

**Source Emissions Testing –
Summer Round 2015**



Prepared for:

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File: 121413456
October 16, 2015

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EXECUTIVE SUMMARY

Northern Pulp Nova Scotia Corporation, referred to herein as Northern Pulp, retained Stantec Consulting Ltd. to conduct source emissions testing at the Kraft pulp mill in New Glasgow, Nova Scotia. Source emissions testing were conducted on the Recovery Boiler and the Power Boiler to fulfill the conditions specified in the current Certificate of Approval to Operate (CoA) 2011-076657-R03. The source emissions testing campaign was performed according to the pre-test plan submitted to the Nova Scotia Department of Environment. The testing was conducted on September 15-18, 2015.

In this report, source emissions testing data are presented for measurements which include concentrations and emission rates of combustion gases and total particulate matter (PM) as well as exhaust gas temperature, moisture content, velocity, and volumetric flow rate on the Recovery and Power Boilers.

The measured concentration of PM from the Recovery Boiler was below the stack limit of 77 mg/Rm³ (corrected to 11% oxygen).

The measured concentration of PM from the Power Boiler was above the stack limit of 150 mg/Rm³ (corrected to 11% oxygen).

A summary of the results of the source emissions testing is provided in Table E.1.

Table E.1 Source Emissions Testing Results

Exhaust Gas Parameters	Recovery Boiler	Power Boiler
Total Particulate Matter – TPM (mg/Rm ³ at 11% O ₂)	3.9	190
Sulphur Dioxide – SO ₂ (mg/Rm ³)	87.2	ND
Nitrogen Oxides – NO _x (mg/Rm ³)	-	103
Carbon Monoxide – CO (mg/Rm ³)	1,132	126
Volumetric Flow Rate (Rm ³ /s)	72.0	33.2
Velocity (m/s)	12.3	16.8
Temperature (°C)	68.1	55.4
Moisture Content (%)	30.6	17.5
Oxygen - O ₂ (%)	5.3	12.2
Carbon Dioxide - CO ₂ (%)	10.4	6.4

Production for September 15, 16, 17 and 18 was 742, 833, 884 and 899 air dry metric tonnes of pulp (admt) respectively.



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1.0 INTRODUCTION

Northern Pulp Nova Scotia Corporation, referred to herein as Northern Pulp, retained Stantec Consulting Ltd. (Stantec) to conduct source emissions testing at the Kraft pulp mill in New Glasgow, Nova Scotia. Source emissions testing were conducted on the Recovery Boiler and the Power Boiler to fulfill the conditions specified in the current Certificate of Approval to Operate (CoA) 2011-076657-R03. The source emissions testing campaign was performed according the pre-test plan submitted to the Nova Scotia Department of Environment.

In this report, source emissions testing data are presented for combustion gases, total particulate matter (PM), exhaust gas temperature, exhaust flow rate, moisture content, velocity, and volumetric flow rate.

This report is in five chapters. Chapter 1 contains the introduction and the scope of work for the project. The study approach and a brief description of the various parts of the project are in Chapter 2. Chapter 3 contains a brief description of the testing methodologies, equipment, and calibration techniques used during the source emissions testing program. In Chapter 4, the results of the source emissions testing are presented and discussed, and concluding remarks are presented in Chapter 5. Appendices A through D contain supporting information for the report.

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2.0 OVERALL APPROACH

The project consisted of five parts:

1. submission of the pre-test plan
2. site preparation and preliminary survey
3. on-site source emissions testing
4. laboratory analysis
5. information review and reporting

Each of these parts is described below.

2.1 SUBMISSION OF PRE-TEST PLAN

The on-site testing was conducted in accordance with the Pre-Test Plan (Appendix A) submitted on February 20, 2015 to Nova Scotia Environment (NSE). The Pre-Test Plan outlined the rationale for the selection of the associated contaminants to be tested, as well as the methodologies proposed for conducting the source testing on the exhaust stacks.

2.2 ON-SITE SOURCE EMISSIONS TESTING

Stantec set up the source emissions testing equipment and conducted a preliminary survey to measure the exhaust gas temperature, velocity, and flue gas composition in each of the boiler stacks. The data from this survey was used to determine the appropriate nozzle size to conduct isokinetic sampling (where the velocity of the gas entering the nozzle is equal to the gas velocity in the stack) for particulate matter during the source emissions testing part of the work.

Three (3) tests for total particulate matter and combustion gases were conducted at defined sampling locations on the exhaust stacks of the Recovery Boiler and the Power Boiler. The testing was completed in compliance with the sampling methods presented in Table 2.1, in accordance with the Air Quality Regulation, under the Environment Act, Section 112 issued by Nova Scotia Environment (NSE) and the requirements of the facility's approval (2011-076657-R03) issued by the NSE.

The methodologies used for testing the emissions from each exhaust stack are summarized in Table 2.1.



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Table 2.1 Source Emissions Testing Matrix

Source	Number of Samples per Source	Approval Condition	Parameter	Sampling Method
Recovery Boiler	3	6. a)	Total Particulate Matter (PM)	EPS 1/RM/8
	3	-	Combustion Gases	EPS 1/RM/15
Power Boiler	3	6. a)	Total Particulate Matter (PM)	EPS 1/RM/8
	3	-	Combustion Gases	EPS 1/RM/15

2.3 LABORATORY ANALYSIS

Prior to the particulate matter testing, several filters were conditioned and pre-weighed. Following the testing, particulate matter was recovered from the nozzle, the sampling probe and the in-line filter. Following testing the filter, containing the particulate sample, was conditioned and weighed, and the net weight of the collected particulate matter was determined. After each test, the probe and nozzle were rinsed with acetone and this acetone was collected, placed into a pre-weighed container and evaporated until dry. The amount of particulate for each part of the sample was determined gravimetrically, and the mass of particulate matter collected for each test was calculated as the sum of the particulate matter collected in the filter, probe, and nozzle rinse. The contents of the impingers were recovered gravimetrically for particulate matter and reported separately. These recoveries were performed at Stantec's laboratory in Fredericton, New Brunswick.

2.4 INFORMATION REVIEW AND REPORTING

The data collected in the field, along with data from the laboratory analyses, were entered into the Stantec's source emissions testing spreadsheets for analysis. Emissions calculations were then performed to produce the detailed source emissions testing information. Spreadsheet calculations were verified by hand, and numerous spot checks of spreadsheet formulas were conducted to confirm the accuracy of data. Summary tables were prepared and incorporated into this report for submission to Northern Pulp.



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3.0 TEST METHODS, EQUIPMENT, AND CALIBRATIONS

This section contains a description of the methods and equipment used to conduct the source emissions testing campaign. The calibration procedures used to ensure the quality of the source emissions testing data are also summarized in this section.

3.1 SAMPLING PROCEDURES AND EQUIPMENT

The following sub-sections contain brief descriptions of the sampling equipment and methodologies used during the source emissions testing campaign.

3.1.1 Total Particulate Matter

Particulate matter emissions from the Recovery Boiler and Power Boiler exhaust stacks were measured in accordance with the Environment Canada Reference Method EPS 1/RM/8, entitled *Reference Methods for Source Testing: Measurement of Releases of Particulate from Stationary Sources*.

