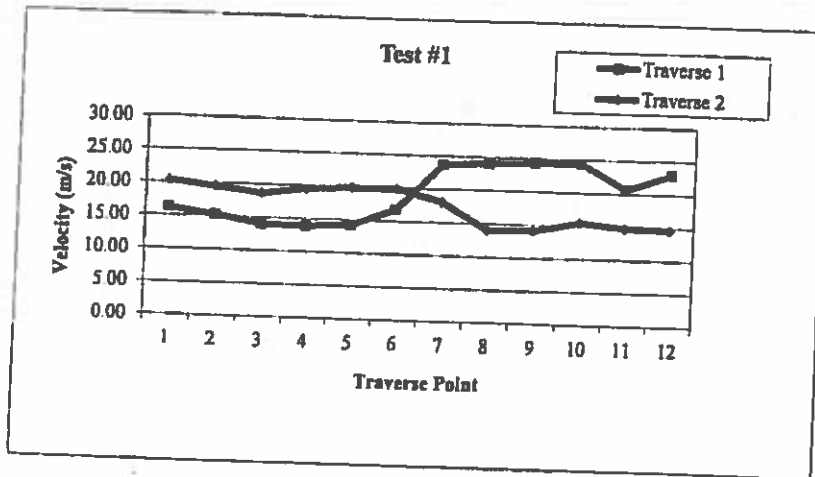
Client: Western N. Corp.
 Facility: Prison
 Location: Prison Road
 Job Number: 1-141920

Customer ID	Product ID# Attributes [6]				Sample ID	Parameters				Number (Per) Variations [6]				Uncontaminated Product Weight [g]	Contaminated Product Weight [g]
	Barcode [12]		Barcode [12]			Jar Temp [°C]	Sample Count/Total [g]	Percent Water	Total Volume	Assigned by		Average			
	Total 4	Total 3	Total 4	Total 3											
W8	112-1872	112-1874	112-1871	112-1873	94-1	454.2	8.7	8.7	112-1828	112-1830	112-1829	0.0208	0.0569		
CR	107-1800	107-1802	107-1801	107-1803	71-3	389.4	17.1	17.1	107-1804	107-1805	107-1804	0.0342	0.0942		
15	107-1806	107-1807	107-1808	107-1809	702-2	521.3	18.4	18.4	107-1800	107-1801	107-1800	0.0364	0.0983		
26	108-0487	108-0482	108-0485	108-0486	88	273.3	8.9	273.3	108-0482	108-0485	108-0484	0.0309	0.020053		

Candidate ID	Student Test Weights by Date				Sample ID	Responses			Total Answered	Gradebook Final Weights (g)			Unanswered Percentage Weight (g)	Corrected Percentage Weight (g)
	Assigned for		Total	Jan 6 Answered		Jan 7 Answered	Jan 8 Answered	Total Answered		Date		Unanswered Percentage Weight (g)		
	Test 1	Test 2								Test 3	Test 1			
V4	111,037/4	111,039/8	111,037/4	204.2	208.4	207.9	620.5	111,037/4	111,039/8	111,037/4	0.0147	0.0147		
V5	113,714/4	113,714/4	113,714/4	378.1	380.0	378.2	1137.3	113,728/9	113,710	113,720/9	0.0065	0.0065		
X1	112,380/5	112,381	112,384/4	381.7	384.4	387.3	1147.4	112,451/9	112,450/9	112,450/9	5.97/9	5.97/9		
V7	109,124/9	109,124/4	109,124/7	477.7	374.3	391.0	1243.0	109,124/3	109,124/4	109,124/4	0.00000	0.00000		
Summary of All Candidates: 109,124/9 109,124/4 109,124/7 477.7 374.3 391.0 1243.0 109,124/3 109,124/4 109,124/4 0.00000 0.00000														

Father ID	Pro Members (%)			Sample ID	Pro Members (d)			Parent male weight (sum) (kg)
	Assigned to				Assigned to			
	Test 1	Test 2	Test 3		Test 1	Test 2	Test 3	
D008-34	0.4156	0.4159	0.4090	PM-1	0.4200	0.4311	0.4332	0.2148
D034-15	0.2662	0.2690	0.2551	PM-2	0.2645	0.2640	0.2458	0.2977
D034-11	0.3618	0.3590	0.3519	PM3-1	0.4080	0.4072	0.4080	0.3410
D038-10	0.3417	0.3415	0.3415	PM3-2	0.2418	0.2425	0.2428	0.1810

Stack Gas Velocity Profiles
Power Boiler



Summary of RAW DATA

Client: Northern Pulp
 Project No.: 12181288
 Block: HLRV
 Test No.: 1

Year	Day	Hour	O ₂	CO ₂	CO	SO ₂	THS+SO2	THS	Year	Day	Hour	O ₂	CO ₂	CO	SO ₂	THS+SO2	THS
(AMST)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(AMST)	(%)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	
2014	121	1300	20.42	0.280	143.3	-0.270	63.3	64.130	2014	221	121	20.43	0.34	144.3	-0.134	70.3	71.710
2014	121	1301	20.44	0.280	143.3	-0.270	63.3	64.130	2014	221	122	20.43	0.330	143.1	-0.250	70.3	71.710
2014	121	1302	20.44	0.280	143.3	-0.270	63.3	64.130	2014	221	123	20.42	0.320	143.1	-0.130	71.3	71.710
2014	121	1303	20.44	0.290	143	-0.271	63.23	64.281	2014	221	124	20.43	0.294	137	-0.110	71.3	71.710
2014	121	1304	20.42	0.311	139	-0.170	64.64	65.020	2014	221	125	20.43	0.31	137.7	-0.06	71.4	71.64
2014	121	1305	20.43	0.337	143.4	-0.488	63.57	64.580	2014	221	126	20.41	0.322	135.2	-0.016	71.7	71.710
2014	121	1306	20.43	0.33	137.1	-0.344	64.15	64.524	2014	221	127	20.43	0.326	136.7	-0.177	71.1	71.777
2014	121	1307	20.42	0.320	138	-0.415	65	65.411	2014	221	128	20.41	0.314	135.4	-0.409	71.4	71.680
2014	121	1311	21.41	0.321	137.9	-0.44	64.78	65.10	2014	221	129	20.36	0.317	130.3	-0.170	70	71.710
2014	121	1310	20.42	0.336	138.3	-0.170	65.05	65.239	2014	221	130	20.41	0.32	130	-0.15	71.5	71.65
2014	121	1310	20.42	0.336	138.3	-0.170	65.05	65.239	2014	221	131	20.41	0.32	130.5	-0.041	71.3	71.701
2014	121	1311	20.41	0.310	138.3	-0.180	64.51	64.813	2014	221	132	20.43	0.32	129.4	-0.007	71.70	71.801
2014	121	1311	20.41	0.310	138.3	-0.180	64.51	64.813	2014	221	133	20.43	0.320	128.7	-0.117	71	71.707
2014	121	1312	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	134	20.43	0.321	128.5	-0.044	70.2	71.690
2014	121	1313	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	135	20.41	0.324	128.5	-0.701	70.4	71.631
2014	121	1314	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	136	20.41	0.320	127	-0.410	71.3	71.590
2014	121	1315	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	137	20.41	0.320	126.5	-0.370	71.3	71.590
2014	121	1316	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	138	20.41	0.320	125.7	-0.310	71.3	71.590
2014	121	1317	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	139	20.41	0.320	124.7	-0.310	71.3	71.590
2014	121	1318	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	140	20.41	0.320	123.7	-0.310	71.3	71.590
2014	121	1319	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	141	20.41	0.320	122.7	-0.310	71.3	71.590
2014	121	1320	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	142	20.41	0.320	121.7	-0.310	71.3	71.590
2014	121	1321	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	143	20.41	0.320	120.7	-0.310	71.3	71.590
2014	121	1322	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	144	20.41	0.320	119.7	-0.310	71.3	71.590
2014	121	1323	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	145	20.41	0.320	118.7	-0.310	71.3	71.590
2014	121	1324	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	146	20.41	0.320	117.7	-0.310	71.3	71.590
2014	121	1325	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	147	20.41	0.320	116.7	-0.310	71.3	71.590
2014	121	1326	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	148	20.41	0.320	115.7	-0.310	71.3	71.590
2014	121	1327	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	149	20.41	0.320	114.7	-0.310	71.3	71.590
2014	121	1328	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	150	20.41	0.320	113.7	-0.310	71.3	71.590
2014	121	1329	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	151	20.41	0.320	112.7	-0.310	71.3	71.590
2014	121	1330	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	152	20.41	0.320	111.7	-0.310	71.3	71.590
2014	121	1331	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	153	20.41	0.320	110.7	-0.310	71.3	71.590
2014	121	1332	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	154	20.41	0.320	109.7	-0.310	71.3	71.590
2014	121	1333	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	155	20.41	0.320	108.7	-0.310	71.3	71.590
2014	121	1334	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	156	20.41	0.320	107.7	-0.310	71.3	71.590
2014	121	1335	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	157	20.41	0.320	106.7	-0.310	71.3	71.590
2014	121	1336	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	158	20.41	0.320	105.7	-0.310	71.3	71.590
2014	121	1337	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	159	20.41	0.320	104.7	-0.310	71.3	71.590
2014	121	1338	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	160	20.41	0.320	103.7	-0.310	71.3	71.590
2014	121	1339	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	161	20.41	0.320	102.7	-0.310	71.3	71.590
2014	121	1340	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	162	20.41	0.320	101.7	-0.310	71.3	71.590
2014	121	1341	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	163	20.41	0.320	100.7	-0.310	71.3	71.590
2014	121	1342	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	164	20.41	0.320	99.7	-0.310	71.3	71.590
2014	121	1343	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	165	20.41	0.320	98.7	-0.310	71.3	71.590
2014	121	1344	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	166	20.41	0.320	97.7	-0.310	71.3	71.590
2014	121	1345	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	167	20.41	0.320	96.7	-0.310	71.3	71.590
2014	121	1346	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	168	20.41	0.320	95.7	-0.310	71.3	71.590
2014	121	1347	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	169	20.41	0.320	94.7	-0.310	71.3	71.590
2014	121	1348	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	170	20.41	0.320	93.7	-0.310	71.3	71.590
2014	121	1349	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	171	20.41	0.320	92.7	-0.310	71.3	71.590
2014	121	1350	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	172	20.41	0.320	91.7	-0.310	71.3	71.590
2014	121	1351	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	173	20.41	0.320	90.7	-0.310	71.3	71.590
2014	121	1352	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	174	20.41	0.320	89.7	-0.310	71.3	71.590
2014	121	1353	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	175	20.41	0.320	88.7	-0.310	71.3	71.590
2014	121	1354	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	176	20.41	0.320	87.7	-0.310	71.3	71.590
2014	121	1355	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	177	20.41	0.320	86.7	-0.310	71.3	71.590
2014	121	1356	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	178	20.41	0.320	85.7	-0.310	71.3	71.590
2014	121	1357	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	179	20.41	0.320	84.7	-0.310	71.3	71.590
2014	121	1358	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	180	20.41	0.320	83.7	-0.310	71.3	71.590
2014	121	1359	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	181	20.41	0.320	82.7	-0.310	71.3	71.590
2014	121	1360	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	182	20.41	0.320	81.7	-0.310	71.3	71.590
2014	121	1361	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	183	20.41	0.320	80.7	-0.310	71.3	71.590
2014	121	1362	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	184	20.41	0.320	79.7	-0.310	71.3	71.590
2014	121	1363	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	185	20.41	0.320	78.7	-0.310	71.3	71.590
2014	121	1364	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	186	20.41	0.320	77.7	-0.310	71.3	71.590
2014	121	1365	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	187	20.41	0.320	76.7	-0.310	71.3	71.590
2014	121	1366	20.41	0.315	138.7	-0.433	64.7	65.111	2014	221	188	20.41	0.320	75.7	-0.310	71.3	71.590
2014	121	1367	20.41														

Client: Northern Pulp
Project No.: 121819249
Stack: HLRV
Test No.: 1

Year	Day (Julian)	Hour	O ₃ [m]	CO ₂ [ppm]	CO [ppmv]	SO ₂ [ppmv]	THO+OCS [ppmv]	THO [ppmv]	Year	Day (Julian)	Hour	O ₃ [m]	CO ₂ [ppm]	CO [ppmv]	SO ₂ [ppmv]	THO+OCS [ppmv]	THO [ppmv]
2011	2011	1200	20.43	0.23	126.7	-4.391	70.3	75.091	2014	212	201	20.49	0.239	141.7	-4.094	70.3	77.339
2011	201	1201	20.43	0.232	126.7	-4.391	70.3	75.091	2014	213	202	20.49	0.234	141.6	-4.094	70.3	77.340
2011	202	1202	20.43	0.232	126.7	-4.391	70.3	75.091	2014	214	203	20.42	0.231	141.8	-4.094	70.3	76.308
2011	203	1203	20.44	0.241	127.0	-4.390	69.64	75.020	2014	215	204	20.43	0.23	140.7	-4.094	70.3	76.308
2011	204	1204	20.44	0.241	127.0	-4.391	69.64	75.021	2014	216	205	20.41	0.224	139.8	-4.094	70.3	76.308
2011	205	1205	20.44	0.241	127.0	-4.391	69.64	75.021	2014	217	206	20.41	0.219	138.5	-4.094	70.3	76.308
2011	206	1206	20.44	0.241	127.0	-4.391	69.64	75.021	2014	218	207	20.43	0.214	140.7	-4.094	70.3	76.308
2011	207	1207	20.44	0.241	127.0	-4.391	69.64	75.021	2014	219	208	20.41	0.219	138.5	-4.094	70.3	76.308
2011	208	1208	20.44	0.241	127.0	-4.391	69.64	75.021	2014	220	209	20.43	0.214	140.7	-4.094	70.3	76.308
2011	209	1209	20.44	0.241	127.0	-4.391	69.64	75.021	2014	221	210	20.41	0.219	138.5	-4.094	70.3	76.308
2011	210	1210	20.44	0.241	127.0	-4.391	69.64	75.021	2014	222	211	20.43	0.214	140.7	-4.094	70.3	76.308
2011	211	1211	20.44	0.241	127.0	-4.391	69.64	75.021	2014	223	212	20.41	0.219	138.5	-4.094	70.3	76.308
2011	212	1212	20.44	0.241	127.0	-4.391	69.64	75.021	2014	224	213	20.43	0.214	140.7	-4.094	70.3	76.308
2011	213	1213	20.44	0.241	127.0	-4.391	69.64	75.021	2014	225	214	20.41	0.219	138.5	-4.094	70.3	76.308
2011	214	1214	20.44	0.241	127.0	-4.391	69.64	75.021	2014	226	215	20.43	0.214	140.7	-4.094	70.3	76.308
2011	215	1215	20.44	0.241	127.0	-4.391	69.64	75.021	2014	227	216	20.41	0.219	138.5	-4.094	70.3	76.308
2011	216	1216	20.44	0.241	127.0	-4.391	69.64	75.021	2014	228	217	20.43	0.214	140.7	-4.094	70.3	76.308
2011	217	1217	20.44	0.241	127.0	-4.391	69.64	75.021	2014	229	218	20.41	0.219	138.5	-4.094	70.3	76.308
2011	218	1218	20.44	0.241	127.0	-4.391	69.64	75.021	2014	230	219	20.43	0.214	140.7	-4.094	70.3	76.308
2011	219	1219	20.44	0.241	127.0	-4.391	69.64	75.021	2014	231	220	20.41	0.219	138.5	-4.094	70.3	76.308
2011	220	1220	20.44	0.241	127.0	-4.391	69.64	75.021	2014	232	221	20.43	0.214	140.7	-4.094	70.3	76.308
2011	221	1221	20.44	0.241	127.0	-4.391	69.64	75.021	2014	233	222	20.41	0.219	138.5	-4.094	70.3	76.308</

Client: Northern Pulp
Project No.: 121811200
Stock: HLMV
Test No.: 1

Year	Day (Julian)	Hour	O ₃ (Pa)	CO ₂ (Pa)	CO (ppmv)	SO ₂ (ppmv)	THO-NOX (ppmv)	THO (ppmv)	Year	Day (Julian)	Hour	O ₃ (Pa)	CO ₂ (Pa)	CO (ppmv)	SO ₂ (ppmv)	THO-NOX (ppmv)	THO (ppmv)
2004	711	1649	10.41	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	712	1649	10.42	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	713	1649	10.43	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	714	1649	10.44	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	715	1649	10.45	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	716	1649	10.46	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	717	1649	10.47	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	718	1649	10.48	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	719	1649	10.49	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	720	1649	10.50	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	721	1649	10.51	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	722	1649	10.52	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	723	1649	10.53	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	724	1649	10.54	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	725	1649	10.55	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	726	1649	10.56	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	727	1649	10.57	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	728	1649	10.58	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	729	1649	10.59	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	730	1649	10.60	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	731	1649	10.61	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296
2004	732	1649	10.62	0.238	3.693	-4.456	177.8	181.296	2004	332	421	10.48	0.233	3.683	-4.768	193	181.296

Summary of RAW DATA

Client: Northern Pipe
Project No.: 121811283
Stack: HLRV
Test No.: 1

Year	Day	Hour	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	THS+SO ₂ (ppm)	THS (ppm)	Year	Day	Hour	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	THS+SO ₂ (ppm)	THS (ppm)
2014	231	1800	20.44	0.239	141.3	-4.875	76.1	76.779	2014	231	251	20.43	0.247	141.3	-4.811	76.1	81.811
2014	231	1801	20.43	0.23	141.3	-4.854	75.9	82.754	2014	231	252	20.44	0.234	141.3	-4.875	76.3	84.875
2014	231	1802	20.44	0.233	141.3	-4.171	76.3	81.871	2014	231	253	20.44	0.236	141.3	-4.864	76.6	85.864
2014	231	1803	20.43	0.231	140.8	-4.185	76.8	81.883	2014	231	254	20.44	0.238	141.7	-4.116	83.8	90.346
2014	231	1804	20.44	0.235	140.7	-4.731	77.7	83.491	2014	231	255	20.44	0.238	141.3	-4.838	127.5	112.338
2014	231	1805	20.44	0.23	142.7	-4.821	76	86.821	2014	231	256	20.44	0.238	141.3	-4.214	86.9	86.154
2014	231	1806	20.43	0.238	140.4	-4.368	76.1	82.498	2014	231	257	20.44	0.236	140.9	-4.807	79.4	84.387
2014	231	1807	20.44	0.235	141.1	-4.888	75.8	81.583	2014	231	258	20.44	0.234	139.8	-4.172	90.9	86.871
2014	231	1808	20.43	0.22	141.1	-4.398	77.8	83.898	2014	231	259	20.43	0.231	139.7	-4.488	82.7	87.898
2014	231	1809	20.43	0.238	139.9	-4.28	76.1	82.32	2014	231	260	20.43	0.232	141.8	-4.865	81.9	86.385
2014	231	1810	20.43	0.231	141.8	-4.879	85.88	84.888	2014	231	261	20.43	0.232	142.3	-5.329	81.4	87.929
2014	231	1811	20.43	0.231	140.5	-4.894	84.91	85.895	2014	231	262	20.44	0.231	141.8	-4.749	85.9	86.849
2014	231	1812	20.43	0.236	140.3	-4.19	81.34	86.88	2014	231	263	20.44	0.237	140.4	-4.886	79.5	85.264
2014	231	1813	20.43	0.236	141.8	-4.289	80.1	84.389	2014	231	264	20.43	0.23	139.6	-4.184	79.5	85.754
2014	231	1814	20.43	0.243	141.8	-4.888	83.42	84.233	2014	231	265	20.44	0.236	140.4	-4.889	80.4	85.889
2014	231	1815	20.43	0.248	141.8	-4.968	84.12	84.873	2014	231	266	20.43	0.239	140.4	-4.288	81.1	87.361
2014	231	1816	20.43	0.238	141	-4.371	83.91	83.891	2014	231	267	20.44	0.234	140.8	-4.144	79.3	84.344
2014	231	1817	20.43	0.231	140	-4.179	84.84	85.824	2014	231	268	20.44	0.239	140	-4.184	79.4	85.284
2014	231	1818	20.43	0.237	141.8	-4.884	83.87	84.388	2014	231	269	20.44	0.239	140.3	-4.115	79.7	85.215
2014	231	1819	20.43	0.23	141.1	-4.164	84.13	84.924	2014	231	270	20.44	0.23	140.3	-4.268	79.5	84.788
2014	231	1820	20.43	0.239	140	-4.813	88	85.413	2014	231	271	20.44	0.23	140.7	-4.8	79.8	85.288
2014	231	1821	20.43	0.231	137.9	-4.64	84.75	85.39	2014	231	272	20.44	0.237	142.1	-4.883	118.4	112.483
2014	231	1822	20.43	0.234	140.4	-4.179	83.89	85.289	2014	231	273	20.44	0.23	140.8	-4.788	80.8	85.888
2014	231	1823	20.43	0.238	140.3	-4.179	84.83	84.349	2014	231	274	20.44	0.237	140.4	-4.364	80.8	85.864
2014	231	1824	20.43	0.238	139.3	-4.184	84.84	84.727	2014	231	275	20.44	0.234	140.4	-4.124	79.7	84.824
2014	231	1825	20.43	0.231	140.3	-4.134	84.7	85.133	2014	231	276	20.44	0.236	140.4	-4.408	79.4	84.888
2014	231	1826	20.43	0.235	140.7	-4.633	84.4	85.888	2014	231	277	20.44	0.239	140.4	-4.811	79.8	85.311
2014	231	1827	20.43	0.238	139.3	-4.884	84.83	85.414	2014	231	278	20.44	0.237	140.7	-4.474	80.8	85.778
2014	231	1828	20.43	0.238	139.7	-4.885	83.81	84.135	2014	231	279	20.44	0.233	140	-4.381	80.3	85.381
2014	231	1829	20.44	0.238	141.3	-4.878	86.78	84.254	2014	231	280	20.47	0.23	140.8	-4.14	79.8	84.84
2014	231	1830	20.43	0.238	140.8	-4.77	85.81	84.36	2014	231	281	20.44	0.231	140.4	-4.888	79.8	85.788
2014	231	1831	20.43	0.234	140.3	-4.88	83.17	84.16	2014	231	282	20.43	0.23	140.4	-4.888	238.6	238.628
2014	231	1832	20.43	0.234	141.3	-4.188	83.18	83.398	2014	231	283	20.43	0.239	142.3	-5.34	231.8	231.864
2014	231	1833	20.44	0.238	140	-4.188	84.83	84.838	2014	231	284	20.44	0.237	140.8	-4.883	81.4	87.883
2014	231	1834	20.43	0.239	140.3	-4.188	83.81	83.811	2014	231	285	20.43	0.233	140.3	-4.12	79.8	85.82
2014	231	1835	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	286	20.43	0.238	140.3	-4.188	80.3	85.818
2014	231	1836	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	287	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1837	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	288	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1838	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	289	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1839	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	290	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1840	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	291	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1841	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	292	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1842	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	293	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1843	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	294	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1844	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	295	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1845	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	296	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1846	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	297	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1847	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	298	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1848	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	299	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1849	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	300	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1850	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	301	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1851	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	302	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1852	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	303	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1853	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	304	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1854	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	305	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1855	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	306	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1856	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	307	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1857	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	308	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1858	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	309	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1859	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	310	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1900	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	311	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1901	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	312	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1902	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	313	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1903	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	314	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1904	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	315	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1905	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	316	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1906	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	317	20.43	0.233	140.8	-4.188	79	85.818
2014	231	1907	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	318	20.43	0.237	140.7	-4.187	80.3	84.827
2014	231	1908	20.43	0.238	140.3	-4.188	83.81	83.811	2014	231	319	20.43	0.233	14			

Client: Northern Pip
Project No.: 121511259
Stock: HJTV
Test No.: 1

Year	Day (Julian)	Hour	O ₁ (%)	CO ₂ (%)	CO (ppmv)	SO ₂ (ppmv)	Tras-SO ₂ (ppmv)	TRO (ppmv)
2021	111	2020	20.81	0.21	117	-1.136	60.66	60.74
2021	719	1801	20.81	0.21	117.0	-1.136	61.11	61.09
2020	203	1991	20.81	0.21	116.3	-1.171	61.77	61.69
2020	215	2000	20.81	0.23	116.7	-1.015	61.65	61.67
2020	111	2020	20.81	0.224	118	-1.308	60.29	60.40
2020	101	1998	20.81	0.229	116.8	-1.348	60.26	61.00
2020	261	1998	20.81	0.223	116.1	-1.407	60.5	61.007
2020	275	1997	20.81	0.225	116.4	-1.353	60.8	61.119
2020	341	1998	20.81	0.218	116.6	-1.148	60.77	61.016
2020	111	2020	20.81	0.224	116.8	-1.062	60.11	60.11
2020	111	2000	20.81	0.222	117.1	-1.154	60.98	60.81
2020	211	1941	20.81	0.222	116.8	-1.107	60.8	61.007
2020	111	1902	20.81	0.21	120.4	-1.259	60.03	61.000
2020	111	1904	20.81	0.221	116.4	-1.154	60.98	61.004
2020	111	1904	20.81	0.229	119.9	-1.001	61.00	61.078
2020	201	1906	20.81	0.23	121	-1.058	60.47	61.163
2020	111	1906	20.81	0.228	118.3	-1.204	60.27	61.016
2020	111	1907	20.81	0.236	119.7	-1.019	61.47	61.009
2020	111	1908	20.81	0.239	119.2	-1.177	60.8	61.077
2020	111	1908	20.81	0.238	119.4	-1.048	60.8	61.055
2020	111	1909	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1910	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1911	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1912	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1913	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1914	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1915	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1916	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1917	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1918	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1919	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1920	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1921	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1922	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1923	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1924	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1925	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1926	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1927	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1928	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1929	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1930	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1931	20.81	0.233	119.1	-1.058	60.8	61.055
2020	111	1932	20.81	0.233	1			

Year	Day [dd/mm]	Hour	O ₃ [ppb]	CO ₂ [ppm]	CO [ppmv]	NO ₂ [ppbv]	TRP+NO2 [ppbv]	TRP [ppbv]
2010	283	721	20.60	0.134	100.0	-0.139	0.0	17.000
2010	287	723	20.60	0.132	100.3	-0.139	0.0	17.170
2010	291	724	20.60	0.133	100.1	-0.131	0.0	16.800
2010	295	724	20.60	0.137	100.0	-0.125	0.0	16.820
2010	298	726	20.60	0.121	100	-0.100	0.0	16.800
2010	301	731	20.60	0.135	100	-0.100	0.0	16.900
2010	304	736	20.60	0.119	100	-0.050	0.0	16.820
2010	308	738	20.60	0.123	100.0	-0.100	0.0	16.800
2010	311	740	20.60	0.123	100	-0.111	0.0	16.800
2010	315	740	20.60	0.120	100.7	-0.10	0.0	16.80
2010	318	739	20.60	0.127	100.7	-0.11	0.0	16.80
2010	322	739	20.60	0.127	100.7	-0.11	0.0	16.80
2010	325	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	328	739	20.60	0.129	100	-0.100	0.0	16.800
2010	331	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	335	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	338	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	342	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	345	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	348	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	352	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	355	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	358	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	362	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	365	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	368	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	372	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	375	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	378	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	382	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	385	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	388	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	392	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	395	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	398	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	402	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	405	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	408	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	412	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	415	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	418	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	422	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	425	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	428	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	432	739	20.60	0.129	100.7	-0.102	0.0	16.800
2010	435	739	20.					

Summary of RAW DATA

Client: Northern Pulp
Project No.: 121811268
Stack: HLRV
Test No.: 1

Year	Day (Julian)	Hour	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	THS+SO ₂ (ppm)	THS (ppm)	Year	Day (Julian)	Hour	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	THS+SO ₂ (ppm)	THS (ppm)
2014	111	2100	20.44	0.224	143	-0.273	60.23	60.501	2014	211	231	20.21	0.262	166.8	-7.04	60.6	60.64
2014	111	2101	20.43	0.221	136	-0.179	64.84	65.019	2014	211	232	20.23	0.252	153.2	-7.03	60.8	60.82
2014	111	2102	20.41	0.217	140.4	-0.020	63.87	64.008	2014	211	233	20.40	0.236	168.1	-7.70	61.2	61.29
2014	111	2103	20.43	0.219	137.2	-0.244	64.16	64.314	2014	211	234	20.5	0.225	152.2	-7.26	60.8	60.86
2014	111	2104	20.42	0.220	136	-0.413	66	66.413	2014	211	235	20.49	0.234	151.2	-7.40	60.8	60.82
2014	111	2105	20.41	0.231	137.0	-0.44	64.70	65.10	2014	211	236	20.5	0.223	160.2	-7.36	60.8	60.86
2014	111	2106	20.43	0.224	141.2	-0.041	62.57	62.612	2014	211	237	20.21	0.222	154.2	-7.11	61	61.11
2014	111	2107	20.41	0.220	140.8	0.23	60.20	60.43	2014	211	238	20.40	0.226	151.4	-6.007	60.4	60.507
2014	111	2108	20.43	0.221	139.2	-0.130	62.25	62.320	2014	211	239	20.31	0.220	166.4	-7.20	61.2	61.29
2014	111	2109	20.41	0.223	144.6	-0.201	64.20	64.401	2014	211	240	20.42	0.216	159.8	-6.54	107.9	112.74
2014	111	2110	20.4	0.218	147.2	0.001	64.30	64.301	2014	211	241	20.48	0.212	157.1	-7.36	61.8	61.82
2014	111	2111	20.41	0.224	140	-0.27	62.20	62.47	2014	211	242	20.49	0.206	157.5	-7.03	60.3	60.505
2014	111	2112	20.4	0.212	140.4	-0.094	60.79	60.888	2014	211	243	20.5	0.214	153.8	-6.44	61.2	61.24
2014	111	2113	20.4	0.210	140.8	-0.214	64.71	64.94	2014	211	244	20.5	0.203	152.3	-7.06	60.8	60.86
2014	111	2114	20.42	0.208	139.7	-0.230	64	64.19	2014	211	245	20.5	0.217	152.3	-7.06	60.8	60.86
2014	111	2115	20.43	0.206	138.9	0.009	64.10	64.109	2014	211	246	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2116	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	247	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2117	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	248	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2118	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	249	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2119	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	250	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2120	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	251	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2121	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	252	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2122	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	253	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2123	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	254	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2124	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	255	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2125	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	256	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2126	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	257	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2127	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	258	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2128	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	259	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2129	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	260	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2130	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	261	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2131	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	262	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2132	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	263	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2133	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	264	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2134	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	265	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2135	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	266	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2136	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	267	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2137	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	268	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2138	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	269	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2139	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	270	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2140	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	271	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2141	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	272	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2142	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	273	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2143	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	274	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2144	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	275	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2145	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	276	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2146	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	277	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2147	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	278	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2148	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	279	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2149	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	280	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2150	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	281	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2151	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	282	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2152	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	283	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2153	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	284	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2154	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	285	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2155	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	286	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2156	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	287	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2157	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	288	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2158	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	289	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2159	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	290	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2200	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	291	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2201	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	292	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2202	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	293	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2203	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	294	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2204	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	295	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2205	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	296	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2206	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	297	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2207	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	298	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2208	20.4	0.204	136.6	-0.170	64.70	64.71	2014	211	299	20.49	0.213	152.4	-7.06	60.8	60.86
2014	111	2209	20.4	0.204	136.6	-0.170	64.70	64.71									