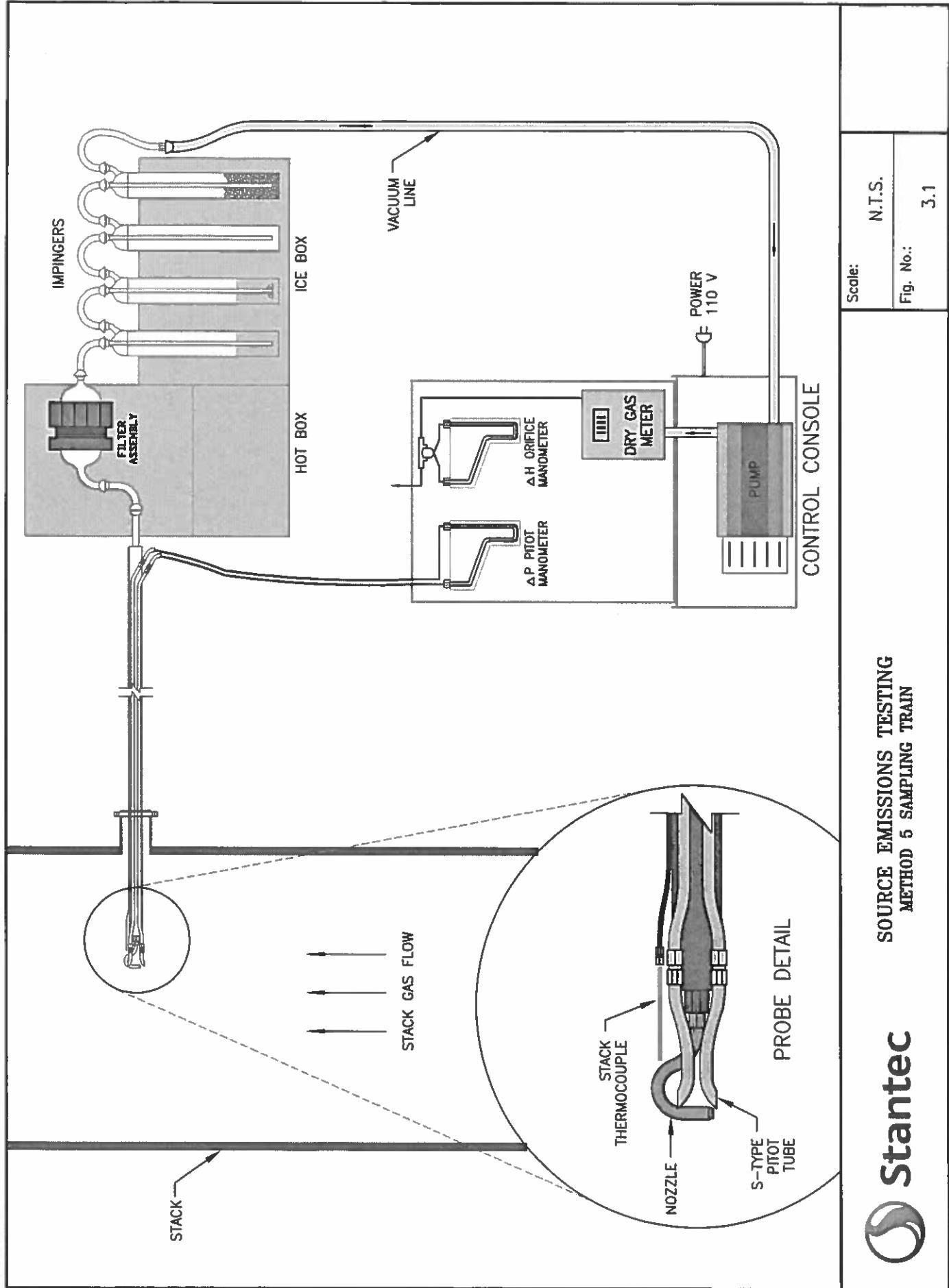
The sampling train, used specifically for isokinetic sampling of particulate matter, is described in detail in EPS 1/RM/8, and is generally referred to as the 'Method 5' sampling train for particulate matter, named after the United States Environmental Protection Agency (US EPA) protocol. The sampling train consists of several different components which include: a heated sampling probe (a nozzle, stainless steel liner, thermocouple, and pitot tube assembly), a heated sample case containing a filter, an ice box containing impinger glassware, and an umbilical cord leading to the pump and control console. A schematic of the sampling system is shown in Figure 3.1. The operation of the Method 5 sampling train can be generally described as follows.

Exhaust gases are drawn through the probe nozzle at or near isokinetic conditions (i.e., where the gas velocity in the nozzle is at the same velocity as the gas in the stack). The gases are then drawn through the inner stainless steel liner of the electrically heated sampling probe to the other components of the sampling train.

A pitot tube assembly is attached to the probe next to the nozzle to measure the exhaust gas velocity in the area of the probe nozzle. Using the differential pressure reading on the control console, the desired nozzle flow rate is determined from the differential pressure across a calibrated orifice.

The exhaust gases are drawn from the probe liner through a pre-weighed glass fiber filter, in the hot side of the sampling unit, and then through pre-weighed impingers in an ice bath to cool the gases and condense the moisture in the gas, before the gas enters the umbilical cord.





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The umbilical cord carries the filtered, cooled exhaust gases from the sampling site to the control console. The control console contains a fiber vane vacuum pump, which is used to draw the exhaust gases through the sampling train. A calibrated dry gas meter records the volume of gas sampled.

After completion of testing, the impingers are re-weighed, with the difference in mass corresponding to the mass of water collected. This measurement is used to calculate the moisture content of the exhaust gas.

Total particulate matter is determined gravimetrically at Stantec's laboratory in Fredericton, New Brunswick.

Appendix B contains the calibration data.

3.1.2 Combustion Gases

The combustion gases (O_2 , CO_2 , CO, NO_x, and SO₂) were sampled according to the Environment Canada reference method EPS 1/RM/15, entitled *Reference Method for the Monitoring of Gaseous Emissions from Fossil Fuel-fired Burners*. In this method, samples of flue gas are drawn through a probe, non-isokinetically, from a single point near the centre of the stack. The combustion gases were analyzed using a Testo 350 XL Flue Gas Analyzer manufactured by Testo GmbH and Co. This unit is equipped with electrochemical cells that are used to measure the concentrations of oxygen, carbon dioxide, sulphur dioxide, nitrogen oxides, carbon monoxide, and total hydrocarbons, in accordance with EPS 1/RM/15. The system is equipped with a flue gas probe that has an integrated filter trap and condensate trap and a housing unit that contains the pump and the electrochemical cells. The equipment is manufactured and calibrated to provide an accuracy of +/- 4% for carbon monoxide, nitrogen oxides, and sulphur dioxide, +/- 0.2% for oxygen, and +/- 5% for carbon dioxide.

3.2 QUALITY ASSURANCE AND QUALITY CONTROL

Throughout the source emissions testing program, quality assurance and quality control procedures were applied to confirm the accuracy of the accurate emissions data. These checks were performed by test personnel throughout the program under the guidance of the source testing crew chief in the field and the project manager during post testing review.

The quality control (QC) checks included the following:

- use of standardized checklists and field notebooks to ensure completeness, traceability, and comparability of the process information and samples collected
- field checking of standardized forms by a second person to confirm completeness
- testing for cyclonic or reverse flow, as well as stratified flow conditions
- leak checks of sampling trains



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Equipment was calibrated according to the protocols and schedule as prescribed by Environment Canada. These calibrations include the following:

Pitots: Calibrated in a wind tunnel with probe and nozzles attached.

Gas meters: Calibrated using a critical orifice calibration set.

Nozzle: Four diameter measurements made using a micrometer across the sharpened edges.

Thermocouples: Calibrated using a potentiometric technique.

Gas Analyzer: Calibrated against reference gases using standard calibration gases within the expected range of concentrations from the source.

Calibration data are in Appendix B of this report.

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4.0 RESULTS AND DISCUSSION

The results of the source emissions testing campaigns are provided and discussed in this section.

Appendices B through D contain supporting information including calibration information, field data sheets, and calculations.

4.1 EXHAUST STACK SAMPLE LOCATION DETAILS

Table 4.1 provides a summary of the sample location details for each exhaust stack sampled.

Table 4.1 Sample Location Details

Parameter	Recovery Boiler	Power Boiler
Stack Height – Above Grade (m)	69	51
Diameter / Equivalent Diameter (m)	3.51	1.93
Stack/Duct Description	Circular	Circular
Stack Orientation	Vertical	Vertical
Number of Sample Ports	4	2
Sample Port Diameter (m)	0.1	0.1
Location Upstream from any Disturbance,	>2	>2
Location Downstream from any Disturbance,	1.45	>4
Ideal or Non Ideal Flow Characteristics at The Sample Location ¹	Not Ideal	Not Ideal
Total Number of Sample Points	24	24
Number of Sample Points per Traverse	12	12
Sample Time per Point (min)	5	5
Sample time per Test for PM (min)	120	120
Sample time per test for combustion gases (min)	30	30

Notes:

¹ The exhaust gas flow characteristics at the sampling location are referred to as being "Ideal" if the sample ports are located in a straight section of stack at least eight stack diameters downstream and two stack diameters upstream of any flow disturbance.

4.2 RECOVERY BOILER

The results of the source emissions testing for total particulate matter and combustion gases from the Recovery Boiler exhaust stack are in Tables 4.2 and 4.3, respectively.



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Table 4.2 Source Testing Results - Recovery Boiler - Particulate Matter

Parameter	Test #1	Test #2	Test #3	Average	Stack Emission Limit
Test Date	Sept 15, 2015	Sept 16, 2015	Sept 16, 2015	-	-
% of Normal Maximum Operating Rate ¹	97.1	97.3	97.5	97.3	
Test Start	11:15	8:40	12:30	-	-
Test Duration (min)	120	120	120	120	-
Volume of Gas Sampled (Rm ³)	2.49	2.49	2.52	2.50	-
Average Isokineticity (%)	98	98	99	99	-
Total Volume of Moisture Collected in Impingers (mL)	802.9	827.6	805.6	812.0	-
Particulate Matter From Filter and Probe Wash (mg)	19.8	13.5	13.0	15.4	-
Particulate Matter From Impingers (mg)	8.0	8.1	72.9	29.7	-
Exhaust Gas Parameters					
Exhaust Gas Temperature (°C)	68.2	68.1	68.0	68.1	-
Exhaust Gas Moisture Content (%)	30.4	31.2	30.3	30.6	-
Exhaust Gas Velocity (m/s)	12.3	12.3	12.2	12.3	-
Exhaust Gas Volumetric Flow Rate (Rm ³ /s)	72.2	71.8	72.0	72.0	-
Oxygen - O ₂ (%)	5.3	5.5	5.2	5.3	-
Carbon Dioxide - CO ₂ (%)	10.4	10.4	10.5	10.4	-
<u>Total Particulate Matter - PM</u>					
Concentration at 11% O ₂ (mg/Rm ³)	5.04	3.49	3.26	3.93	77
Emission Rate (kg/hr)	2.07	1.41	1.34	1.60	-
Legend:					
°C	Degrees Celsius.				
m/s	Metres per second.				
Rm ³ /s	Dry cubic metres per second at reference conditions (25°C and 101.3 kPa).				
mg/Rm ³	Milligrams per dry cubic metre at reference conditions (25°C and 101.3 kPa).				
kg/hr	Kilograms per hour.				
1Normal maximum operating rate is 154,000 lb/hour black liquor as fired.					