Summary of RAW DATA

Client: Northern Pip
 Project No.: 121011260
 Stack: HLRV
 Test No.: 1

Year	Day	Hour	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	TRB-905 (ppm)	TRM (ppm)	Yr	Day	Hour	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	TRB-905 (ppm)	TRM (ppm)
2014	251	2239	20.44	0.294	130	-1.824	64.81	64.828	2014	252	1001	20.53	0.218	141.9	-4.25	61.9	64.9
2014	251	2235	20.41	0.298	130.9	-0.411	64.87	65.382	2014	252	1022	20.51	0.224	141.7	-4.71	61.9	64.9
2014	251	2233	20.41	0.294	130.3	-0.381	64.78	65.371	2014	252	1028	20.51	0.219	140.2	-0.21	61.5	65.71
2014	251	2231	20.45	0.291	140.1	-0.894	63.72	63.834	2014	252	1034	20.49	0.214	138.6	-0.23	61.5	65.71
2014	251	2234	20.46	0.216	147.3	-0.844	63.8	64.299	2014	252	1039	20.52	0.222	139.1	-0.18	61.4	65.76
2014	251	2235	20.41	0.298	143.3	-0.798	63.81	65.375	2014	252	1046	20.51	0.219	141	-0.21	61.2	65.81
2014	251	2236	20.41	0.297	140.3	-0.688	63.89	64.319	2014	252	1052	20.5	0.221	143.8	-0.08	61.4	65.86
2014	251	2237	20.41	0.297	140.1	-0.628	63.86	65.367	2014	252	1058	20.54	0.205	140.9	-0.24	61.1	65.84
2014	251	2238	20.44	0.234	140	-0.608	63.88	64.265	2014	252	1059	20.5	0.225	142.4	-0.25	61.6	65.75
2014	251	2239	20.41	0.295	140.5	-1.252	64.59	65.642	2014	252	1068	20.5	0.208	142.1	-0.28	61.3	65.81
2014	251	2240	20.41	0.295	140.5	-0.789	63.11	63.839	2014	252	1061	20.51	0.204	142.3	-0.4	61.3	65.8
2014	251	2241	20.41	0.295	140.5	-1.54	64.32	65.6	2014	252	1069	20.5	0.207	141.6	-0.3	61.7	65.8
2014	251	2242	20.41	0.292	140.7	-1.089	63.98	64.879	2014	252	1074	20.51	0.204	140.5	-0.29	61.1	65.89
2014	251	2243	20.41	0.292	140.7	-1.015	64.81	64.768	2014	252	1080	20.53	0.204	140.5	-0.23	61.8	65.83
2014	251	2244	20.41	0.293	139	-1.015	64.81	64.768	2014	252	1086	20.53	0.204	140	-0.24	61.8	65.83
2014	251	2245	20.41	0.293	139.4	-1.389	65.57	66.908	2014	252	1092	20.57	0.222	140.8	-0.234	61.8	65.84
2014	251	2246	20.44	0.292	140.5	-1.073	65.54	66.412	2014	252	1097	20.52	0.228	142.9	-0.23	61.6	65.83
2014	251	2247	20.44	0.298	140.5	-1.032	64.5	65.832	2014	252	1100	20.53	0.227	142.9	-0.23	61.6	65.83
2014	251	2248	20.43	0.297	139.1	-1.472	65.31	67.382	2014	252	1106	20.5	0.234	141.3	-0	61.1	65.81
2014	251	2249	20.43	0.23	141.7	-0.179	65.89	65.259	2014	252	1109	20.49	0.228	142.3	-0.057	61.4	65.87
2014	251	2250	20.43	0.23	141.7	-0.179	65.89	65.259	2014	252	1113	20.51	0.21	142.3	-0.2	61.8	65.8
2014	251	2251	20.41	0.295	139.9	-1.289	64.99	67.042	2014	252	1114	20.5	0.204	140.3	-0.72	61.2	65.82
2014	251	2252	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1118	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2253	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1124	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2254	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1130	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2255	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1136	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2256	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1142	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2257	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1148	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2258	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1154	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2259	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1160	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2300	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1166	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2301	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1172	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2302	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1178	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2303	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1184	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2304	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1190	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2305	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1196	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2306	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1202	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2307	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1208	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2308	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1214	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2309	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1220	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2310	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1226	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2311	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1232	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2312	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1238	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2313	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1244	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2314	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1250	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2315	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1256	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2316	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1262	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2317	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1268	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2318	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1274	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2319	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1280	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2320	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1286	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2321	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1292	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2322	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1298	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2323	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1304	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2324	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1310	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2325	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1316	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2326	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1322	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2327	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1328	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2328	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1334	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2329	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1340	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2330	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1346	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2331	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1352	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2332	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1358	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2333	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1364	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2334	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1370	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2335	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1376	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2336	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1382	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2337	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1388	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2338	20.44	0.292	140.7	-0.899	65.17	65.359	2014	252	1394	20.5	0.204	141	-0.14	61.3	65.84
2014	251	2339	20.44	0.292													

Client: Northern Pulp
Project No.: 121811200
Stack: HLRV
Test No.: 1

Year	Day (Julian)	Hour	O ₁ (°)	CO ₂ (%)	CO (ppmv)	SO ₂ (ppmv)	THS+OCS (ppmv)	THS (ppmv)	Year	Day (Julian)	Hour	O ₁ (°)	CO ₂ (%)	CO (ppmv)	SO ₂ (ppmv)	THS+OCS (ppmv)	THS (ppmv)
2024	221	1400	20.42	0.232	189.4	-1.953	66.82	70.682	2024	221							
2024	222	2	20.42	0.234	188	-1.845	66.84	71.428	2024	222	1131	20.5	0.234	186	-1.87	66.2	70.62
2024	223	3	20.43	0.234	186.7	-1.778	66.87	71.748	2024	223	1132	20.54	0.236	183.8	-1.89	66.2	70.62
2024	224	4	20.43	0.235	184.7	-1.696	70.3	71.888	2024	224	2150	20.5	0.125	183.4	-1.837	66.9	70.62
2024	225	5	20.43	0.237	182.7	-1.613	66.81	71.883	2024	225	1134	20.53	0.239	183	-1.85	66.2	70.62
2024	226	6	20.43	0.238	180.8	-1.527	66.7	71.477	2024	226	2151	20.53	0.232	181.3	-1.83	66.4	70.62
2024	227	7	20.43	0.239	179.3	-1.432	66.57	71.681	2024	227	1135	20.53	0.238	179	-1.87	66.5	70.62
2024	228	8	20.43	0.240	177.8	-1.332	66.57	71.681	2024	228	2152	20.54	0.236	180.3	-1.87	66.5	70.62
2024	229	9	20.43	0.238	185.3	-1.335	66.5	71.136	2024	229	1136	20.53	0.231	180.4	-1.834	66.9	70.62
2024	230	10	20.42	0.234	188.8	-1.223	70.2	72.813	2024	230	2153	20.52	0.232	181.3	-1.8	67.0	70.62
2024	231	11	20.42	0.233	186.8	-1.119	69.49	72.889	2024	231	1137	20.51	0.234	182.8	-1.877	66.7	70.62
2024	232	12	20.44	0.23	184.8	-1.132	70.2	72.332	2024	232	2154	20.51	0.231	180.8	-1.831	67.5	70.62
2024	233	13	20.43	0.235	182.7	-1.035	68.63	71.170	2024	233	1138	20.51	0.241	180.8	-1.831	66.5	70.62
2024	234	14	20.43	0.231	180.8	-0.931	68.4	71.153	2024	234	2155	20.51	0.235	180.4	-1.831	66.5	70.62
2024	235	15	20.43	0.238	180.1	-0.835	68.23	71.866	2024	235	1139	20.51	0.235	180.4	-1.837	67.9	70.62
2024	236	16	20.43	0.241	178.6	-0.735	68.36	72.82	2024	236	2156	20.51	0.238	180.8	-1.838	66.4	70.62
2024	237	17	20.43	0.246	180.6	-0.635	68.39	72.857	2024	237	1140	20.51	0.237	180.9	-1.838	66.2	70.62
2024	238	18	20.43	0.249	180.2	-0.535	68.49	72.857	2024	238	2157	20.51	0.238	180.8	-1.838	66.2	70.62
2024	239	19	20.43	0.252	179.7	-0.435	68.59	72.857	2024	239	1141	20.51	0.238	180.8	-1.838	66.2	70.62
2024	240	20	20.43	0.255	179.2	-0.335	68.69	72.857	2024	240	2158	20.51	0.238	180.8	-1.838	66.2	70.62
2024	241	21	20.43	0.258	178.7	-0.235	68.79	72.857	2024	241	1142	20.51	0.238	180.8	-1.838	66.2	70.62
2024	242	22	20.43	0.261	178.2	-0.135	68.89	72.857	2024	242	2159	20.51	0.238	180.8	-1.838	66.2	70.62
2024	243	23	20.43	0.264	177.7	-0.035	68.99	72.857	2024	243	1143	20.51	0.238	180.8			

Client: Northern Pulp
Project No.: 121511259
Stack: HLMV
Test No.: 1

Client: Northern Pulp
Project No.: 121511259
Stack: HLMV
Test No.: 1

Year	Day (Julian)	Hour	O ₂ (%)	CO ₂ (%)	DO (ppm)	NO ₃ (ppm)	TDS-POD (ppm)	TDS (ppm)	Year	Day (Julian)	Hour	O ₂ (%)	CO ₂ (%)	DO (ppm)	NO ₃ (ppm)	TDS-POD (ppm)	TDS (ppm)
2014	232	1330	28.49	0.226	140.1	-11.42	91.2	182.62	2014	232	1330	28.49	0.226	140.1	-11.42	91.2	182.62
2014	232	1321	20.51	0.232	147.3	-12.05	89.8	101.95	2014	232	1322	20.48	0.231	141.5	-11.15	90.6	101.75
2014	232	1323	20.5	0.232	145.8	-11.09	90.9	101.99	2014	232	1324	20.5	0.238	144.9	-10.91	89.9	100.91
2014	232	1325	20.5	0.234	142.8	-12.03	89.6	101.63	2014	232	1326	20.5	0.232	146.5	-11.57	90.2	101.77
2014	232	1327	20.5	0.231	148.3	-10.55	89.8	100.35	2014	232	1328	20.51	0.246	150.8	-11.32	88.5	99.82
2014	232	1329	20.51	0.238	146.8	-11.79	89.4	101.19	2014	232	1330	20.5	0.239	143.6	-10.98	89.8	100.78

SUMMARY OF CORRECTED DATA

Client: Northern Poly
Project No.: 121811300
Street: HLTV
Test No.: 1

[illegible]

Client:	Northern Pol
Project No.:	12161200
Station:	HLRV
Test No.:	1

Year	Day	Hour	Q1	Q2	Q3	Q4	TS0 + TS2	TS0 - TS2	TS0 + TS2	TS0 - TS2	Year	Day	Hour	Q1	Q2	Q3	Q4	TS0 + TS2	TS0 - TS2	TS0 + TS2	TS0 - TS2
Year	Day	Hour	Q1	Q2	Q3	Q4	TS0 + TS2	TS0 - TS2	TS0 + TS2	TS0 - TS2	Year	Day	Hour	Q1	Q2	Q3	Q4	TS0 + TS2	TS0 - TS2	TS0 + TS2	TS0 - TS2
2014	201	1010	20.20	0.24	102.70	2.10	104.60	88.23			2014	202	120	20.20	0.10	102.60	1.10	71.74	71.61	88.75	
2014	201	1010	20.20	0.20	101.85	2.00	103.64	88.21			2014	202	140	20.20	0.20	101.95	1.20	68.26	67.20	88.75	
2014	201	1000	20.20	0.20	101.85	2.00	103.64	87.20			2014	202	160	20.20	0.20	101.95	1.20	68.46	67.20	88.75	
2014	201	1001	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	180	20.20	0.20	101.95	1.10	64.12	63.00	88.87	
2014	201	1002	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	190	20.20	0.20	101.95	1.40	63.43	62.00	88.88	
2014	201	1003	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	200	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201	1004	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	210	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201	1005	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	220	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201	1006	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	230	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201	1007	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	240	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201	1008	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	250	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201	1009	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	260	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201	1010	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	270	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201	1011	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	280	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201	1012	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	290	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201	1013	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	300	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201	1014	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	310	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201	1015	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	320	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201	1016	20.20	0.20	101.85	2.10	103.75	88.20			2014	202	330	20.20	0.20	101.95	1.40	62.91	61.20	88.88	
2014	201																				