The average measured concentration of particulate matter was 3.93 mg/Rm³ (corrected to 11% O₂), which is below the current stack emission limit of 77 mg/Rm³ presented in Table 5 of the facility's Approval (No. 2011-076657-A03).



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Table 4.3 Source Testing Results - Recovery Boiler - Combustion Gases

Parameter	Test #1	Test #2	Test #3	Average
Test Date	Sept 15, 2015	Sept 16, 2015	Sept 16, 2015	-
Test Duration (min)	30	30	30	30
Exhaust Gas Volumetric Flow Rate (Rm ³ /s)	72.2	71.8	72.0	72.0
<u>Sulphur Dioxide - SO₂</u>				
Concentration (ppm)	43.7	59.1	54.1	52.3
Concentration (mg/Rm ³)	72.6	99.3	89.6	87.2
Emissions Rate (kg/hr)	29.8	40.1	36.8	35.5
<u>Nitrogen Oxides - NO_x</u>				
Concentration (ppm)				-
Concentration (mg/Rm ³)				-
Emissions Rate (kg/hr)	Not available	Not available	Not available	-
<u>Carbon Monoxide - CO</u>				
Concentration (ppm)	2,033	305	627	988
Concentration (mg/Rm ³)	2,328	349	718	1,132
Emissions Rate (kg/hr)	606	90.1	186	294
Legend:				
Rm ³ /s Dry cubic metres per second at reference conditions (25°C and 101.3 kPa).				
mg/Rm ³ Milligrams per dry cubic metre at reference conditions (25°C and 101.3 kPa).				
kg/hr Kilograms per hour.				
Not available- an error in the electrochemical cell for NOX occurred during Recovery Boiler testing, therefore data are not available				

4.3 POWER BOILER

The results of the source emissions testing for total particulate matter and combustion gases from the Power Boiler exhaust stack are in Tables 4.4 and 4.5, respectively.

Table 4.4 Source Testing Results - Power Boiler - Particulate Matter

Parameter	Test #1	Test #2	Test #3	Average	Stack Emission Limit
Test Date	Sept 17, 2015	Sept 17, 2015	Sept 18, 2015	-	-
Steam Load (klb/hr)	123.0	126.3	122.2	123.8	
Test Start	9:10	13:40	8:00	-	-
Test Duration (min)	120	120	120	120	-
Volume of Gas Sampled (Rm ³)	1.37	1.45	1.50	1.44	-
Average Isokineticity (%)	104	100	103	102	-



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Table 4.4 Source Testing Results - Power Boiler - Particulate Matter

Parameter	Test #1	Test #2	Test #3	Average	Stack Emission Limit
Total Volume of Moisture Collected in Impingers (mL)	222.3	223.5	225.8	223.9	-
Particulate Matter From Filter and Probe Wash (mg)	251.8	258.7	205.1	238.5	-
Particulate Matter From Impingers (mg)	15.8	5.9	39.2	20.3	-
Exhaust Gas Parameters					
Exhaust Gas Temperature (°C)	56.1	55.1	55.2	55.4	-
Exhaust Gas Moisture Content (%)	18.1	17.3	16.9	17.5	-
Exhaust Gas Velocity (m/s)	15.9	17.2	17.3	16.8	-
Exhaust Gas Volumetric Flow Rate (Rm ³ /s)	31.2	34.1	34.4	33.2	-
Oxygen - O ₂ (%)	12.8	11.9	11.8	12.2	-
Carbon Dioxide - CO ₂ (%)	5.8	6.6	6.7	6.4	-
<u>Total Particulate Matter - PM</u>					
Concentration at 11% O ₂ (mg/Rm ³)	226	196	149	190	150
Emission Rate (kg/hr)	20.6	21.9	16.9	19.8	-
Legend:					
°C	Degrees Celsius.				
m/s	Metres per second.				
Rm ³ /s	Dry cubic metres per second at reference conditions (25°C and 101.3 kPa).				
mg/Rm ³	Milligrams per dry cubic metre at reference conditions (25°C and 101.3 kPa).				
kg/hr	Kilograms per hour.				
Klb/hr	Thousand pounds per hour				

The average measured concentration of particulate matter (corrected to 11% O₂) was 190 mg/Rm³, which is above the stack emission limit of 150 mg/Rm³ presented in Table 5 of the facility's Approval (No. 2011-076657-A03).

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Table 4.5 Source Testing Results - Power Boiler - Combustion Gases

Parameter	Test #1	Test #2	Test #3	Average
Test Date	Sept 17, 2015	Sept 17, 2015	Sept 18, 2015	-
Test Duration (min)	30	30	30	30
Exhaust Gas Volumetric Flow Rate (Rm ³ /s)	31.2	34.1	34.4	
<u>Sulphur Dioxide - SO₂</u>				
Concentration (ppm)	ND	ND	ND	-
Concentration (mg/Rm ³)	ND	ND	ND	-
Emissions Rate (kg/hr)	ND	ND	ND	-
<u>Nitrogen Oxides - NO_x</u>				
Concentration (ppm)	48.4	62.3	53.7	54.8
Concentration (mg/Rm ³)	91.1	117	101	103
Emissions Rate (kg/hr)	10.2	14.4	12.5	12.4
<u>Carbon Monoxide - CO</u>				
Concentration (ppm)	71.9	190	67.1	110
Concentration (mg/Rm ³)	82.3	218	76.9	126
Emissions Rate (kg/hr)	9.24	26.8	9.52	15.2
Legend:				
Rm ³ /s	Dry cubic metres per second at reference conditions (25°C and 101.3 kPa).			
mg/Rm ³	Milligrams per dry cubic metre at reference conditions (25°C and 101.3 kPa).			
kg/hr	Kilograms per hour.			
ND	not detected in sample			

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5.0 CLOSURE

This report has been prepared for the sole benefit of Northern Pulp Nova Scotia Corporation. This report may not be relied upon by any other person or entity without the express written consent of Stantec and Northern Pulp Nova Scotia Corporation. Any use of this report by a third party, or any reliance on decisions made based upon this report, are the responsibility of the third party. Stantec accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this report.

Stantec makes no representation or warranty with respect to this report, other than the work was undertaken by trained professional and technical staff in accordance with generally accepted engineering and scientific practices current at the time the work was performed. Any information or facts provided by others and referred to or utilized in the preparation of this report was assumed by Stantec to be accurate.

This study was undertaken exclusively for the purpose outlined herein and was limited to those contaminants and sources specifically referenced in this report. It should be noted that the measurements were taken over a relatively short time period on-site, and the emissions results may be considered representative only for the conditions present at the time of testing. This report cannot be used or applied under any circumstances to another location or situation or for any other purpose without further evaluation of the data and related limitations.

This report was prepared by Chris Lyons, P.Eng and reviewed by Vicki Corning, P.Eng. If you have any questions regarding the contents of this report, or require any additional information, please do not hesitate to contact the undersigned.



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Appendix A

Pre-test plan

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February 20, 2015
File: 121413456

Attention: Mr. Marc Theriault
Nova Scotia Environment
20 Pumphouse Road
Pictou, NS B2H 5C6

Dear Mr. Theriault,

**Reference: Pre-Test Plan for Source Emissions Testing Northern Pulp,
Pictou Mill – 2015 Calendar Year**

Please accept this Pre-test Plan for the completion of source emissions required at the Pictou Mill in New Glasgow, Nova Scotia for the 2015 calendar year.

Introduction

Northern Pulp is required to perform source emissions testing on the Recovery Boiler, Lime Kiln, Smelt Dissolving Tank, Power Boiler and the High Level Roof Vent to fulfil the conditions specified in the current Certificate of Approval (CoA) to Operate 2011-076657-R03. The required annual testing for 2015 consists of:

- Recovery Boiler and Power Boiler particulate matter testing 4 times per year;
- Lime Kiln and Smelt Dissolving Tank particulate matter testing 2 times per year;
- Lime Kiln, High Level Roof Vent and Smelt Dissolving Tank total reduced sulphur (TRS) testing 2 times per year;
- One PM_{2.5} testing event per year on the four stacks noted above for particulate matter; and
- One Chlorine (Cl) and Chlorine Dioxide (ClO₂) event per year on the bleach plant exhaust (High Level Roof Vent being the source of these emissions).