Client: Northern Poly
Project No.: 127811200
Block: HLRV
Test No.: 1

Year	Day	Month	C1	C2	C3	C4	C5	C6	C7	C8	C9	C10	C11	C12	C13	C14	C15	C16	C17	C18	C19	C20	C21	C22	C23	C24	C25	C26	C27	C28	C29	C30	C31	C32	C33	C34	C35	C36	C37	C38	C39	C40	C41	C42	C43	C44	C45	C46	C47	C48	C49	C50	C51	C52	C53	C54	C55	C56	C57	C58	C59	C60	C61	C62	C63	C64	C65	C66	C67	C68	C69	C70	C71	C72	C73	C74	C75	C76	C77	C78	C79	C80	C81	C82	C83	C84	C85	C86	C87	C88	C89	C90	C91	C92	C93	C94	C95	C96	C97	C98	C99	C100	C101	C102	C103	C104	C105	C106	C107	C108	C109	C110	C111	C112	C113	C114	C115	C116	C117	C118	C119	C120	C121	C122	C123	C124	C125	C126	C127	C128	C129	C130	C131	C132	C133	C134	C135	C136	C137	C138	C139	C140	C141	C142	C143	C144	C145	C146	C147	C148	C149	C150	C151	C152	C153	C154	C155	C156	C157	C158	C159	C160	C161	C162	C163	C164	C165	C166	C167	C168	C169	C170	C171	C172	C173	C174	C175	C176	C177	C178	C179	C180	C181	C182	C183	C184	C185	C186	C187	C188	C189	C190	C191	C192	C193	C194	C195	C196	C197	C198	C199	C200	C201	C202	C203	C204	C205	C206	C207	C208	C209	C210	C211	C212	C213	C214	C215	C216	C217	C218	C219	C220	C221	C222	C223	C224	C225	C226	C227	C228	C229	C230	C231	C232	C233	C234	C235	C236	C237	C238	C239	C240	C241	C242	C243	C244	C245	C246	C247	C248	C249	C250	C251	C252	C253	C254	C255	C256	C257	C258	C259	C260	C261	C262	C263	C264	C265	C266	C267	C268	C269	C270	C271	C272	C273	C274	C275	C276	C277	C278	C279	C280	C281	C282	C283	C284	C285	C286	C287	C288	C289	C290	C291	C292	C293	C294	C295	C296	C297	C298	C299	C300	C301	C302	C303	C304	C305	C306	C307	C308	C309	C310	C311	C312	C313	C314	C315	C316	C317	C318	C319	C320	C321	C322	C323	C324	C325	C326	C327	C328	C329	C330	C331	C332	C333	C334	C335	C336	C337	C338	C339	C340	C341	C342	C343	C344	C345	C346	C347	C348	C349	C350	C351	C352	C353	C354	C355	C356	C357	C358	C359	C360	C361	C362	C363	C364	C365	C366	C367	C368	C369	C370	C371	C372	C373	C374	C375	C376	C377	C378	C379	C380	C381	C382	C383	C384	C385	C386	C387	C388	C389	C390	C391	C392	C393	C394	C395	C396	C397	C398	C399	C400	C401	C402	C403	C404	C405	C406	C407	C408	C409	C410	C411	C412	C413	C414	C415	C416	C417	C418	C419	C420	C421	C422	C423	C424	C425	C426	C427	C428	C429	C430	C431	C432	C433	C434	C435	C436	C437	C438	C439	C440	C441	C442	C443	C444	C445	C446	C447	C448	C449	C450	C451	C452	C453	C454	C455	C456	C457	C458	C459	C460	C461	C462	C463	C464	C465	C466	C467	C468	C469	C470	C471	C472	C473	C474	C475	C476	C477	C478	C479	C480	C481	C482	C483	C484	C485	C486	C487	C488	C489	C490	C491	C492	C493	C494	C495	C496	C497	C498	C499	C500	C501	C502	C503	C504	C505	C506	C507	C508	C509	C510	C511	C512	C513	C514	C515	C516	C517	C518	C519	C520	C521	C522</
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Summary of CORRECTED DATA

Client: Northern Pip
Project No.: 12541254
Sheet: 61UV
Tool No.: 1

Year	Day	Hour	Q ₁	Q ₂	Q ₃	Q ₄	Q ₅	Q ₆	Q ₇	Q ₈	Q ₉	Q ₁₀	Q ₁₁	Q ₁₂	Q ₁₃	Q ₁₄	Q ₁₅	Q ₁₆	Q ₁₇	Q ₁₈	Q ₁₉	Q ₂₀	Q ₂₁	Q ₂₂	Q ₂₃	Q ₂₄	Q ₂₅	Q ₂₆	Q ₂₇	Q ₂₈	Q ₂₉	Q ₃₀	Q ₃₁	Q ₃₂	Q ₃₃	Q ₃₄	Q ₃₅	Q ₃₆	Q ₃₇	Q ₃₈	Q ₃₉	Q ₄₀	Q ₄₁	Q ₄₂	Q ₄₃	Q ₄₄	Q ₄₅	Q ₄₆	Q ₄₇	Q ₄₈	Q ₄₉	Q ₅₀	Q ₅₁	Q ₅₂	Q ₅₃	Q ₅₄	Q ₅₅	Q ₅₆	Q ₅₇	Q ₅₈	Q ₅₉	Q ₆₀	Q ₆₁	Q ₆₂	Q ₆₃	Q ₆₄	Q ₆₅	Q ₆₆	Q ₆₇	Q ₆₈	Q ₆₉	Q ₇₀	Q ₇₁	Q ₇₂	Q ₇₃	Q ₇₄	Q ₇₅	Q ₇₆	Q ₇₇	Q ₇₈	Q ₇₉	Q ₈₀	Q ₈₁	Q ₈₂	Q ₈₃	Q ₈₄	Q ₈₅	Q ₈₆	Q ₈₇	Q ₈₈	Q ₈₉	Q ₉₀	Q ₉₁	Q ₉₂	Q ₉₃	Q ₉₄	Q ₉₅	Q ₉₆	Q ₉₇	Q ₉₈	Q ₉₉	Q ₁₀₀	Q ₁₀₁	Q ₁₀₂	Q ₁₀₃	Q ₁₀₄	Q ₁₀₅	Q ₁₀₆	Q ₁₀₇	Q ₁₀₈	Q ₁₀₉	Q ₁₁₀	Q ₁₁₁	Q ₁₁₂	Q ₁₁₃	Q ₁₁₄	Q ₁₁₅	Q ₁₁₆	Q ₁₁₇	Q ₁₁₈	Q ₁₁₉	Q ₁₂₀	Q ₁₂₁	Q ₁₂₂	Q ₁₂₃	Q ₁₂₄	Q ₁₂₅	Q ₁₂₆	Q ₁₂₇	Q ₁₂₈	Q ₁₂₉	Q ₁₃₀	Q ₁₃₁	Q ₁₃₂	Q ₁₃₃	Q ₁₃₄	Q ₁₃₅	Q ₁₃₆	Q ₁₃₇	Q ₁₃₈	Q ₁₃₉	Q ₁₄₀	Q ₁₄₁	Q ₁₄₂	Q ₁₄₃	Q ₁₄₄	Q ₁₄₅	Q ₁₄₆	Q ₁₄₇	Q ₁₄₈	Q ₁₄₉	Q ₁₅₀	Q ₁₅₁	Q ₁₅₂	Q ₁₅₃	Q ₁₅₄	Q ₁₅₅	Q ₁₅₆	Q ₁₅₇	Q ₁₅₈	Q ₁₅₉	Q ₁₆₀	Q ₁₆₁	Q ₁₆₂	Q ₁₆₃	Q ₁₆₄	Q ₁₆₅	Q ₁₆₆	Q ₁₆₇	Q ₁₆₈	Q ₁₆₉	Q ₁₇₀	Q ₁₇₁	Q ₁₇₂	Q ₁₇₃	Q ₁₇₄	Q ₁₇₅	Q ₁₇₆	Q ₁₇₇	Q ₁₇₈	Q ₁₇₉	Q ₁₈₀	Q ₁₈₁	Q ₁₈₂	Q ₁₈₃	Q ₁₈₄	Q ₁₈₅	Q ₁₈₆	Q ₁₈₇	Q ₁₈₈	Q ₁₈₉	Q ₁₉₀	Q ₁₉₁	Q ₁₉₂	Q ₁₉₃	Q ₁₉₄	Q ₁₉₅	Q ₁₉₆	Q ₁₉₇	Q ₁₉₈	Q ₁₉₉	Q ₂₀₀	Q ₂₀₁	Q ₂₀₂	Q ₂₀₃	Q ₂₀₄	Q ₂₀₅	Q ₂₀₆	Q ₂₀₇	Q ₂₀₈	Q ₂₀₉	Q ₂₁₀	Q ₂₁₁	Q ₂₁₂	Q ₂₁₃	Q ₂₁₄	Q ₂₁₅	Q ₂₁₆	Q ₂₁₇	Q ₂₁₈	Q ₂₁₉	Q ₂₂₀	Q ₂₂₁	Q ₂₂₂	Q ₂₂₃	Q ₂₂₄	Q ₂₂₅	Q ₂₂₆	Q ₂₂₇	Q ₂₂₈	Q ₂₂₉	Q ₂₃₀	Q ₂₃₁	Q ₂₃₂	Q ₂₃₃	Q ₂₃₄	Q ₂₃₅	Q ₂₃₆	Q ₂₃₇	Q ₂₃₈	Q ₂₃₉	Q ₂₄₀	Q ₂₄₁	Q ₂₄₂	Q ₂₄₃	Q ₂₄₄	Q ₂₄₅	Q ₂₄₆	Q ₂₄₇	Q ₂₄₈	Q ₂₄₉	Q ₂₅₀	Q ₂₅₁	Q ₂₅₂	Q ₂₅₃	Q ₂₅₄	Q ₂₅₅	Q ₂₅₆	Q ₂₅₇	Q ₂₅₈	Q ₂₅₉	Q ₂₆₀	Q ₂₆₁	Q ₂₆₂	Q ₂₆₃	Q ₂₆₄	Q ₂₆₅	Q ₂₆₆	Q ₂₆₇	Q ₂₆₈	Q ₂₆₉	Q ₂₇₀	Q ₂₇₁	Q ₂₇₂	Q ₂₇₃	Q ₂₇₄	Q ₂₇₅	Q ₂₇₆	Q ₂₇₇	Q ₂₇₈	Q ₂₇₉	Q ₂₈₀	Q ₂₈₁	Q ₂₈₂	Q ₂₈₃	Q ₂₈₄	Q ₂₈₅	Q ₂₈₆	Q ₂₈₇	Q ₂₈₈	Q ₂₈₉	Q ₂₉₀	Q ₂₉₁	Q ₂₉₂	Q ₂₉₃	Q ₂₉₄	Q ₂₉₅	Q ₂₉₆	Q ₂₉₇	Q ₂₉₈	Q ₂₉₉	Q ₃₀₀	Q ₃₀₁	Q ₃₀₂	Q ₃₀₃	Q ₃₀₄	Q ₃₀₅	Q ₃₀₆	Q ₃₀₇	Q ₃₀₈	Q ₃₀₉	Q ₃₁₀	Q ₃₁₁	Q ₃₁₂	Q ₃₁₃	Q ₃₁₄	Q ₃₁₅	Q ₃₁₆	Q ₃₁₇	Q ₃₁₈	Q ₃₁₉	Q ₃₂₀	Q ₃₂₁	Q ₃₂₂	Q ₃₂₃	Q ₃₂₄	Q ₃₂₅	Q ₃₂₆	Q ₃₂₇	Q ₃₂₈	Q ₃₂₉	Q ₃₃₀	Q ₃₃₁	Q ₃₃₂	Q ₃₃₃	Q ₃₃₄	Q ₃₃₅	Q ₃₃₆	Q ₃₃₇	Q ₃₃₈	Q ₃₃₉	Q ₃₄₀	Q ₃₄₁	Q ₃₄₂	Q ₃₄₃	Q ₃₄₄	Q ₃₄₅	Q ₃₄₆	Q ₃₄₇	Q ₃₄₈	Q ₃₄₉	Q ₃₅₀	Q ₃₅₁	Q ₃₅₂	Q ₃₅₃	Q ₃₅₄	Q ₃₅₅	Q ₃₅₆	Q ₃₅₇	Q ₃₅₈	Q ₃₅₉	Q ₃₆₀	Q ₃₆₁	Q ₃₆₂	Q ₃₆₃	Q ₃₆₄	Q ₃₆₅	Q ₃₆₆	Q ₃₆₇	Q ₃₆₈	Q ₃₆₉	Q ₃₇₀	Q ₃₇₁	Q ₃₇₂	Q ₃₇₃	Q ₃₇₄	Q ₃₇₅	Q ₃₇₆	Q ₃₇₇	Q ₃₇₈	Q ₃₇₉	Q ₃₈₀	Q ₃₈₁	Q ₃₈₂	Q ₃₈₃	Q ₃₈₄	Q ₃₈₅	Q ₃₈₆	Q ₃₈₇	Q ₃₈₈	Q ₃₈₉	Q ₃₉₀	Q ₃₉₁	Q ₃₉₂	Q ₃₉₃	Q ₃₉₄	Q ₃₉₅	Q ₃₉₆	Q ₃₉₇	Q ₃₉₈	Q ₃₉₉	Q ₄₀₀	Q ₄₀₁	Q ₄₀₂	Q ₄₀₃	Q ₄₀₄	Q ₄₀₅	Q ₄₀₆	Q ₄₀₇	Q ₄₀₈	Q ₄₀₉	Q ₄₁₀	Q ₄₁₁	Q ₄₁₂	Q ₄₁₃	Q ₄₁₄	Q ₄₁₅	Q ₄₁₆	Q ₄₁₇	Q ₄₁₈	Q ₄₁₉	Q ₄₂₀	Q ₄₂₁	Q ₄₂₂	Q ₄₂₃	Q ₄₂₄	Q ₄₂₅	Q ₄₂₆	Q ₄₂₇	Q ₄₂₈	Q ₄₂₉	Q ₄₃₀	Q ₄₃₁	Q ₄₃₂	Q ₄₃₃	Q ₄₃₄	Q ₄₃₅	Q ₄₃₆	Q ₄₃₇	Q ₄₃₈	Q ₄₃₉	Q ₄₄₀	Q ₄₄₁	Q ₄₄₂	Q ₄₄₃	Q ₄₄₄	Q ₄₄₅	Q ₄₄₆	Q ₄₄₇	Q ₄₄₈	Q ₄₄₉	Q ₄₅₀	Q ₄₅₁	Q ₄₅₂	Q ₄₅₃	Q ₄₅₄	Q ₄₅₅	Q ₄₅₆	Q ₄₅₇	Q ₄₅₈	Q ₄₅₉	Q ₄₆₀	Q ₄₆₁	Q ₄₆₂	Q ₄₆₃	Q ₄₆₄	Q ₄₆₅	Q ₄₆₆	Q ₄₆₇	Q ₄₆₈	Q ₄₆₉	Q ₄₇₀	Q ₄₇₁	Q ₄₇₂	Q ₄₇₃	Q ₄₇₄	Q ₄₇₅	Q ₄₇₆	Q ₄₇₇	Q ₄₇₈	Q ₄₇₉	Q ₄₈₀	Q ₄₈₁	Q ₄₈₂	Q ₄₈₃	Q ₄₈₄	Q ₄₈₅	Q ₄₈₆	Q ₄₈₇	Q ₄₈₈	Q ₄₈₉	Q ₄₉₀	Q ₄₉₁	Q ₄₉₂	Q ₄₉₃	Q ₄₉₄	Q ₄₉₅	Q ₄₉₆	Q ₄₉₇	Q ₄₉₈	Q ₄₉₉	Q ₅₀₀	Q ₅₀₁	Q ₅₀₂	Q ₅₀₃	Q ₅₀₄	Q ₅₀₅	Q ₅₀₆	Q ₅₀₇	Q ₅₀₈	Q ₅₀₉	Q ₅₁₀	Q ₅₁₁	Q ₅₁₂	Q ₅₁₃	Q ₅₁₄	Q ₅₁₅	Q ₅₁₆	Q ₅₁₇	Q ₅₁₈	Q ₅₁₉	Q ₅₂₀	Q ₅₂₁	Q ₅₂₂	Q ₅₂₃	Q ₅₂₄	Q ₅₂₅	Q ₅₂₆	Q ₅₂₇	Q ₅₂₈	Q ₅₂₉	Q ₅₃₀	Q ₅₃₁	Q ₅₃₂	Q ₅₃₃	Q ₅₃₄	Q ₅₃₅	Q ₅₃₆	Q ₅₃₇	Q ₅₃₈	Q ₅₃₉	Q ₅₄₀	Q ₅₄₁	Q ₅₄₂	Q ₅₄₃	Q ₅₄₄	Q ₅₄₅	Q ₅₄₆	Q ₅₄₇	Q ₅₄₈	Q ₅₄₉	Q ₅₅₀	Q ₅₅₁	Q ₅₅₂	Q ₅₅₃	Q ₅₅₄	Q ₅₅₅	Q ₅₅₆	Q ₅₅₇	Q ₅₅₈	Q ₅₅₉	Q ₅₆₀	Q ₅₆₁	Q ₅₆₂	Q ₅₆₃	Q ₅₆₄	Q ₅₆₅	Q ₅₆₆	Q ₅₆₇	Q ₅₆₈	Q ₅₆₉	Q ₅₇₀	Q ₅₇₁	Q ₅₇₂	Q ₅₇₃	Q ₅₇₄	Q ₅₇₅	Q ₅₇₆	Q ₅₇₇	Q ₅₇₈	Q ₅₇₉	Q ₅₈₀	Q ₅₈₁	Q ₅₈₂	Q ₅₈₃	Q ₅₈₄	Q ₅₈₅	Q ₅₈₆	Q ₅₈₇	Q ₅₈₈	Q ₅₈₉	Q ₅₉₀	Q ₅₉₁	Q ₅₉₂	Q ₅₉₃	Q ₅₉₄	Q ₅₉₅	Q ₅₉₆	Q ₅₉₇	Q ₅₉₈	Q ₅₉₉	Q ₆₀₀	Q ₆₀₁	Q ₆₀₂	Q ₆₀₃	Q ₆₀₄	Q ₆₀₅	Q ₆₀₆	Q ₆₀₇	Q ₆₀₈	Q ₆₀₉	Q ₆₁₀	Q ₆₁₁	Q ₆₁₂	Q ₆₁₃	Q ₆₁₄	Q ₆₁₅	Q ₆₁₆	Q ₆₁₇	Q ₆₁₈	Q ₆₁₉	Q ₆₂₀	Q ₆₂₁	Q ₆₂₂	Q ₆₂₃	Q ₆₂₄	Q ₆₂₅	Q ₆₂₆	Q ₆₂₇	Q ₆₂₈	Q ₆₂₉	Q ₆₃₀	Q ₆₃₁	Q ₆₃₂	Q ₆₃₃	Q ₆₃₄	Q ₆₃₅	Q ₆₃₆	Q ₆₃₇	Q ₆₃₈	Q ₆₃₉	Q ₆₄₀	Q ₆₄₁	Q ₆₄₂	Q ₆₄₃	Q ₆₄₄	Q ₆₄₅	Q ₆₄₆	Q ₆₄₇	Q ₆₄₈	Q ₆₄₉	Q ₆₅₀	Q ₆₅₁	Q ₆₅₂	Q ₆₅₃	Q ₆₅₄	Q ₆₅₅	Q ₆₅₆	Q ₆₅₇	Q ₆₅₈	Q ₆₅₉	Q ₆₆₀	Q ₆₆₁	Q ₆₆₂	Q ₆₆₃	Q ₆₆₄	Q ₆₆₅	Q ₆₆₆	Q ₆₆₇	Q ₆₆₈	Q ₆₆₉	Q ₆₇₀	Q ₆₇₁	Q ₆₇₂	Q ₆₇₃	Q ₆₇₄	Q ₆₇₅	Q ₆₇₆	Q ₆₇₇	Q ₆₇₈	Q ₆₇₉	Q ₆₈₀	Q ₆₈₁	Q ₆₈₂	Q ₆₈₃	Q ₆₈₄	Q ₆₈₅	Q ₆₈₆	Q ₆₈₇	Q ₆₈₈	Q ₆₈₉	Q ₆₉₀	Q ₆₉₁	Q ₆₉₂	Q ₆₉₃	Q ₆₉₄	Q ₆₉₅	Q ₆₉₆	Q ₆₉₇	Q ₆₉₈	Q ₆₉₉	Q ₇₀₀	Q ₇₀₁	Q ₇₀₂	Q ₇₀₃	Q ₇₀₄	Q ₇₀₅	Q ₇₀₆	Q ₇₀₇	Q ₇₀₈	Q ₇₀₉	Q ₇₁₀	Q ₇₁₁	Q ₇₁₂	Q ₇₁₃	Q ₇₁₄	Q ₇₁₅	Q ₇₁₆	Q ₇₁₇	Q ₇₁₈	Q ₇₁₉	Q ₇₂₀	Q ₇₂₁	Q ₇₂₂	Q ₇₂₃	Q ₇₂₄	Q ₇₂₅	Q ₇₂₆	Q ₇₂₇	Q ₇₂₈	Q ₇₂₉	Q ₇₃₀	Q ₇₃₁	Q ₇₃₂	Q ₇₃₃	Q ₇₃₄	Q ₇₃₅	Q ₇₃₆	Q ₇₃₇	Q ₇₃₈	Q ₇₃₉	Q ₇₄₀	Q ₇₄₁	Q ₇₄₂	Q ₇₄₃	Q ₇₄₄	Q ₇₄₅	Q ₇₄₆	Q ₇₄₇	Q ₇₄₈	Q ₇₄₉	Q ₇₅₀	Q ₇₅₁	Q ₇₅₂	Q ₇₅₃	Q ₇₅₄	Q ₇₅₅	Q ₇₅₆	Q ₇₅₇	Q ₇₅₈	Q ₇₅₉	Q ₇₆₀	Q ₇₆₁	Q ₇₆₂	Q ₇₆₃	Q ₇₆₄	Q ₇₆₅	Q ₇₆₆	Q ₇₆₇	Q ₇₆₈	Q ₇₆₉	Q ₇₇₀	Q ₇₇₁	Q ₇₇₂	Q ₇₇₃	Q ₇₇₄	Q ₇₇₅	Q ₇₇₆	Q ₇₇₇	Q ₇₇₈	Q ₇₇₉	Q ₇₈₀	Q ₇₈₁	Q ₇₈₂	Q ₇₈₃	Q ₇₈₄	Q ₇₈₅	Q ₇₈₆	Q ₇₈₇	Q ₇₈₈	Q ₇₈₉	Q ₇₉₀	Q ₇₉₁	Q ₇₉₂	Q ₇₉₃	Q ₇₉₄	Q ₇₉₅	Q ₇₉₆	Q ₇₉₇	Q ₇₉₈	Q ₇₉₉	Q ₈₀₀	Q ₈₀₁	Q ₈₀₂	Q ₈₀₃	Q ₈₀₄	Q ₈₀₅	Q ₈₀₆	Q ₈₀₇	Q ₈₀₈	Q ₈₀₉	Q ₈₁₀	Q ₈₁₁	Q ₈₁₂	Q ₈₁₃	Q ₈₁₄	Q ₈₁₅	Q ₈₁₆	Q ₈₁₇	Q ₈₁₈	Q ₈₁₉	Q ₈₂₀	Q ₈₂₁	Q ₈₂₂	Q ₈₂₃	Q ₈₂₄	Q ₈₂₅	Q ₈₂₆	Q ₈₂₇	Q ₈₂₈	Q ₈₂₉	Q ₈₃₀	Q ₈₃₁	Q ₈₃₂	Q ₈₃₃	Q ₈₃₄	Q ₈₃₅	Q ₈₃₆	Q ₈₃₇	Q ₈₃₈	Q ₈₃₉	Q ₈₄₀	Q ₈₄₁	Q ₈₄₂	Q ₈₄₃	Q ₈₄₄	Q ₈₄₅	Q ₈₄₆	Q ₈₄₇	Q ₈₄₈	Q ₈₄₉	Q ₈₅₀	Q ₈₅₁	Q ₈₅₂	Q ₈₅₃	Q ₈₅₄	Q ₈₅₅	Q ₈₅₆	Q ₈₅₇	Q ₈₅₈	Q ₈₅₉	Q ₈₆₀	Q ₈₆₁	Q ₈₆₂	Q ₈₆₃	Q ₈₆₄	Q ₈₆₅	Q ₈₆₆	Q ₈₆₇	Q ₈₆₈	Q ₈₆₉	Q ₈₇₀	Q ₈₇₁	Q ₈₇₂	Q ₈₇₃	Q ₈₇₄	Q ₈₇₅	Q ₈₇₆	Q ₈₇₇	Q ₈₇₈	Q ₈₇₉	Q ₈₈₀	Q ₈₈₁
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Client:	Northern Pulp
Project No.:	121611238
Block:	HLRV
Test No.:	1