Test Program Organization

The source emissions testing will be performed for:

Company Name: Northern Pulp
Company Address: P.O. Box 549, Station Main, New Glasgow, NS, B2H 5E8
Contact Name:
Position: Environmental/Technical Leader
Telephone Number: (902) 752-8461
Email: northernpulp.com



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**Reference: Pre-Test Plan for Source Emissions Testing Northern Pulp,
Pictou Mill – 2015 Calendar Year**

Sampling Company: Stantec Consulting Ltd.
Project Manager: Gillian Hatcher
Telephone Number: (902) 468-7777
Fax Number: (902) 468-9009
Email: @Stantec.com
Key Sampling Team: , with support from other staff as needed)

Source Emissions Testing Program

The proposed source emissions testing methodology and proposed sampling timeframes are presented in Table 1.

Table 1 Source Emissions Testing Matrix

Source	Number of Visits	Number of Tests per Visit	Parameter	Sampling Method	Proposed Timeframe
Recovery Boiler	4	3	Total Particulate Matter (PM)	EPS 1/RM/8	Winter, Spring, Summer, Fall
	4	3	Combustion Gases	EPS 1/RM/15	Winter, Spring, Summer, Fall
	1	3	Particle Size Analysis	Microscopic technique	Fall
Power Boiler	4	3	Total Particulate Matter (PM)	EPS 1/RM/8	Winter, Spring, Summer, Fall
	4	3	Combustion Gases	EPS 1/RM/15	Winter, Spring, Summer, Fall
	1	3	Particle Size Analysis	Microscopic technique	Fall
Lime Kiln	2	3	Total Particulate Matter (PM)	EPS 1/RM/8	Spring, Fall
	2	3	Combustion Gases	EPS 1/RM/15	Spring, Fall
	1	3	Particle Size Analysis	Microscopic technique	Fall
	2	3	Total Reduced Sulphur (TRS)	US EPA Method 16B/C	Spring, Fall
Smelt Dissolving Tank	2	3	Total Particulate Matter (PM)	EPS 1/RM/8	Spring, Fall
	2	3	Combustion Gases	EPS 1/RM/15	Spring, Fall
	1	3	Particle Size Analysis	Microscopic technique	Fall
	2	3	Total Reduced Sulphur (TRS)	US EPA Method 16B/C	Winter, Summer
High Level Roof Vent	2	3	Total Reduced Sulphur (TRS)	US EPA Method 16B/C	Spring, Fall
	2	3	Combustion Gases	EPS 1/RM/15	Spring, Fall



February 20, 2015
Mr. Marc Theriault
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Reference: Pre-Test Plan for Source Emissions Testing Northern Pulp,
Pictou Mill – 2015 Calendar Year

Table 1 Source Emissions Testing Matrix

Source	Number of Visits	Number of Tests per Visit	Parameter	Sampling Method	Proposed Timeframe
	1	3	Chlorine and chlorine dioxide	NCASI Special Report 91-07	Spring

Note:
Timeframes are as follows based on the approval deadlines-Winter: January-March 31, 2015, Spring: April – June 30, 2015, Summer: July-September 30, 2015, Fall: October-December 31, 2015

Details of each of the methods identified in Table 1, in addition to the preliminary testing methodology, are provided in the sections that follow.

Preliminary Testing: Upon arrival at each sampling location, Stantec will set up the source emissions testing equipment and conduct a preliminary survey to measure the average velocity, flue gas composition, and moisture content in the stack gases using EPS 1/RM/8 Methods B, C, and D, respectively. The data from this survey will be used to determine the appropriate nozzle size to conduct isokinetic sampling (where the velocity of the gas entering the nozzle is equal to the gas velocity in the stack) for particulate matter during the official testing part of the work. Verification for cyclonic or reverse flow will also be conducted during the preliminary survey, according to procedures outlined in the Environment Canada reference method EPS 1/RM/8.

Should fluctuations in the velocity pressure at a selected traverse point exceed 20% of the average pressure for that point; the diameter of the testing cross section will be reduced to include only those areas along the traverse which meet this requirement (less than 20% of the average). Although the diameter may be reduced, the number of sampling points along each traverse will remain the same as determined from EPS 1/RM/8, Method A, using the equivalent diameter.

Volumetric flow and exhaust gas emissions will be calculated using the full cross sectional area.

Particulate Matter: The source emissions testing of the Recovery Boiler, Lime Kiln, Smelt Dissolving Tank, and the Power Boiler for total particulate matter will be conducted in accordance with the Environment Canada reference method EPS 1/RM/8, entitled "Measurement of Releases of Particulate from Stationary Sources". In addition the alignment approach, as specified in the US EPA Guidance Document – GD-008, will be applied when source testing the Lime Kiln due to the cyclonic flow this source exhibits.

The particulate sampling train, used specifically for isokinetic sampling, is described in detail in EPS 1/RM/8, and is generally referred to as the "Method 5" sampling train for particulate matter (after the US EPA protocol). The sampling train has several different components which include: a heated sampling probe (a nozzle, stainless steel liner, thermocouple, and pitot tube assembly), a heated sample case containing a filter, an ice box containing impinger glassware, and an



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umbilical cord leading to the pump, and control console. A schematic of the sampling system is shown in Figure 1.

For all source tests, leak checks of the sampling train will be performed as per accepted US EPA and Environment Canada methods. For each official test, two (2) traverses with up to twelve (12) sampling points per traverse will be used. Sampling will be conducted for five (5) minutes per sampling point, up to a maximum sampling time of 120 minutes per test.

The amount of material caught in the impingers will be determined gravimetrically and reported separately from the calculated total particulate matter emissions. All particulate matter samples will be recovered and analyzed at the Stantec laboratory in Fredericton, NB.

Microscopic Analysis (Fine Particulate, PM_{2.5}): As per the facility's Industrial Approval to Operate, the Environment Canada EPS 1/RM/55 or an alternative method acceptable to the Department is required for PM_{2.5} testing. As the method quoted in the approval is not valid for stacks with potential for entrained water droplets in the exhaust (which applies to boilers and dissolving tank at Northern) or cyclonic flow (which applies to the Lime Kiln), we propose microscopic analysis of filters as the viable option. This method involves analysis of total particulate matter filters (collected as described above) for fine particulate percentage.

The particle size analyses will be performed by MVA Scientific Consultants, based in Duluth, GA, using a JEOL JSM-6500F field emission scanning electron microscope operating in automated mode under the control of a Thermo Scientific Noran System SIX x-ray analysis system, using their automated particle size analysis method.

Total Reduced Sulphur: The source emissions testing of the Lime Kiln, the Smelt Dissolving Tank and the High Level Roof Vent for total reduced sulphur will be conducted in accordance with US EPA Method 16B. In this method, the sample is extracted from the exhaust gas of the stack through a heated Teflon line. The sample is chilled and then passes through an SO₂ analyzer to measure SO₂ from the source. The sample exits the analyzer and is then passed through a furnace where all sulphur compounds in the gas stream are thermally oxidized to SO₂, this SO₂ is measured in a second inline analyzer. The difference in the initial SO₂ and the final SO₂ measurement is the total reduced sulphur concentration (reported as H₂S). The analyzers are both Western Research SO₂ non-dispersive ultra-violet (NDUV) continuous analyzer. Monitoring will be conducted continuously over a 24 hour period as required by the approval condition.

Chlorine, Chlorine Dioxide (Cl₂, ClO₂): Sampling will be conducted in accordance with NCASI's sampling method which consists of the extraction of a sample bubbling through midget impingers and subsequent analysis by titration. The sampling train for the Cl₂ and ClO₂ consists of series of three mini impingers, connected by Teflon tubing. The first two impingers each contain 20 ml of potassium iodide (KI) solution buffered with potassium di-hydrogen phosphate (KH₂PO₄). The third impinger contains silica gel to remove any remaining moisture from the gas stream. The impingers are cooled by an ice bath, and the dried gas is then drawn through the sampling train with a calibrated pump. Total sampling time for each test is sixty (60) minutes.



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Following completion of each test for Cl₂ and ClO₂, the contents of the first two impingers are combined in a pre-cleaned beaker. Subsequent analysis via titration will be performed onsite by Stantec. The combined impinger solutions and de-ionized water rinse of the sample line and empty impingers would be titrated with sodium thiosulphate solution (0.010 N). The volume of titrant required to reach the first colorless endpoint would be recorded on a recovery data form. Five (5) ml of 10% sulphuric acid would be added to the sample and the titration continued. The volume of titrant required to reach the second colorless endpoint would be recorded on a recovery data form. These titrations would be conducted on site shortly following sampling by one of the field staff during the testing due to the instability of the samples, which begin to degrade after 24 hours.

Combustion Gases:

The combustion gases (O₂, CO₂, CO, NO_x, and SO₂) will be sampled according to the Environment Canada reference method EPS 1/RM/15, entitled *Reference Method for the Monitoring of Gaseous Emissions from Fossil Fuel-fired Burners*. In this method, samples of flue gas are drawn through a probe, non-isokinetically, from a single point near the centre of the stack. An ENERAC Model 500 Micro-Emission Analyzer, manufactured by ENERAC Inc., will be used to conduct the sampling. The Model 500 is equipped with a flue gas probe that has an integrated filter trap and condensate trap, and a housing unit that contains the pump and the electrochemical cells which are used to measure concentrations of sulphur dioxide, nitrogen oxides, carbon monoxide, carbon dioxide, and oxygen.

In accordance with the regulatory requirements for compliance testing, three replicate tests for each contaminant will be conducted on each stack.

Reporting

As per Approval No. 2011-076657-R03, actual particulate matter emission rates will be reported in units of g/s. The concentration released to the atmosphere will be reported in units of mg/m³ at reference conditions of 25 °C and 101.3 kPa corrected for 11 % oxygen for the Recovery Boiler and Power Boiler and in units of kg/adubmt for the Lime Kiln and the Dissolving Tank. Fine particulate matter concentrations for the Lime Kiln, Dissolving Tank, Power Boiler and Recovery Boiler will be reported in units of mg/m³ at reference conditions of 25 °C and 101.3 kPa corrected for 11 % oxygen. Total reduced sulphur will be reported in units of parts per million by dry volume (ppmdv). Emission rates of chlorine and chlorine dioxide from the High Level Roof Vent will be reported in units of g/s and the concentrations released to the atmospheric will be reported in units of mg/m³.

Results of each source emissions testing event will be documented in a final report for submission to Nova Scotia Environment (NSE) for review and approval within 60 days of completing the testing.



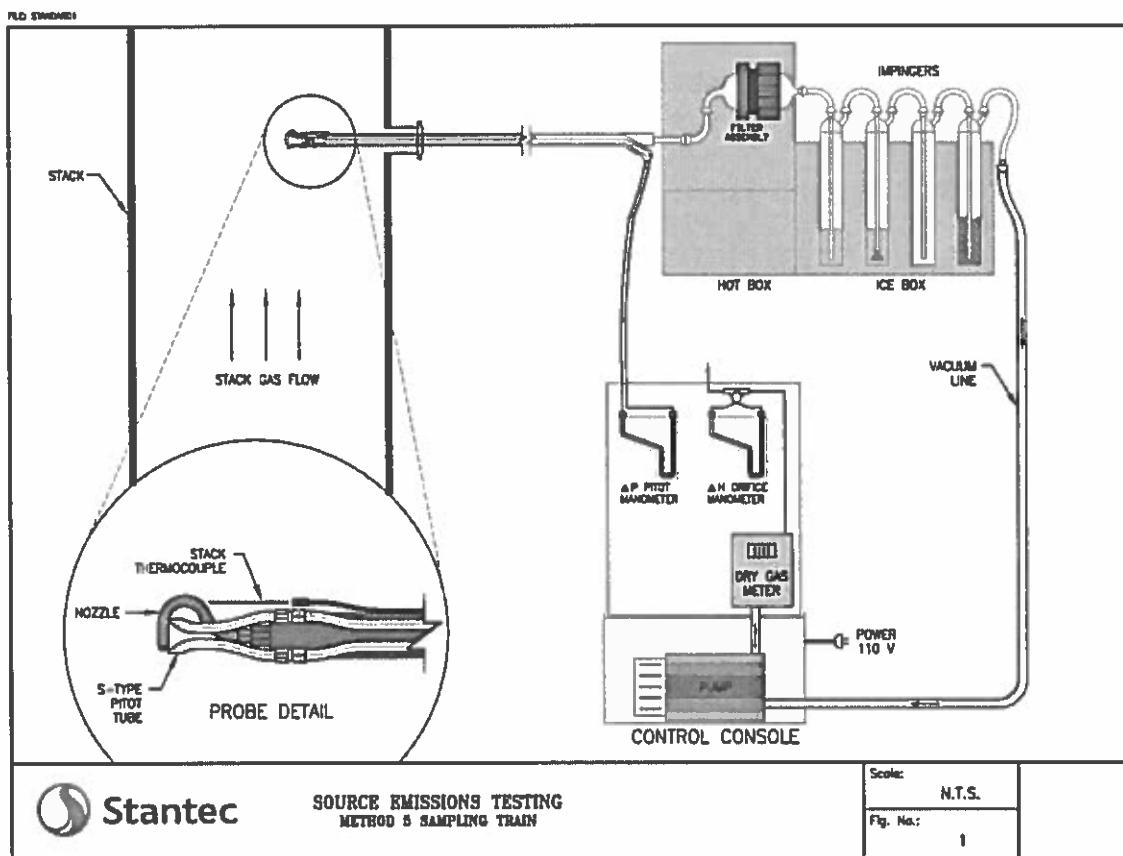
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Reference: Pre-Test Plan for Source Emissions Testing Northern Pulp,
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Sampling Locations

The number and location of sample points along each traverse were previously determined according to EPS 1/RM/8, Method A, using the exhaust stack diameter. A diagram of a typical sample location is provided in Figure 2.

Figure 1 Source Emission Testing, Method 5 Sampling Train

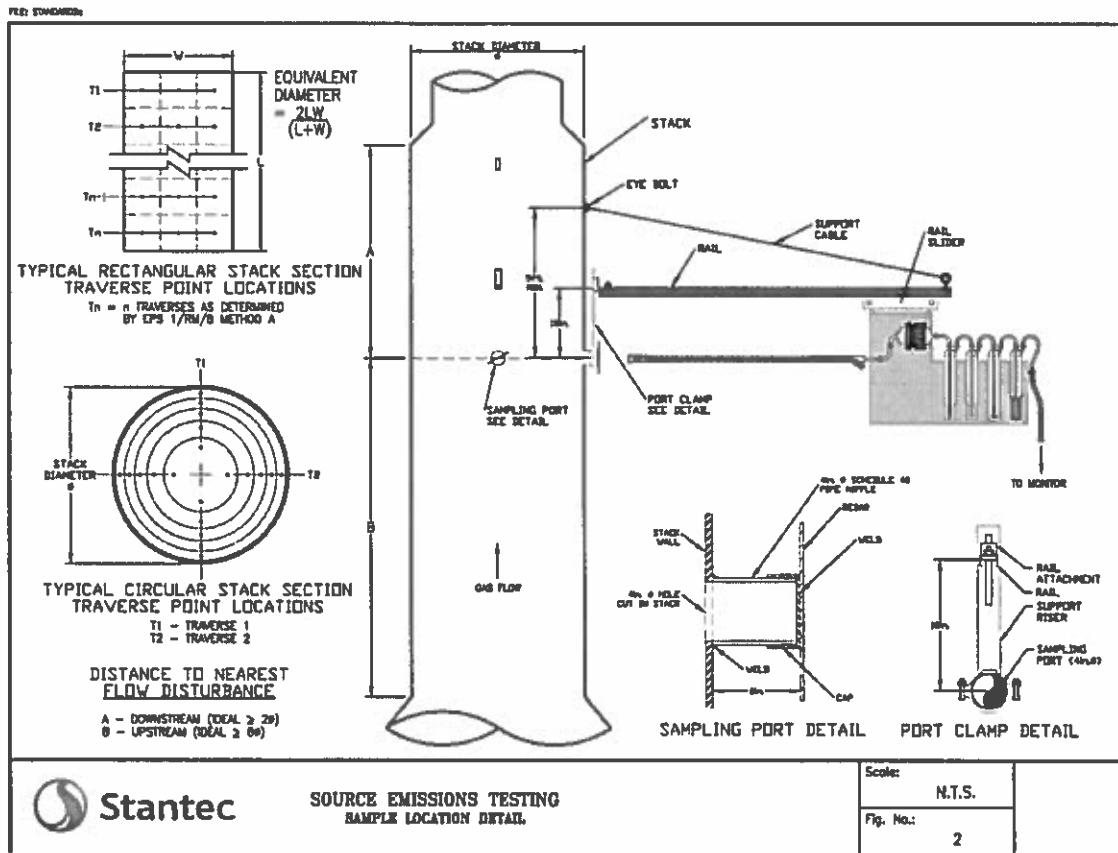




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Reference: Pre-Test Plan for Source Emissions Testing Northern Pulp,
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Figure 2 Source Emissions Testing, Sample Location Details





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A summary of the sample location details is provided in Table 2.