[illegible]

Client:	Northern Poly.
Project No.:	125011200
Sheet:	HLRV
Task No.:	1

Year	Day	Hour	TSS				TSS loading		Year	Day	Hour	TSS				TSS loading	
			Q ₁	Q ₂	Q ₃	Q ₄	Time + Q ₂	TSS average				Q ₁	Q ₂	Q ₃	Q ₄	Time + Q ₂	TSS average
2014	201	22:00	25.30	0.20	128.94	0.21	68.33	48.44	-0.06	2014	201	22:00	25.30	0.20	128.94	0.21	68.33
2014	201	22:01	26.07	0.20	128.43	0.20	68.33	-0.06	-0.06	2014	201	22:01	26.07	0.20	128.43	0.20	68.33
2014	201	22:02	26.50	0.20	128.74	0.20	68.33	-0.06	-0.06	2014	201	22:02	26.50	0.20	128.74	0.20	68.33
2014	201	22:03	26.50	0.20	128.47	0.20	68.33	-0.06	-0.06	2014	201	22:03	26.50	0.20	128.47	0.20	68.33
2014	201	22:04	26.57	0.20	128.66	0.20	68.33	-0.06	-0.06	2014	201	22:04	26.57	0.20	128.66	0.20	68.33
2014	201	22:05	26.50	0.20	128.47	0.20	68.33	-0.06	-0.06	2014	201	22:05	26.50	0.20	128.47	0.20	68.33
2014	201	22:06	26.57	0.20	128.66	0.20	68.33	-0.06	-0.06	2014	201	22:06	26.57	0.20	128.66	0.20	68.33
2014	201	22:07	26.50	0.20	128.47	0.20	68.33	-0.06	-0.06	2014	201	22:07	26.50	0.20	128.47	0.20	68.33
2014	201	22:08	26.57	0.20	128.66	0.20	68.33	-0.06	-0.06	2014	201	22:08	26.57	0.20	128.66	0.20	68.33
2014	201	22:09	26.50	0.20	128.47	0.20	68.33	-0.06	-0.06	2014	201	22:09	26.50	0.20	128.47	0.20	68.33
2014	201	22:10	26.57	0.20	128.66	0.20	68.33	-0.06	-0.06	2014	201	22:10	26.57	0.20	128.66	0.20	68.33
2014	201	22:11	26.50	0.20	128.47	0.20	68.33	-0.06	-0.06	2014	201	22:11	26.50	0.20	128.47	0.20	68.33
2014	201	22:12	26.57	0.20	128.66	0.20	68.33	-0.06	-0.06	2014	201	22:12	26.57	0.20	128.66	0.20	68.33
2014	201	22:13	26.50	0.20	128.47	0.20	68.33	-0.06	-0.06	2014	201	22:13	26.50	0.20	128.47	0.20	68.33
2014	201	22:14	26.57	0.20	128.66	0.20	68.33	-0.06	-0.06	2014	201	22:14	26.57	0.20	128.66	0.20	68.33
2014	201	22:15	26.50	0.20	128.47	0.20	68.33	-0.06	-0.06	2014	201	22:15	26.50	0.20	128.47	0.20	68.33
2014	201	22:16	26.57	0.20	128.66	0.20	68.33	-0.06	-0.06	2014	201	22:16	26.57	0.20	128.66	0.20	68.33
2014	201	22:17	26.50	0.20	128.47	0.20	68.33	-0.06	-0.06	2014	201	22:17	26.50	0.20	128.47	0.20	68.33
2014	201	22:18	26.57	0.20	128.66	0.20	68.33	-0.06	-0.06	2014	201	22:18	26.57	0.20	128.66	0.20	68.33
2014	201	22:19	26.50	0.20	128.47	0.20	68.33	-0.06	-0.06	2014	201	22:19	26.50	0.20	128.47	0.20	68.33
2014	201	22:20	26.57	0.20	128.66	0.20	68.33	-0.06	-0.06	2014	201	22:20	26.57	0.20	128.66	0.20	68.33
2014	201	22:21	26.50	0.20	128.47	0.20	68.33	-0.06	-0.06	2014	201	22:21	26.50	0.20	128.47	0.20	68.33
2014	201	22								2014	201	22					

Client:	Northern Pipe
Project No.:	121011210
State:	ILRIV
Test No.:	1

[illegible]

GAS CALCULATIONS

Client: Northern Pipe
 Plant: New Glasgow
 Location: High Level Roof Vent

	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	NO _x (ppm)
Ave. Gas 1	20.4	0.2	137.4	4.4	0.0
Ave. Gas 2	20.4	0.2	138.4	3.3	0.0
Ave. Gas 3	20.4	0.2	139.6	3.0	0.0

Test 1 Time	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	NO _x (ppm)
8/19/2014 13:30	20.36038	0.227152	137.4182	4.449723	0

Test 2 Time	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	NO _x (ppm)
8/19/2014 14:00	20.38413	0.221871	138.4394	3.31528	0

Test 3 Time	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	NO _x (ppm)
8/19/2014 14:30	20.36105	0.223677	139.6234	3.021197	0

Note: O₂, CO₂, CO, and SO₂ data from continuous monitoring using the trailer. The NO_x testing was conducted concurrently with flow measurements.

Raw Data for: Northern Pulp Summer Testing Test #1

Client: Northern Pulp
Job Number: 12191700

Plant: New Glasgow
Location: High Level Road Vent
Test: 1
Date: 20-Aug-11
Personnel: CM

Test Start: 11:15 PM
Test Finish: 12:15 PM

Parameters

Barometric Pressure, Pbar (in. Hg)
Stack Static Pressure, Pstatic (in. H2O)
Ambient Temp. (°F)
Assumed Moisture Content (as decimal)

29.85
0.00
0.3

CO₂ (%)
CO (%)
H₂ (%)

30.4
0.2
70.4

Stack Diameter (in.)
Stack Area (sq. ft.)
Plot Coefficient (Cp)

12
22.37
0.849

Traverse
Point

Time
(min)

Stack Gas
Temp, Tg
(°F)

8-type Pitot
static P
(in. H2O)

1	134	0.78
2	141	0.78
3	133	0.78
4	78	0.60
5	114	0.50
6	120	0.51
7	137	0.57
8	131	0.53
9	144	0.61
10	141	0.57
11	140	0.57
12	139	0.56

10.