Table 2 Sample Location Details

Parameter	Recovery Boiler	Lime Kiln	Smelt Dissolving Tank	Power Boiler Scrubber Stack	High Level Roof Vent
Stack Height – Above Grade (m)	69	37	51	51	65
Diameter / Equivalent Diameter (m)	3.51	1.22 ³	1.22	1.93	1.83
Stack/Duct Description	Circular	Circular	Circular	Circular	Circular
Stack Orientation	Vertical	Vertical	Vertical	Vertical	Vertical
Location of Source Testing	In Stack	In Stack	In Stack	In Stack	In Stack
Number of Sample Ports	4	2	2	2	1
Sample Port Diameter (m)	0.1	0.15	0.1	0.1	0.1
Location Upstream from any Disturbance,	>2	2	>2	>2	-
Location Downstream from any Disturbance,	1.45	8	6	> 4	-
Ideal or Non Ideal Flow Characteristics at The Sample Location ¹	Not Ideal	Not Ideal ²	Not Ideal	Not Ideal	-
Total Number of Sample Points	24 (for PM)	24 (for PM) 1 (for TRS)	20 (for PM) 1 (for TRS)	24 (for PM)	1 (for TRS and Cl, ClO ₂)
Number of Sample Points per Traverse (PM sampling)	12	12	10	12	NA
Sample Time per Point for PM samples (min)	5	5	5	5	NA
Sample time per Test for PM (min)	120	120	100	120	NA
Sample time per Test for combustion gas (min)	30	30	30	30	30 (for TRS) 60 (for Cl, ClO ₂)
Sample time per Test for TRS (min)	NA	1,440	1,440	NA	1,440

¹ The exhaust gas flow characteristics at the sampling location are referred to as being "ideal" if the sample ports are located in a straight section of stack at least eight stack diameters downstream and two stack diameters upstream of any flow disturbance.

² The lime kiln sampling location has been changed from ideal to not ideal due to the cyclonic flow.

³ Field measurement – to be confirmed during the Winter/Spring Event

Quality Assurance / Quality Control

Throughout the stack testing program, rigorous quality assurance and quality control procedures will be applied to ensure the collection of reliable, representative, and reproducible emissions data. All equipment will be calibrated according to the protocols as prescribed by Environment Canada, and the US EPA. These calibrations include the following:



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Pitots:	calibrated in a wind tunnel with probe and nozzles attached;
Gas meters:	calibrated against a critical orifice set;
Thermocouples:	calibrated using a potentiometric technique;
Nozzle:	four diameter measurements made using a micrometer across the sharpened edges; and
Combustion Gas Analyser:	2 point calibrations using span gases of known concentrations.

Calibration data will be provided in the final report.

Quality control checks will be performed at several stages during the testing program to ensure the collection of representative samples and the generation of valid results. These checks are performed by test personnel throughout the program under the guidance of the source testing crew chief. The Quality Control (QC) checks include the following:

- Use of standardized checklists and field notebooks to ensure completeness, traceability, and comparability of the process information and samples collected;
- Field checking of standardized forms by a second person to ensure accuracy and completeness;
- Strict adherence to sample chain-of-custody procedures;
- Use of appropriate field blanks (e.g., filter and solution samples); and
- Leak checks of sample trains.

All internal quality assurance and quality control procedures will be strictly adhered to during all test programs to ensure the production of useful and high quality data throughout the course of the program.

Qualifications of Source Testing Team

The successful completion of this project requires the skills of competent and experienced professionals who have a strong commitment to complete the project quickly and efficiently and to produce high quality results. The source testing team we have assembled to meet the challenges of this assignment consists of highly trained professionals who bring a broad range of expertise and experience to the project. The following paragraphs provide brief descriptions of the qualifications of the source emissions testing team:

Senior Reviewer:



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Project Manager and Report Writer:



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Source Testing Team:

Schedule

Table 3 provides an overview of the proposed schedule to complete the testing, as described in the above sections, for the 2015 calendar year. Stantec will confirm actual test dates, in writing, with NSE within thirty days prior to the testing commencing.

Currently we are proposing to conduct the winter testing event within the week of March 9th.



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Table 3 Proposed Schedule

Event	Proposed Date	Scope
Winter	February-March 31 (March 9 th week)	Recovery and Power Boiler PM, gases, dissolving tank TRS
Spring	April-June 30	Recovery, Power Boiler, kiln, dissolving tank PM, gases, kiln, HLRV TRS, HLRV chlorine
Summer	July-Sept. 30	Recovery and Power Boiler PM, gases, dissolving tank TRS
Fall	October-Dec. 31	Recovery, Power Boiler, kiln, dissolving tank PM, PM _{2.5} , gases, kiln, HLRV TRS

Closing

Your timely written approval of this pre-test plan is greatly appreciated. If you have any questions, please do not hesitate to contact me directly at (902) 468-7777.

Regards,

STANTEC CONSULTING LTD.

A handwritten signature in black ink.

Gillian Hatcher
Project Manager – Environmental Services
Phone: (902) 468-7777
Fax: (902) 468-9009
@stantec.com

A handwritten signature in black ink.

Vicky Corning
Team Lead
Phone: (506) 457-3200
Fax: (506) 452-7652
@stantec.com

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**SOURCE EMISSIONS TESTING –
SUMMER ROUND 2015**

October 16, 2015

Appendix B

Calibration Data

**SOURCE EMISSIONS TESTING –
SUMMER ROUND 2015**

October 16, 2015

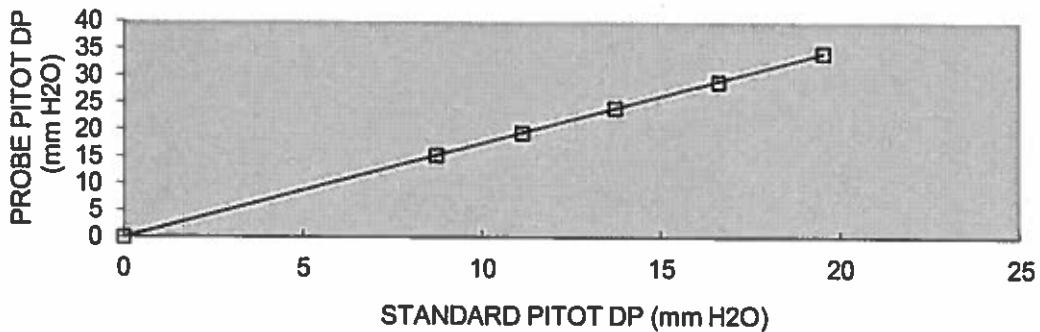
VALLEY ENVIRONMENTAL CALIBRATION SERVICES
PITOT TUBE CALIBRATION REPORT

CLIENT - Stantec
PROBE ID - 4FT M5
NOZZLE - #10- 0.3125"
DATE - February 23, 2015

FAN SPEED m/s	STANDARD PITOT (mm H ₂ O)	PROBE PITOT (mm H ₂ O)
0.00	0.00	0.00
12.1	8.70	15.30
13.6	11.10	19.40
15.1	13.70	24.00
16.6	16.60	28.90
18.0	19.50	34.30

PITOT FACTOR Cp = 0.756

PITOT - 4FT M5 NOZZLE - #10- 0.3125"
February 23, 2015



Technician: T. Ryan

Signature 

VALLEY ENVIRONMENTAL SERVICES
160 Pony Drive #1
Newmarket, Ontario L3Y 7B6
PH: (905) 830 0136
FAX: (905) 830 0137

Tunnel	VES
Std. Pitot Cp	0.999
Static	-0.25
Barometric	29.15
Temperature	65
Abs Static	29.13

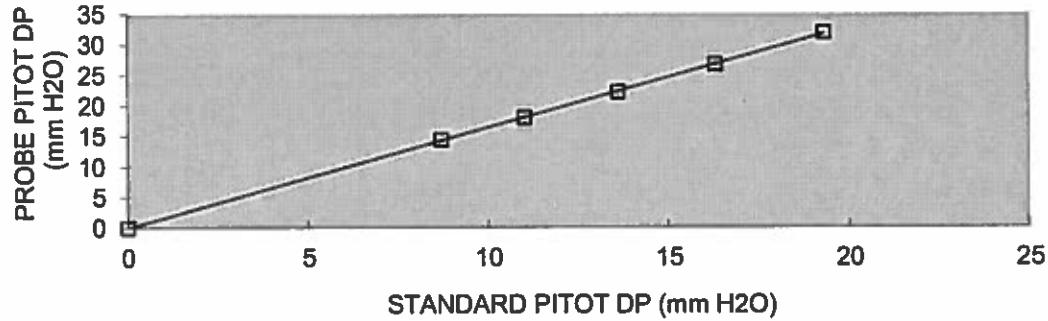
VALLEY ENVIRONMENTAL CALIBRATION SERVICES
PITOT TUBE CALIBRATION REPORT

CLIENT - Stantec
 PROBE ID - 8-2 FT M5
 NOZZLE - #6- 0.1875"
 DATE - March 3, 2015

FAN SPEED	STANDARD	PROBE
	PITOT	PITOT
m/s	(mm H ₂ O)	(mm H ₂ O)
0.00	0.00	0.00
12.1	8.70	14.40
13.6	11.00	18.00
15.1	13.60	22.20
16.5	16.30	26.70
18.0	19.30	31.90

PITOT FACTOR C_p = 0.780

PITOT - 8-2 FT M5 NOZZLE - #6- 0.1875"
 March 3, 2015

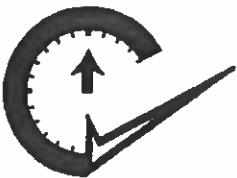


Technician: T. Ryan

Signature 

VALLEY ENVIRONMENTAL SERVICES
 160 Pony Drive #1
 Newmarket, Ontario L3Y 7B6
 PH: (905) 830 0136
 FAX: (905) 830 0137