1	141	0.58
2	144	0.58
3	141	0.58
4	141	0.58
5	147	0.64
6	146	0.63
7	149	0.67
8	149	0.67
9	149	0.67
10	149	0.67
11	149	0.67
12	149	0.67

Calculations for Northern Pulp Summer Testing Test #1

Client: Northern Pulp

Job Number: 127611268

Plant: New Chapow

Location: High Level Road Vent

Test: 1

Date: 28 Aug-14

Personnel: CM

Calculated Parameters

Stack Gas Pressure, Pa (in.Hg)
Stack Gas Molecular Weight, Dry Basis, Mol (lb/lb-mole)
Volume of Water Vapour Collected, Vwc (cu.ft)
Stack Gas Moisture Content (% as decimal)
Stack Gas Molecular Weight, Wet Basis, Mol (lb/lb-mole)

28.95
28.86
0.094
0.300
28.60

	Traverse Point	Time (min)	Stack Gas Temp, T _s (°F)	S-type Pitot, delta P (in. H ₂ O)	Stack Gas Velocity, U _s (ft/s)
1	1	10	594	0.78	55.72
	2		595	0.78	55.77
	3		598	0.79	56.17
	4		600	0.80	56.72
	5		601	0.80	56.77
	6		605	0.81	57.31
	7		605	0.83	58.01
	8		604	0.80	58.91
	9		604	0.81	57.28
	10		601	0.78	56.06
	11		600	0.77	56.06
	12		599	0.76	55.24
2	1		603	0.80	56.89
	2		604	0.81	57.28
	3		605	0.82	57.86
	4		604	0.81	57.28
	5		603	0.80	56.93
	6		602	0.79	56.46
	7		601	0.78	56.05
	8		600	0.77	55.65
	9		600	0.77	55.65
	10		601	0.77	55.59
	11		602	0.79	56.46
	12		603	0.80	56.89
	Total 10		Average 601	Average 0.79	Average 56.5

Raw Data for: Northern Pulp Slansner Testing
Test #2

Client: Northern Pulp
Job Number: 1551809

Plant: Hiss Changer
Location: High Level Road Vent
Test: 2
Date: 28-Sep-16
Personnel: CM

Test Start: 12:25 PM
Test Finish: 12:55 PM

Parameters

Barometric Pressure, Pbar (in. Hg)
Stack Static Pressure, Pstatic (in. H2O)
Ambient Temp. (°F)
Assumed Moisture Content (as default)

20.4
0.2
79.4

O₂ (%)
CO₂ (%)
N₂ (%)

Stack Diameter, (in.)
Stack Area, (sq. ft.)
Pilot Coefficient, (Cp)

79
28.27
0.540

Traverse Point	Time (min)	Stack Gas Temp, Tg (°F)	S-type Pilot delta P (in. H2O)
1	19	64	0.91
2		59	0.94
3		70	0.91
4		78	0.91
5		10	0.91
6		14	0.91
7		14	0.91
8		14	0.91
9		14	0.91
10		14	0.91
11		14	0.91
12		14	0.91
1		74	0.91
2		74	0.91
3		74	0.91
4		74	0.91
5		74	0.91
6		74	0.91
7		74	0.91
8		74	0.91
9		74	0.91
10		74	0.91
11		74	0.91
12		74	0.91

Calculations for Northern Pipe Summer Testing Test #1

Client: Northern Pipe
Job Number: 12161129

Plant: New Glasgow
Location: High Level Roof Vent
Test: 2
Date: 20-Aug-14
Personnel: CM

Calculated Parameters

Stack Gas Pressure, Pa (in.Hg)
Stack Gas Molecular Weight, Dry Basis, M_d (lb/lb-mole)
Volume of Water Vapour Collected, V_w (cu.ft)
Stack Gas Moisture Content (% as decimal)
Stack Gas Molecular Weight, Wet Basis, M_w (lb/lb-mole)

29.46
33.86
0.014
0.528
25.69

Traverse Point	Time (min)	Stack Gas Temp, T _s (°F)	S-type Pitot, delta P (in. H ₂ O)	Stack Gas Velocity, U _s (ft/s)
1	10	600	0.78	58.36
		599	0.80	58.07
		600	0.81	57.07
		599	0.82	57.38
		601	0.81	57.12
		602	0.83	57.87
		605	0.78	58.80
		605	0.78	58.24
		602	0.78	58.10
		602	0.77	58.74
		600	0.77	58.66
		600	0.76	58.28
2		602	0.80	58.61
		603	0.79	58.90
		601	0.81	57.12
		601	0.81	57.12
		601	0.82	57.47
		605	0.81	57.31
		604	0.81	57.28
		603	0.79	58.90
		604	0.79	58.56
		604	0.78	58.16
		605	0.78	58.61
		601	0.76	58.33
Total	10	Average 602	Average 0.79	Average 58.6

Raw Data for: Northern Pulp Summer Tooling Test 63

Client: Northern Pulp
Job Number: 12151258

Plant: New Slegger
Location: High Level Road Vent
Test: 3
Date: 10-Aug-14
Personnel: CM

Test Start: 12:30 PM
Test Finish: 12:45 PM

Parameters

Barometric Pressure, Pbar (in. Hg)
Stack Static Pressure, Pstatic (in. H2O)
Ambient Temp. (°F)
Assumed Moisture Content (as decimal)

12.75
5.41
61.3

O₂ (%)
CO₂ (%)
H₂ (%)

23.4
0.2
70.4

Stack Diameter (in.)
Stack Area (sq. ft.)
Pilot Coefficient (Cp)

18
28.27
0.846

Time
(min)

Stack Gas
Temp. T_s
(°F)

B-type Pilot
d_{stack} p
(in. H2O)

1	1	141	0.74
2	2	140	0.74
3	3	139	0.74
4	4	138	0.74
5	5	137	0.74
6	6	136	0.74
7	7	135	0.74
8	8	134	0.74
9	9	133	0.74
10	10	132	0.74
11	11	131	0.74
12	12	130	0.74

1	1	140	0.68
2	2	141	0.74
3	3	140	0.74
4	4	141	0.74
5	5	140	0.74
6	6	141	0.74
7	7	140	0.74
8	8	141	0.74
9	9	140	0.74
10	10	141	0.74
11	11	140	0.74
12	12	141	0.74

Calculations for: Northern Pulp Summer Testing Test #1

Client: Northern Pulp
Job Number: 121011209

Plant: New Glasgow
Location: High Level Road Vent
Test: 3
Date: 28-Aug-14
Personnel: C&I

Calculated Parameters

Stack Gas Pressure, Pa (in.Hg) 29.86
Stack Gas Molecular Weight, Dry Basis, lbs (lb/lb-mole) 29.86
Volume of Water Vapour Collected, Vwc (cu.ft) 0.014
Stack Gas Moisture Content (% as declared) 0.300
Stack Gas Molecular Weight, Wet Basis, lbs (lb/lb-mole) 28.60

Traverse Point	Time (min)	Stack Gas Temp, T _s (°F)	S-type Pilot, delta P (in. H ₂ O)	Stack Gas Velocity, U _s (ft/s)
1	10	601	0.79	56.41
2		602	0.80	56.81
3		604	0.81	57.26
4		605	0.82	57.66
5		606	0.81	57.31
6		604	0.83	57.97
7		601	0.80	56.77
8		604	0.78	56.56
9		602	0.78	56.10
10		603	0.77	56.78
11		602	0.77	56.74
12		600	0.76	56.28
1		602	0.78	56.10
2		601	0.79	56.41
3		603	0.80	56.68
4		601	0.81	57.12
5		602	0.82	57.52
6		601	0.81	57.12
7		602	0.83	57.87
8		603	0.81	57.21
9		603	0.79	56.50
10		604	0.78	56.56
11		605	0.77	56.86
12		601	0.76	56.33
Total	10	Average 603	Average 0.80	Average 56.7

CALCULATIONS

Northern Pulp
 New Glasgow
 High Level Roof Vent
 Operating Conditions: Normal

Reference Temperature, Tref (F): 77
 (K): 288
 Reference Pressure, Pref (in.Hg): 29.92
 (Bar): 1.0

Parameter	Symbol	Units	Test 1	Test 2	Test 3	Average
Test ID	-	-	1	2	3	n/a
Date	-	-	20-Aug-14	20-Aug-14	20-Aug-14	n/a
Start Time	-	-	12:15 PM	12:25 PM	12:35 PM	n/a
End Time	-	-	12:25 PM	12:35 PM	12:45 PM	n/a
Total Sampling Time	-	min	10	10	10	10
Stack Diameter	D	in.	72	72	72	72
Average Stack Gas Temperature	Ts	F	141	142	143	142
Barometric Pressure	Pbar	in.Hg	29.95	29.95	29.95	29.9
Stack Static Pressure	Pstatic	in.H ₂ O	0	0	0	0
Average Pressure Drop (Head)	dp	in.H ₂ O	0.79	0.79	0.80	0.79
Pilot Coefficient	Cp	-	0.840	0.840	0.840	0.840
Reference Temperature	Tref	R	537	537	537	537
Reference Pressure	Pref	in.Hg	29.92	29.92	29.92	29.92
Water Fraction	Bwo	-	0.30	0.30	0.30	0.30
Average Stack Velocity	Us	ft/s	56.51	56.57	56.87	56.6
Actual Flow Rate	Actm	cu.ft/m	95,871	95,875	96,141	95,998
Dry Standard Flow Rate	Dscfm	cu.ft/m	59,909	59,963	60,037	60,003
Wet Standard Flow Rate	MMSCFH	-	3.60	3.60	3.60	3.60

GAS CALCULATIONS
Northern Pulp
New Glasgow
High Level Roof Vent

Variable	Symbol	Units	Calculation	Test 1	Test 2	Test 3	Average
Dry Stack Gas Flow Rate	Q _d	dcfm dscfm	$Q_d (\text{dscfm}) = 0.889473 \times Q_g (\text{dcfm})$	59,989 28.3	59,983 28.3	59,037 28.3	59,003 28.3
Stack Gas Oxygen Content	Co ₂	%	Measurement from Flue Gas Analyser	20.4	20.4	20.4	20.4
Stack Gas Carbon Dioxide Content	Co ₂	%	Measurement from Flue Gas Analyser	0.2	0.2	0.2	0.2
Sulphur Dioxide - SO ₂							
SO ₂ Measured Concentration	Co ₂	ppm	Measurement from Flue Gas Analyser	4.45	3.32	3.02	3.60
Uncorrected @ STP	Co ₂	mg/dscfm	$Co_2 (\text{mg/dscfm}) = Co_2 (\text{ppm}) \times 1.63$	11.7	8.69	7.92	9.42
SO ₂ Emission Rate	ER _{SO2}	g/s kg/hr	$ER_{SO2} = Co_2 / 60 \times Q_d$ $ER_{SO2} (\text{kg/hr}) = 3.6 \times ER_{SO2} (\text{g/s})$	0.33 1.19	0.25 0.89	0.22 0.81	0.27 0.86
SO ₂ Concentration							
Corrected to 11% O ₂	Co ₂	mg/dscfm	$Co_2 (11\% O_2) = Co_2 (\text{mg/dscfm}) \times (20.9-11) / (20.9-Co_2)$	214	180	145	173
Corrected to 3% O ₂	Co ₂	mg/dscfm	$Co_2 (3\% O_2) = Co_2 (\text{mg/dscfm}) \times (20.9-3) / (20.9-Co_2)$	387	290	263	313
Corrected to 12% CO ₂	Co ₂	mg/dscfm	$Co_2 (12\% CO_2) = Co_2 (\text{mg/dscfm}) \times (12/Co_2)$	616	470	425	503
Nitrogen Oxides - NO _x							
NO _x Measured Concentration	Co _{NOx}	ppm	Measurement from Flue Gas Analyser	0.0	0.0	0.0	0.00
Uncorrected @ STP	Co _{NOx}	mg/dscfm	$Co_{NOx} (\text{mg/dscfm}) = Co_{NOx} (\text{ppm}) \times 1.63$	0.0	0.0	0.0	0.0
NO _x Emission Rate	ER _{NOx}	g/s kg/hr	$ER_{NOx} = Co_{NOx} / 60 \times Q_d$ $ER_{NOx} (\text{kg/hr}) = 3.6 \times ER_{NOx} (\text{g/s})$	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.00
NO _x Concentration							
Corrected to 11% O ₂	Co _{NOx}	mg/dscfm	$Co_{NOx} (11\% O_2) = Co_{NOx} (\text{mg/dscfm}) \times (20.9-11) / (20.9-Co_2)$	0	0	0	0
Corrected to 3% O ₂	Co _{NOx}	mg/dscfm	$Co_{NOx} (3\% O_2) = Co_{NOx} (\text{mg/dscfm}) \times (20.9-3) / (20.9-Co_2)$	0	0	0	0
Corrected to 12% CO ₂	Co _{NOx}	mg/dscfm	$Co_{NOx} (12\% CO_2) = Co_{NOx} (\text{mg/dscfm}) \times (12/Co_2)$	0	0	0	0
Carbon Monoxide - CO							
CO Measured Concentration	Co _{CO}	ppm	Measurement from Flue Gas Analyser	137	138	140	138
Uncorrected @ STP	Co _{CO}	mg/dscfm	$Co_{CO} (\text{mg/dscfm}) = Co_{CO} (\text{ppm}) \times 1.145$	157	158	160	159
CO Emission Rate	ER _{CO}	g/s kg/hr	$ER_{CO} = Co_{CO} / 60 \times Q_d$ $ER_{CO} (\text{kg/hr}) = 3.6 \times ER_{CO} (\text{g/s})$	4.45 16.0	4.49 16.2	4.53 16.3	4.49 16.2
CO Concentration							
Corrected to 11% O ₂	Co _{CO}	mg/dscfm	$Co_{CO} (11\% O_2) = Co_{CO} (\text{mg/dscfm}) \times (20.9-11) / (20.9-Co_2)$	2,887	2,928	2,937	2,917
Corrected to 3% O ₂	Co _{CO}	mg/dscfm	$Co_{CO} (3\% O_2) = Co_{CO} (\text{mg/dscfm}) \times (20.9-3) / (20.9-Co_2)$	5,219	5,295	5,310	5,275
Corrected to 12% CO ₂	Co _{CO}	mg/dscfm	$Co_{CO} (12\% CO_2) = Co_{CO} (\text{mg/dscfm}) \times (12/Co_2)$	8,312	8,573	8,577	8,487

Legend:
sq.ft - square feet
sq.m - square metres
Pi - 3.142
R - degrees Rankine
ppm - parts per million

in.Hg - inches of mercury
o.f.t. - cubic feet
o.s.m. - cubic metres
STP - standard temperature and pressure (23 C and 101.3 kPa)
dscfm - dry standard cubic metres per second
dcfm - dry standard cubic feet per minute

mg/dscfm - milligrams per dry standard cubic metre
g/s - grams per second
NO_x - as NO₂
scfm - actual cubic feet per minute

STACK TESTING RESULTS
GAS CALCULATIONS
Northern Pulp
New Glasgow
High Level Roof Vent

Parameter	Test 1	Test 2	Test 3	Average	Limits
Oxygen - O ₂ (%)	20.4	20.4	20.4	20.4	-
Carbon Dioxide - CO ₂ (%)	0.2	0.2	0.2	0.2	-
Sulphur Dioxide - SO ₂					
SO ₂ Measured Concentration (ppm)	4.4	3.32	3.02	3.60	-
Uncorrected at STP (mg/dscm)	11.7	8.69	7.92	9.42	-
Emission Rate (kg/hr)	1.19	0.89	0.81	0.98	-
Nitrogen Oxides - NO _x					
NO _x Measured Concentration (ppm)	ND	ND	ND	ND	-
Uncorrected at STP (mg/dscm)	ND	ND	ND	ND	-
Emission Rate (kg/hr)	ND	ND	ND	ND	-
Carbon Monoxide - CO					
CO Measured Concentration (ppm)	137	138	140	138	-
Uncorrected at STP (mg/dscm)	157	159	160	159	-
Emission Rate (kg/hr)	18.0	18.2	18.3	18.2	-