Tunnel	VES
Std. Pitot Cp	0.999
Static	-0.25
Barometric	29.1
Temperature	65
Abs Static	29.08



CAL-CHEK CANADA

250 GOVERNOR'S ROAD - DUNDAS, ONTARIO L9H 3K3
TELEPHONE: (905) 628-4636 FAX: (905) 627-5903
email calchek@cogeco.ca

Scale / Balance Certification

Date: February 9, 2015

Certificate Number: S150165

Customer: Stantec Consulting Ltd.
845 Prospect Street
Fredericton, New Brunswick E3B 2T7

Room Temperature: 20.1°C

Calibration Location: 10 Timothy Road North Kingsclear Lab

Resolution: 0.0001g

Scale / Balance Manufacturer: Radwag

Model Number: XA220-2X

Serial Number: 336271

Capacity: 220 g

Capacity Calibrated To: 220 g

<u>ACTUAL WEIGHT</u>	<u>SCALE</u>	<u>ERROR</u>	<u>ACTUAL WEIGHT</u>	<u>SCALE</u>	<u>ERROR</u>
<u>APPLIED</u>	<u>READINGS</u>	<u>AS FOUND</u>	<u>APPLIED</u>	<u>READINGS</u>	<u>AS LEFT</u>
<u>GRAMS</u>	<u>AS FOUND</u>	<u>AS FOUND</u>	<u>GRAMS</u>	<u>AS LEFT</u>	<u>AS LEFT</u>
0.0020	0.0020	0.0000	0.0020	0.0020	0.0000
0.0050	0.0050	0.0000	0.0050	0.0050	0.0000
0.0100	0.0100	0.0000	0.0100	0.0100	0.0000
0.0500	0.0500	0.0000	0.0500	0.0500	0.0000
0.1000	0.1000	0.0000	0.1000	0.1000	0.0000
0.5000	0.5001	-0.0001	0.5000	0.5000	0.0000
1.0000	0.9998	0.0002	1.0000	0.9999	0.0001
5.0000	4.9999	0.0001	5.0000	4.9990	0.0010
10.0000	10.0001	-0.0001	10.0000	10.0000	0.0000
20.0000	20.0016	-0.0016	20.0000	20.0009	-0.0009
50.0000	50.0030	-0.0030	50.0000	50.0020	-0.0020
100.0000	99.9982	0.0018	100.0000	99.9992	0.0008
200.0000	200.0134	-0.0134	200.0000	200.0027	-0.0027
220.0000	220.0170	-0.0170	220.0000	220.0110	-0.0110

The above mentioned Scale / Balance has been checked for accuracy using the following N.I.S.T. calibrated dead weights as per the CSA method.

STANDARD CAL DATE NIST LAB #
22XE 03/10/13 681/280058-10

Obtained results are within the manufacturer's stated accuracy and/or are within +/-0.01% or 1 division whichever is greater at any point of the calibrated range.

Pass/Fail statements are based on data from measurements made, procedures utilized, professional experience and the uncertainty associated with this calibration. It is the responsibility of the user of this equipment to determine if the results identified meet specific requirements for its intended application.

Calibration Technician: Dave Newitt

Authorized Signatory: Roni Newitt

Suggested Calibration Due Date: February 2016

Due dates appearing on the certificate of calibration and label are determined by client for administrative purposes and do not imply continued conformance to specifications.

All calibrations performed at customer location unless otherwise noted.

This certificate shall not be reproduced except in full, without the written approval of Cal-Chek Canada

Pre-Test Dry Gas Meter - Control Unit Calibration

Date : 11/7/2015
 Barometric Pressure, Pb : 30.03
 Model Number : 1848
 Calibrated By : NGM
 Job #:

Orifice Manometer Setting, deltaH (in. H2O)				Dry Gas Meter Volume, Vm (cu.ft)		Temperatures (F)			Time, theta (min)
				Dry Gas Meter		Dry Gas Meter			
		Total				Outlet, to	Average, tm		
0.8					6.593		71	71	10
1.2					6.427		72	73	8
1.8					6.853		73	74	7

Calculations

Orifice Manometer Setting, deltaH (in. H2O)	Dry Gas Correction Factor, gamma (Tolerance = 0.95 - 1.05, +/-1.5% of avg)	Orifice Pressure Differential (delta H@) yielding 0.75 cfm of air at 68F and 29.92 in.Hg as in. H2O (Tolerance = +/- 0.15 in.)	Orifice Coefficient Ko
0.8	0.821	1.478	0.797
1.2	0.825	1.541	0.777
1.8	0.840	1.503	0.772
Average	0.829	1.507	0.782

Calibration Data
Enerac 500 Combustion Analyzer

Stantec Consulting Ltd.

Location: Fredericton, NB

Date: March 11, 2015

Parameter	Unit	Span Gas Concentration	Pre-Test Calibration		Post Test Check	
			Date	11-Mar-15	Date	11-Mar-15
			Personnel	NGM	Personnel	NGM
			Ambient Air Reading	Span Gas Reading	Ambient Air Reading	Span Gas Reading
CO	ppm	200 1000	0	193 1012	0	200 1001
SO ₂	ppm	200	0	178	0	200
NOX	ppm	200	0	198	0	200

Stantec Consulting Ltd.						
Steel Nozzle Calibration Data Sheet						
NozzleID	Nozzle Diameter (inches)					
Set - 2	<1>	<2>	<3>	<4>	Hi-L.O	Avg.
2-4	0.124	0.126	0.125	0.127		0.126
2-6	0.177	0.174	0.176	0.173		0.175
2-8	0.245	0.249	0.231	0.244		0.242
2-10	0.306	0.306	0.304	0.302		0.305
2-12	0.359	0.363	0.365	0.361		0.362
2-14	0.432	0.430	0.432	0.433		0.432
2-16	0.493	0.500	0.497	0.492		0.496
QA/QC	Check					
	Each Diameter Measured To Within = 0.001 Inches					
	High - Low </= 0.004					
	Prepared By: JB					
	Date: Feb 05, 2015					



**SOURCE EMISSIONS TESTING –
SUMMER ROUND 2015**

October 16, 2015

Appendix C

Field data sheets

**SOURCE EMISSIONS TESTING –
SUMMER ROUND 2015**

October 16, 2015

MOISTURE FIELD DATA SHEET

Project No.: 123456
Client: Northern Pulp
Plant: Power Boiler Outfit
Location: Pictou NS
Test: PM - 1
Date: Sep 17, 2015
Analyst: JBC/JWC

Moisture Data

See other sheet

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	896.7	705.9	190.8
2	100 mL H ₂ O	751.2	727.8	23.4
3	Blank	629.6	627.4	2.2
4	200g Silica Gel	911.2	905.3	5.9
		Total Weight Gain (g)		222.3
		Moisture Volume (mL)		

Volume H₂O Collected: 221.3 ml
X 0.048 = 10.6 ft³ H₂O (MwC)

DGM Final _____ ft³
 DGM Initial _____ ft³
 Final - Initial = _____ ft³ (Vm)

$$\text{Moisture} = \frac{V_{wc}}{(V_{wc} + V_{mc})}$$

Moisture =

oisture =

17% 10,700

SOURCE TESTING FIELD DATA SHEET

Job No.: 1214/3456
 Client: American Pipe
 Plant: Power- Boiler- Outlet
 Location: Piping AS
 Test: 2m-
 Date: 5.27.17, 2015
 Operators: JBP/JC
 Gamma: 0.329
 Delta H@: 1.507
 Pilot Ceff: 0.780
 Start: 9:10
 Finish: 11:12

Static Pressure (in.H2O): 0.18
 Port Length (in): 4
 Stack Dia. (in.): .72
 Probe Length (ft): 6 (8-2)
 Nozzle ID (in.): .26 (.175)
 Console S/N: /648

Pre-Test Leak Check: _____
 Vacuum Pressure: _____
 Post-Test Leak Check: _____
 Vacuum Pressure: _____