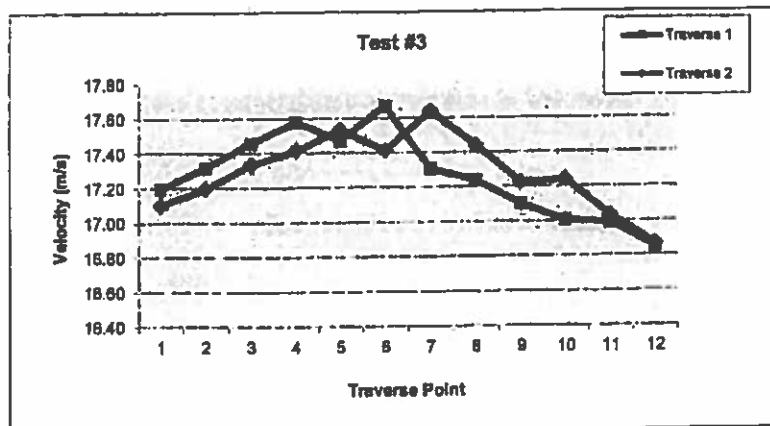
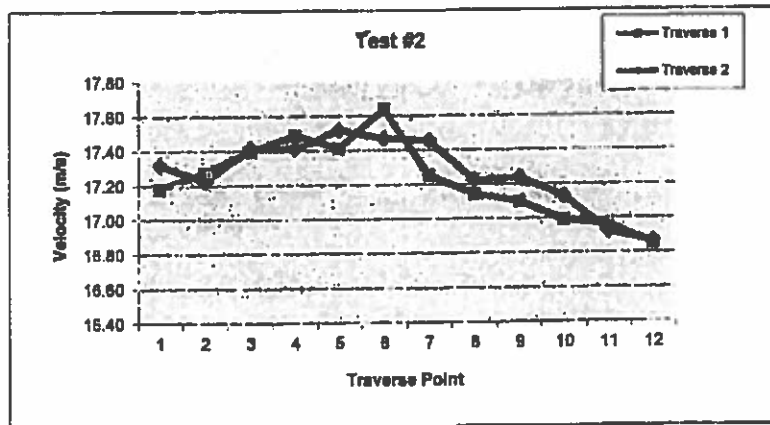
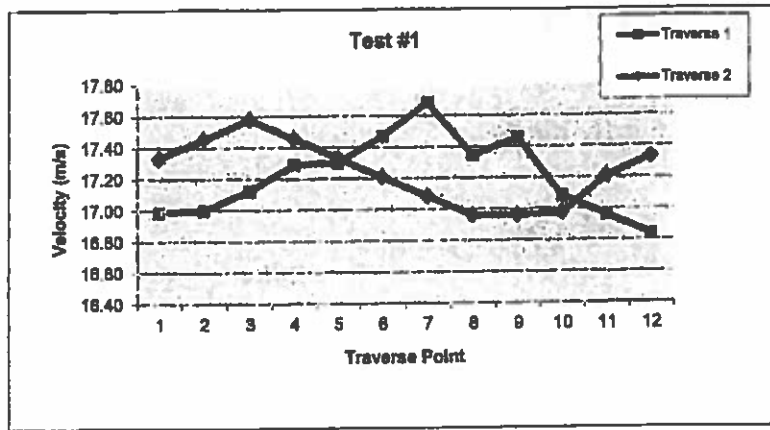
Legend: C - degrees Celsius
m/s - metres per second
dscms - dry standard cubic metres per second
ppm - parts per million

STP - standard temperature and pressure (25 C and 101.3 kPa)
mg/dscm - milligrams per dry standard cubic metre
NO_x - as NO₂
ND - non-detectable

Raw Data for:
High Level Roof Vent

Job No. 121511269

Northern Pulp Summer Testing
Velocity Profile



Project: 12511269 Northern Pulp
 Test: Recovery Boiler Test #1
 Date: Sept. 3 2014
 Analyst: _____

Hand Calculations
 Page 1 of 6

Absolute stack gas pressure (Ps) in in.Hg is:

$$\begin{aligned}
 P_s &= P_{bar} + \frac{P_{static \text{ in.H}_2\text{O}}}{13.6 \text{ in.H}_2\text{O/in.Hg}} \\
 P_s &= \underline{30.00 \text{ in.Hg}} + \frac{\underline{1.10 \text{ in.H}_2\text{O}}}{13.6 \text{ in.H}_2\text{O/in.Hg}} \\
 P_s &= \underline{30.08} \text{ in.Hg} \\
 A
 \end{aligned}$$

The molecular weight of the stack gas on a dry basis (Md) in lb/lb-mole is:

$$\begin{aligned}
 Md &= 0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 [(\%N_2)] \\
 Md &= 0.44 \times \underline{9.4} + 0.32 \times \underline{7.7} + 0.28 \left(\frac{\underline{82.9}}{+ 0.40(\underline{\quad} + \underline{\quad})} \right) \\
 Md &= \underline{4.136} + \underline{2.464} + \underline{23.212} + \underline{\quad} \\
 Md &= \underline{29.812} \text{ lb/lb-mole}
 \end{aligned}$$

The volume of water vapour collected at reference conditions (Vwc) in ft³ is:

$$\begin{aligned}
 V_{wc} &= 0.0480 \text{ ft}^3/\text{mL} \times \text{volume of moisture collected mL.} \\
 V_{wc} &= 0.0480 \times \underline{581.6 \text{ mL}} \\
 V_{wc} &= \underline{27.9168} \text{ ft}^3
 \end{aligned}$$

The average H orifice in in.H₂O is:

$$\begin{aligned}\underline{H}_{\text{orifice}_{\text{avg}}} &= \frac{\Sigma \text{H orifice}}{\# \text{ points}} \\ \underline{H}_{\text{orifice}_{\text{avg}}} &= \frac{21.87 + 22.25}{48} \\ \underline{H}_{\text{orifice}_{\text{avg}}} &= \underline{0.92} \text{ in.H}_2\text{O}\end{aligned}$$

The pressure at the gas meter (P_m) in in.Hg is:

$$\begin{aligned}P_m &= P_{\text{bar}} + \frac{\underline{H}_{\text{orifice}_{\text{avg}}} \text{ in.H}_2\text{O}}{13.6 \text{ in.H}_2\text{O/in.Hg}} \\ P_m &= \underline{30.00 \text{ in.Hg}} + \frac{\underline{0.92 \text{ in.H}_2\text{O}}}{13.6 \text{ in.H}_2\text{O/in.Hg}} \\ P_m &= \underline{30.00 \text{ in.Hg}} + \underline{0.068 \text{ in.Hg}} \\ P_m &= \underline{30.07} \text{ in.Hg}\end{aligned}$$

The temperature of the gas meter (T_m) in °R is:

$$\begin{aligned}T_m &= \frac{\Sigma \text{ meter temp. } ^\circ\text{F}}{\# \text{ points}} + 460 \\ T_m &= \frac{3229 + 3604}{48 \div 2} + 460 \\ T_m &= \frac{6833}{24} + 460 \\ T_m &= \underline{531} \text{ } ^\circ\text{R}\end{aligned}$$

The total volume of gas metered (V_m) in ft^3 is:

$$V_m = V_f \text{ ft}^3 - V_i \text{ ft}^3$$

$$V_m = 530.75 \text{ ft}^3 - 470.18 \text{ ft}^3$$

$$V_m = 60.57 \text{ ft}^3$$

The dry gas volume at reference conditions (V_{mc}) in ft^3 is:

$$V_{mc} = \frac{T_{ref} \text{ } ^\circ\text{R}}{P_{ref} \text{ in.Hg}} \times \frac{P_m \text{ in.Hg} \times V_m \text{ ft}^3 \times \gamma}{T_m \text{ } ^\circ\text{R}}$$

$$V_{mc} = \frac{(77+460) \times 30.07 \text{ in.Hg} \times 60.57 \text{ ft}^3 \times 1.040}{29.92 \text{ in.Hg} \times 531 \text{ } ^\circ\text{R}}$$

$$V_{mc} = 64.0 \text{ ft}^3 \times 1 \text{ m}^3 / 35.31 \text{ ft}^3 = 1.81 \text{ m}^3$$

The stack gas moisture content, i.e. the proportion by volume of water vapour in the gas stream (B_{wo}) is:

$$B_{wo} = \frac{V_{wc} \text{ ft}^3}{V_{wc} \text{ ft}^3 + V_{mc} \text{ ft}^3}$$

$$B_{wo} = \frac{27.9168 \text{ ft}^3}{27.9168 \text{ ft}^3 + 64.0 \text{ ft}^3}$$

$$B_{wo} = \frac{27.9168 \text{ ft}^3}{91.91 \text{ ft}^3}$$

$$B_{wo} = 0.304$$

D

The Molecular weight of the stack gas on a wet basis (M_s) in lb/lb-mole is:

$$\begin{aligned}
 M_s &= M_d \text{ lb/lb-mole} (1 - B_{wo}) + 18 \text{ lb/lb-mole} \times B_{wo} \\
 M_s &= \frac{29.812 \text{ lb}}{\text{lb-mole}} \times (1 - 0.304) + 18 \times 0.304 \\
 M_s &= \frac{29.812 \text{ lb}}{\text{lb-mole}} \times 0.696 + 5.47 \\
 M_s &= 26.22 \text{ lb/lb-mole}
 \end{aligned}$$

The average temperature of the stack ($T_{s_{avg}}$) in °R is:

$$\begin{aligned}
 T_{s_{avg}} &= \frac{\sum T_s \text{ °F}}{\# \text{ points}} + 460 \\
 T_{s_{avg}} &= \frac{3776 + 3799}{48} + 460 \\
 T_{s_{avg}} &= \frac{7564}{48} + 460 \\
 T_{s_{avg}} &= 618 \text{ °R}
 \end{aligned}$$

The average velocity ($U_{s_{avg}}$) of the stack in ft/s is:

$$\begin{aligned}
 U_{s_{avg}} &= \frac{\sum V}{\# \text{ points}} \\
 U_{s1} &= 85.33 C_F \sqrt{\frac{\Delta P_1 \cdot T_{s1}}{P_s \cdot M_s}} = 85.33 (0.939) \times \sqrt{\frac{(0.62)(159 + 460)}{(30.07)(26.22)}} \\
 U_{s1} &= 49.9 \text{ ft/s} \\
 U_{s_{avg}} &= \frac{2424 \text{ m/s}}{48} \\
 U_{s_{avg}} &= 50.5 \text{ ft/s} \times 1 \text{ m} / 3.281 \text{ ft} = 15.4 \text{ m/s}
 \end{aligned}$$

Point: T4-2-2
 $T_s = 159^\circ \text{F}$
 $\Delta P = 0.62 \text{ in H}_2\text{O}$

The cross-sectional area of the stack (A_s) in ft^2 is:

$$\begin{aligned}
 A_s &= \frac{\pi (D \text{ ft})^2}{4} & D &= 139 \text{ in} \cdot \frac{1 \text{ ft}}{12 \text{ in}} = 11.5 \text{ ft} \\
 A_s &= \frac{\pi}{4} \times (11.5 \text{ ft})^2 \\
 A_s &= 0.7854 \times 132.25 \text{ ft}^2 \\
 A_s &= 103.9 \text{ ft}^2
 \end{aligned}$$

The volumetric stack gas flowrate on a dry-basis at reference conditions (Q_s) in ft^3/hr is:

$$\begin{aligned}
 Q_s &= 3600 \text{ s/hr} \times U_s \text{ ft/s} \times A_s \text{ ft}^2 \times (1 - B_{wO}) \times \frac{T_{\text{ref}} \text{ } ^\circ\text{R}}{T_{s, \text{avg}} \text{ } ^\circ\text{R}} \times \frac{P_s \text{ in.Hg}}{P_{\text{ref}} \text{ in.Hg}} \\
 Q_s &= 3600 \times \frac{50.5 \text{ ft}}{\text{s}} \times 103.9 \text{ ft}^2 \times (1 - 0.304) \times \frac{77 + 460 \text{ } ^\circ\text{R}}{610 \text{ } ^\circ\text{R}} \times \frac{30.03 \text{ in.Hg}}{29.92 \text{ in.Hg}} \\
 Q_s &= 3600 \times \frac{50.5 \text{ ft}}{\text{s}} \times 103.9 \text{ ft}^2 \times 0.696 \times 1.270 \times 1.01 \\
 Q_s &= 114944.68 \text{ ft}^3/\text{hr} \times 1 \text{ hr} / 60 \text{ min} = 191574.5 \text{ ft}^3/\text{min} \\
 Q_s &= 191574.5 \text{ ft}^3/\text{min} \times 1 \text{ m}^3 / 35.31 \text{ ft}^3 \times 1 \text{ min} / 60 \text{ s} = 90.4 \text{ m}^3/\text{s}
 \end{aligned}$$

The total amount of particulate matter collected (Mp) in mg is:

$$M_p = \underline{1,249} \text{ mg} \quad (\text{excluding impingers})$$

The concentration of the particulate matter in the stack gas on a dry basis at reference conditions (Cp) in lb/ft³ is:

$$C_p = 2.205 \times 10^{-6} \text{ lb/mg} \times \frac{M_p \text{ mg}}{V_{mc} \text{ ft}^3}$$

$$C_p = 2.205 \times 10^{-6} \text{ lb/mg} \times \frac{1,249 \text{ mg}}{64.0 \text{ ft}^3}$$

$$C_p = \underline{4.30 \times 10^{-5}} \text{ lb/ft}^3 \times 453,590 \text{ mg/lb} \times 35.31 \text{ ft}^3/\text{m}^3 = \underline{689} \text{ mg/m}^3$$

The emission rate of the particulate matter from the stack on a dry basis at reference conditions (ERp) in lb/hr is:

$$E_{rp} = C_p \text{ lb/ft}^3 \times Q_s \text{ ft}^3/\text{hr}$$

$$E_{rp} = \frac{4.30 \times 10^{-5} \text{ lb}}{\text{ft}^3} \times \frac{11,494,468 \text{ ft}^3}{\text{hr}}$$

$$E_{rp} = \underline{495} \text{ lb/hr} \times 1 \text{ kg}/2.20 \text{ lb} = \underline{225} \text{ kg/hr} \quad (\text{rounding error})$$

Appendix F

Operational Data

	Kiln					PB				RB			
	ca:6fc8010	ca:6ax8030a.p	ca:6ax8020.	ca:6fc8726.pv		pb:6ax8021.	pb:6fc8013.	CALC for		rb:6fc6554	rb:6fc8570.p	Daily Oil	
	.pv	v	p			p	p	bark		.pv	v		
	Natural Gas Flow To Burner	KILN BURNER HEAT INPUT 2	Kiln Oil/Gas Ratio	Mud to Thickener Flow		PB Steam Flow	PB Oil Flow			Liquor Dry Flow	Total RB Steam Flow	Usage	
	scfm	mmBtu/hr	%	GPM		kpph	kpph	T/day		KPPH	kpph	kpph	
8/18/14 7:00 AM	983.3	58.0	0.0	200.1		131.6	0.1	661.0		147.3	407.2	0.0	
8/19/14 8:00 AM	983.3	58.0	0.0	199.9		136.5	0.1			148.8	412.2		
8/19/14 9:00 AM	982.3	58.9	0.0	200.0		128.2	0.1			150.7	418.8		
8/19/14 10:00 AM	947.0	58.8	0.0	200.1		131.2	0.1			150.8	412.5		
8/19/14 11:00 AM	918.9	58.1	0.0	199.8		123.3	0.1			151.1	420.5		
8/19/14 12:00 PM	916.7	66.0	0.0	200.3		132.5	0.1			150.9	421.2		
8/19/14 1:00 PM	918.7	58.0	0.0	200.0		133.4	0.1			151.0	415.3		
8/19/14 2:00 PM	945.7	58.7	0.0	200.0		120.5	0.1			151.0	417.5		
8/19/14 3:00 PM	949.8	57.0	0.0	200.0		123.7	0.1			151.0	416.9		
8/19/14 4:00 PM	938.0	58.2	0.0	198.0		128.7	0.1			150.8	422.2		
8/19/14 5:00 PM	918.7	55.0	0.0	200.0		132.2	0.1			151.0	417.5		
8/19/14 6:00 PM	918.7	55.0	0.0	200.0		128.7	0.1			151.1	419.2		
8/19/14 7:00 PM	918.7	58.0	0.0	200.1		128.5	0.1			151.1	418.0		
8/19/14 8:00 PM	918.6	58.0	0.0	200.2		123.3	0.1			150.8	423.9		
8/19/14 9:00 PM	918.6	58.0	0.0	200.1		121.4	0.1			150.8	421.3		
8/19/14 10:00 PM	918.7	58.0	0.0	200.3		118.9	0.1			151.2	422.2		
8/19/14 11:00 PM	918.6	58.0	0.0	200.0		122.0	0.1			151.1	423.3		
8/20/14 12:00 AM	918.7	55.0	0.0	200.0		116.8	0.1			151.0	424.8		
8/20/14 1:00 AM	918.7	58.0	0.0	200.1		128.7	0.1			151.2	418.1		
8/20/14 2:00 AM	918.8	55.0	0.0	199.9		135.3	0.1			148.4	408.1		
8/20/14 3:00 AM	919.7	55.0	0.0	199.8		128.0	0.1			148.4	415.7		
8/20/14 4:00 AM	918.6	55.0	0.0	200.1		123.2	0.1			150.0	423.4		
8/20/14 5:00 AM	918.7	55.0	0.0	200.0		130.2	0.1			150.1	417.0		
8/20/14 6:00 AM	918.7	55.0	0.0	200.0		131.8	0.1			150.8	414.3		
8/20/14 7:00 AM	918.6	55.0	0.0	200.4		123.5	0.1	847.0		154.5	420.3	0.0	
8/20/14 8:00 AM	918.6	55.0	0.0	200.2		110.4	0.1			154.9	435.7		
8/20/14 9:00 AM	918.7	55.0	0.0	199.9		118.9	0.1			155.0	433.3		
8/20/14 10:00 AM	918.7	55.0	0.0	200.1		113.6	0.1			154.8	432.3		
8/20/14 11:00 AM	918.7	55.0	0.0	198.8		118.3	0.1			155.0	430.7		
8/20/14 12:00 PM	918.6	58.0	0.0	200.1		106.4	0.1			155.0	430.6		
8/20/14 1:00 PM	918.6	58.0	0.0	200.0		112.2	0.1			155.2	430.6		
8/20/14 2:00 PM	918.7	58.0	0.0	200.0		132.4	0.1			153.8	418.6		
8/20/14 3:00 PM	918.7	58.0	0.0	200.1		128.7	0.1			155.1	423.3		
8/20/14 4:00 PM	918.6	58.0	0.0	199.9		131.6	0.1			154.9	427.2		
8/20/14 5:00 PM	918.7	58.0	0.0	199.8		134.4	0.1			154.9	420.5		
8/20/14 6:00 PM	918.8	58.0	0.0	200.2		120.2	0.1			155.0	429.5		
8/20/14 7:00 PM	918.8	58.0	0.0	199.8		128.2	0.1			154.9	426.5		
8/20/14 8:00 PM	918.6	58.0	0.0	199.8		118.2	0.1			154.8	426.5		
8/20/14 9:00 PM	918.7	58.0	0.0	195.8		124.8	0.1			154.9	428.7		
8/20/14 10:00 PM	918.7	58.0	0.0	199.0		128.3	0.1			155.0	424.7		
8/20/14 11:00 PM	918.7	55.0	0.0	203.0		132.3	0.1			154.7	419.3		
8/21/14 12:00 AM	902.0	54.1	0.0	203.9		125.5	0.1			155.0	424.4		
8/21/14 1:00 AM	883.4	53.0	0.0	205.1		128.8	0.1			155.0	426.3		
8/21/14 2:00 AM	883.3	53.0	0.0	205.3		128.2	0.1			154.1	418.4		
8/21/14 3:00 AM	883.2	53.0	0.0	205.1		127.4	0.1			154.4	420.0		
8/21/14 4:00 AM	895.5	53.7	0.0	205.0		141.7	0.1			153.1	412.8		
8/21/14 5:00 AM	911.8	54.7	0.0	201.8		147.8	0.1			149.6	407.3		
8/21/14 6:00 AM	937.9	58.3	0.0	199.8		142.8	0.1			150.7	412.5		
8/21/14 7:00 AM	950.0	57.0	0.0	200.0		139.8	0.1	578.0		150.1	408.4	0.0	
8/21/14 8:00 AM	950.0	57.0	0.0	199.9		41.1	0.1			150.2	412.7		
8/21/14 9:00 AM	950.1	57.0	0.0	200.1		42.1	0.1			148.5	409.2		
8/21/14 10:00 AM	942.9	58.5	0.0	199.9		51.7	0.1			131.4	388.9		
8/21/14 11:00 AM	933.3	58.1	0.0	200.2		93.4	0.1			129.1	357.7		
8/21/14 12:00 PM	933.3	58.0	0.0	202.3		54.4	0.1			135.5	371.4		
8/21/14 1:00 PM	935.8	58.2	0.0	200.4		98.2	0.1			118.3	325.7		
8/21/14 2:00 PM	948.5	58.9	0.0	199.9		118.3	0.1			124.1	325.8		
8/21/14 3:00 PM	950.0	57.0	0.0	199.9		120.2	0.1			123.9	337.4		
8/21/14 4:00 PM	950.1	57.0	0.0	200.0		153.3	0.1			125.2	338.1		
8/21/14 5:00 PM	950.0	57.0	0.0	200.0		128.9	0.1			126.3	338.7		
8/21/14 6:00 PM	950.0	57.0	0.0	200.0		127.4	0.1			126.3	342.8		
8/21/14 7:00 PM	950.0	57.0	0.0	199.7		178.8	2.0			126.0	345.3		
8/21/14 8:00 PM	918.5	55.0	0.0	200.1		182.8	3.7			126.0	343.3		
8/21/14 9:00 PM	900.1	54.1	0.0	205.1		178.8	4.3			130.4	352.8		
8/21/14 10:00 PM	900.0	54.0	0.0	205.0		144.7	1.3			139.8	385.3		

Kiln					PB				RB					
ca:8fc8010		ca:6ax8030a.p	ca:6ax8020.		pb:5ax8021.		pb:5fc8013. CALC for		rb:5fc8554		rb:5fx8570.p			
.pv		v	pv		pv		pv		bark		.pv		Daily Oil	
Natural Gas Flow		KILN BURNER	Kiln Oil/Gas		Mud to Thickener		PB Steam				Heavy Black			
To Burner		HEAT INPUT 2	Ratio		Flow		Flow		PB Oil Flow		Liquor Dry		Total RB	
scfm		mmBtu/hr	%		GPM		kpph		kpph		Flow KPPH		Steam Flow kpph	Usage kpph
8/24/14 3:00 PM	902.1	54.2	0.0		200.1		89.7	0.1			155.0	434.8		
8/24/14 4:00 PM	900.0	54.0	0.0		202.7		89.0	0.1			155.1	433.6		
8/24/14 5:00 PM	900.2	54.0	0.0		200.1		74.3	0.1			154.9	436.5		
8/24/14 6:00 PM	900.0	54.0	0.0		200.0		75.4	0.1			155.8	438.3		
8/24/14 7:00 PM	900.0	54.0	0.0		200.1		98.8	0.1			152.1	425.4		
8/24/14 8:00 PM	900.0	54.0	0.0		200.1		92.9	0.1			152.7	426.1		
8/24/14 9:00 PM	900.0	54.0	0.0		200.0		79.9	0.1			152.8	429.5		
8/24/14 10:00 PM	900.0	54.0	0.0		199.9		85.2	0.1			153.1	431.1		
8/24/14 11:00 PM	900.0	54.0	0.0		200.0		93.4	0.1			154.4	432.9		
8/25/14 12:00 AM	900.0	54.0	0.0		200.1		93.8	0.1			154.8	431.7		
8/25/14 1:00 AM	900.0	54.0	0.0		195.6		93.2	0.1			154.9	431.9		
8/25/14 2:00 AM	929.4	55.7	0.0		199.9		97.6	0.1			155.0	435.4		
8/25/14 3:00 AM	933.3	55.9	0.0		200.1		108.5	0.1			154.9	431.8		
8/25/14 4:00 AM	933.4	55.9	0.0		200.0		86.3	0.1			155.2	438.9		
8/25/14 5:00 AM	933.3	56.0	0.0		200.0		95.9	0.1			155.0	439.4		
8/25/14 6:00 AM	933.3	56.0	0.0		200.1		112.7	0.1			155.2	430.3		
8/25/14 7:00 AM	933.3	56.0	0.0		200.1		101.1	0.1	517.0		156.3	434.8	0.0	
8/25/14 8:00 AM	933.4	56.0	0.0		199.9		89.7	0.1			157.1	434.7		
8/25/14 9:00 AM	933.2	56.0	0.0		200.3		78.3	0.1			157.2	438.7		
8/25/14 10:00 AM	933.2	56.0	0.0		199.9		71.1	0.1			158.9	442.3		
8/25/14 11:00 AM	933.4	56.0	0.0		199.8		78.8	0.1			157.3	434.8		
8/25/14 12:00 PM	933.3	56.0	0.0		200.1		77.0	0.1			155.4	434.3		
8/25/14 1:00 PM	933.3	56.0	0.0		200.0		90.9	0.1			150.3	418.4		
8/25/14 2:00 PM	933.3	56.0	0.0		200.0		81.1	0.1			150.1	419.1		
8/25/14 3:00 PM	933.3	56.0	0.0		200.0		83.5	0.1			183.9	438.7		
8/25/14 4:00 PM	933.4	56.0	0.0		200.0		99.2	0.1			157.1	435.1		
8/25/14 5:00 PM	933.3	56.0	0.0		200.1		102.1	0.1			156.9	428.4		
8/25/14 6:00 PM	933.4	56.0	0.0		200.0		103.7	0.1			157.2	438.2		
8/25/14 7:00 PM	933.3	56.0	0.0		200.0		104.3	0.1			157.1	433.2		
8/25/14 8:00 PM	933.4	56.0	0.0		200.0		107.8	0.1			158.7	434.7		
8/25/14 9:00 PM	933.3	56.0	0.0		200.0		108.7	0.1			158.8	430.9		
8/25/14 10:00 PM	933.4	56.0	0.0		199.9		113.7	0.1			156.8	429.2		
8/25/14 11:00 PM	933.4	56.0	0.0		200.2		111.8	0.1			157.2	429.6		
8/26/14 12:00 AM	933.3	56.0	0.0		200.0		120.3	0.1			158.9	427.2		
8/26/14 1:00 AM	933.3	56.0	0.0		202.8		114.7	0.1			157.1	431.7		
8/26/14 2:00 AM	933.4	56.0	0.0		200.2		117.8	0.1			157.0	430.8		
8/26/14 3:00 AM	933.3	56.0	0.0		200.1		109.1	0.1			158.9	435.3		
8/26/14 4:00 AM	933.3	56.0	0.0		200.1		118.6	0.1			158.8	429.3		
8/26/14 5:00 AM	933.3	56.0	0.0		200.0		114.7	0.1			157.0	431.7		
8/26/14 6:00 AM	933.3	56.0	0.0		200.1		118.8	0.1			158.0	428.1		
8/26/14 7:00 AM	933.3	56.0	0.0		200.0		112.1	0.1	522.0		158.2	428.1	0.0	
8/26/14 8:00 AM	933.3	56.0	0.0		200.1		107.3	0.1			157.8	438.6		
8/26/14 9:00 AM	933.3	56.0	0.0		200.1		111.7	0.1			158.1	438.4		
8/26/14 10:00 AM	933.4	56.0	0.0		199.9		98.1	0.1			157.8	437.1		
8/26/14 11:00 AM	933.3	56.0	0.0		199.8		85.8	0.1			158.0	440.4		
8/26/14 12:00 PM	933.4	56.0	0.0		201.8		99.2	0.1			158.1	437.2		
8/26/14 1:00 PM	933.4	56.0	0.0		199.9		95.2	0.1			157.9	437.1		
8/26/14 2:00 PM	933.4	56.0	0.0		200.8		105.7	0.1			158.0	430.4		
8/26/14 3:00 PM	933.2	56.0	0.0		199.9		104.0	0.1			158.0	434.4		
8/26/14 4:00 PM	933.4	56.0	0.0		199.9		94.9	0.1			158.0	441.6		
8/26/14 5:00 PM	933.3	56.0	0.0		199.9		102.4	0.1			157.9	433.3		
8/26/14 6:00 PM	933.4	56.0	0.0		200.1		104.0	0.1			157.8	438.9		
8/26/14 7:00 PM	933.4	56.0	0.0		199.9		101.2	0.1			157.9	433.8		
8/26/14 8:00 PM	933.4	56.0	0.0		200.0		84.3	0.1			158.0	437.3		
8/26/14 9:00 PM	933.3	56.0	0.0		199.9		92.2	0.1			158.0	438.8		
8/26/14 10:00 PM	933.3	56.0	0.0		200.1		102.4	0.1			158.2	432.4		
8/26/14 11:00 PM	933.4	56.0	0.0		199.9		88.2	0.1			157.8	435.1		
8/27/14 12:00 AM	933.4	56.0	0.0		200.1		99.7	0.1			158.4	431.4		
8/27/14 1:00 AM	933.3	56.0	0.0		200.8		101.9	0.1			158.1	429.8		
8/27/14 2:00 AM	933.3	56.0	0.0		199.9		111.1	0.1			158.0	430.7		
8/27/14 3:00 AM	933.3	56.0	0.0		200.0		114.9	0.1			157.9	432.4		
8/27/14 4:00 AM	933.3	56.0	0.0		199.8		109.2	0.1			157.9	430.4		
8/27/14 5:00 AM	933.3	56.0	0.0		199.8		83.0	0.1			157.9	436.8		
8/27/14 6:00 AM	933.4	56.0	0.0		200.0		82.8	0.1			158.0	434.8		