K: 0.54

Traverse Point	Time (min)	Stack Gas Temp., Ts (F)	Velocity Head, dp (in.H2O)	Orifice dH (in.H2O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)		Gas Meter Temp. (F)	Pump Vacuum (in.Hg)
								In	Out		
1-1	2.5	133	0.35	0.16	802.37	265	260	61	61	60	-1
	5	133	0.55	0.26	810.33	266	261	61	61	60	-1
2	7.5	133	0.60	0.28	812.24	265	260	61	63	61	-1
	10	134	0.62	0.29	813.21	266	255	60	63	61	-1
3	12.5	132	0.62	0.29	814.70	267	255	60	63	61	-1
	15	132	0.64	0.30	815.19	260	253	60	63	61	-1
4	17.5	133	0.57	0.27	816.17	260	260	60	64	62	-1
	20	133	0.57	0.27	817.13	260	260	60	64	62	-1
5	22.5	131	0.57	0.27	818.10	259	266	59	67	62	-1
	25	133	0.57	0.27	819.06	260	262	59	64	62	-1
6	27.5	133	0.57	0.27	820.05	261	257	58	65	63	-1
	30	133	0.51	0.26	821.04	260	255	57	65	63	-1
7	32.5	132	0.60	0.28	822.03	265	250	57	66	64	-1
	35	133	0.61	0.29	823.06	265	248	57	66	64	-1
8	37.5	133	0.73	0.35	824.17	266	250	57	66	64	-1
	40	134	0.76	0.36	825.29	267	250	57	66	64	-1
9	42.5	135	0.91	0.44	826.53	266	255	58	67	65	-1
	45	132	0.95	0.45	827.77	260	225	59	67	65	-1
10	47.5	135	1.10	0.53	829.09	265	232	59	67	65	-1
	50	134	1.10	0.52	830.74	266	232	59	67	65	-1
11	52.5	133	1.20	0.57	831.86*	265	225	59	67	65	-1
	55	133	1.20	0.57	833.73	266	225	59	67	65	-1
12	57.5	131	1.30	0.62	834.67	265	225	59	67	65	-1
	60	132	1.30	0.62	836.11	265	226	59	67	65	-1

SOURCE TESTING FIELD DATA SHEET

Job No.: 121413456
 Client: Alstom P-12
 Plant: Power Gen D-14
 Location: Pit 1-N
 Test: PMI-1
 Date: Sept 17, 2015
 Operators: SJS/JC
 Gamma: 0.529
 Delta H@: 1.507
 Pitot Coeff.: 0.780
 Start: 7:10
 Finish: 11:13

Static Pressure (in.H₂O): 0.15
 Port Length (in): 4
 Stack Dia. (in.): .72
 Probe Length (ft): .8
 Nozzle ID (in.): .26
 Console SN: 18415

K': 0.54

Pre-Test Leak Check: _____
 Vacuum Pressure: _____
 Post-Test Leak Check: _____
 Vacuum Pressure: _____

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dP (in.H ₂ O)	Orifice dH (in.H ₂ O)	Gas Meter Volume (cuf.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)	In	Out	Pump Vacuum (in.Hg)
Z-1	0	(31	0.95	0.45	637.37	264	244	62	68	68	66	-1
	5	130	0.95	0.46	839.62	265	245	61	68	68	66	-1
2	7.5	130	0.90	0.47	639.82	246	251	60	68	68	66	-1
	10	(31	0.90	0.43	*	266	255	60	68	68	66	-1
3	12.5	132	0.80	0.38	642.21	267	257	59	69	69	67	-1
	15	132	0.80	0.38	843.33	265	255	59	69	69	67	-1
4	17.5	133	0.75	0.36	844.45	265	248	59	69	69	67	-2
	20	133	0.75	0.36	845.59	265	247	59	69	69	67	-2
5	22.5	134	0.68	0.33	846.68	266	250	60	69	69	68	-2
	25	134	0.67	0.32	847.75	265	249	60	70	70	68	-2
6	27.5	134	0.72	0.35	848.84	266	270	60	70	68	68	-2
	30	134	0.71	0.34	849.94	267	265	59	70	70	68	-2
7	32.5	134	0.40	0.39	451.10	269	257	60	71	68	68	-2
	35	135	0.42	0.40	452.30	270	258	61	71	69	69	-2
8	37.5	135	0.92	0.44	853.54	265	225	60	71	69	69	-2
	39/40	135	0.93	0.45	854.79	265	228	60	71	69	69	-2
9	42.5	133	1.05	0.51	856.10	260	230	59	72	69	69	-3
	45	134	1.10	0.53	857.46	260	232	59	72	69	69	-3
10	47.5	134	1.10	0.55	858.84	261	225	55	72	70	70	-3
	50	133	1.10	0.53	460.20	262	227	57	72	70	70	-3
11	52.5	132	1.50	0.73	861.73	251	244	56	72	70	70	-4
	55	137	1.45	0.70	863.32	255	250	56	72	70	70	-4
12	57.5	137	1.45	0.70	864.86	262	238	56	72	70	70	-4
	60	131	1.60	0.73	866.42	263	246	56	72	70	70	-4

MOISTURE FIELD DATA SHEET

Filter
0812-35

Project No.: 121413456
 Client: Northern Pulp
 Plant: Power Boiler Outlet
 Location: Dictou NB
 Test: PM-2
 Date: Sept 17, 2015
 Analyst: WB/JWC

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	911.9	726.7	185.2
2	100 mL H ₂ O	754.0	732.5	21.5
3	Blank	628.1	625.6	2.5
4	200g Silica Gel	926.4	912.1	14.3
		Total Weight Gain (g)		223.5
		Moisture Volume (mL)		223.5

$$\text{Volume H}_2\text{O Collected: } \frac{223.5}{\text{ml}} \\ \times 0.048 = \frac{10.728}{\text{ft}^3 \text{H}_2\text{O (Vwc)}}$$

$$\begin{aligned} \text{DGM Final} &= \frac{928.99}{\text{ft}^3} \\ \text{DGM Initial} &= \frac{867.02}{\text{ft}^3} \\ \text{Final - Initial} &= \frac{61.97}{\text{ft}^3 (\text{Vmc})} \end{aligned}$$

$$\text{Moisture} = \frac{\text{Vwc}}{(\text{Vwc} + \text{Vmc})}$$

$$\text{Moisture} = \frac{10.728}{(10.728 + 61.97)}$$

$$\begin{aligned} \text{Moisture} &= \frac{0.1475693}{=} \\ &= 14.96 \% \end{aligned}$$

SOURCE TESTING FIELD DATA SHEET

Job No.: 121413456
 Client: Northern Piping
 Plant: Power - Pipeline - Outlet
 Location: Petrolia, NS
 Test: PM-1
 Date: Sept. 17, 2015
 Operators: J. B. / J. C.
 Gamma: 0.619
 Delta H@: 1.507
 Pilot Coeff.: 0.760
 Start: 1:40
 Finish: 3:40

Static Pressure (in.H2O): 0.18
 Port Length (in.): 4
 Stack Dia. (in.): 7.2
 Probe Length (ft.): 3
 Nozzle ID (in.): 2.6
 Console S/N: 1848

Pre-Test Leak Check: -18
 Vacuum Pressure: -18
 Post-Test Leak Check:
 Vacuum Pressure:

K: 0.54

Traverse Point	Time (min)	Stack Gas Temp., Ts (F)	Head, dP (in.H2O)	Office dH (in.H2O)	Gas Meter Volume (cu.ft.)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)	In	Out	Pump Vacuum (in.Hg)
1-1	0	130	1.20	0.54	867.02	253	245	68	78	-	-	-1
1	2.5	131	1.10	0.54	868.38	255	250	64	80	-8	-8	-1
2	7.5	131	1.10	0.54	869.71	261	256	65	80	79	79	-1
16	16	131	1.00	0.49	871.05	266	250	62	80	79	79	-1
3	17.5	131	0.90	0.45	872.35	266	250	62	80	79	79	-1
4	17.5	131	0.90	0.44	873.60	264	258	59	82	79	79	-1
5	22.5	131	0.90	0.44	874.84	264	258	59	82	80	80	-1
6	27.5	132	0.75	0.37	879.39	266	250	53	83	80	80	-1
7	32.5	130	0.80	0.40	880.54	265	260	53	83	80	80	-1
8	35	130	0.85	0.45	881.72	266	253	53	83	80	80	-1
9	37.5	131	0.92	0.42	882.92	266	252	54	84	80	80	-2
10	40	130	0.91	0.45	884.10	266	254	54	84	80	80	-2
11	42.5	130	0.91	0.45	885.30	266	250	57	84	81	81	-2
12	45	130	0.94	0.55	886.65	266	240	58	84	81	81	-2
13	47.5	130	0.91	0.45	887.87	265	260	59	84	81	81	-2
14	50	130	0.91	0.45	889.22	265	261	60	84	81	81	-2
15	52.5	130	1.50	0.74	890.75	265	230	53	84	81	81	-3
16	55	130	1.50	0.74	892.31	261	226	52	84	81	81	-3
17	57.5	130	1.10	0.54	893.71	260	255	51	84	81	81	-3
18	60	130	1.50	0.74	895.26	260	247	51	84	81	81	-3
19	62.5	131	1.50	0.74	896.75	264	241	52	84	81	81	-3
20	65	130	1.50	0.74	898.29	265	238	52	84	81	81	-3

SOURCE TESTING FIELD DATA SHEET

Job No.: 121413456
 Client: AJW Technologies
 Plant: Plant Bester's Outlet
 Location: P-101
 Test: P-101-2
 Date: Sept. 17, 2015
 Operators: JBB/JC
 Gamma: 0.829
 Delta H@: 1.509
 Pitot Coeff.: 1.740
 Start: 1:43
 Finish: 3:40

Static Pressure (in.H2O): 0.18
 Port Length (in): 4
 Stack Dia. (in.): 72
 Probe Length (ft): 8
 Nozzle ID (in.): 2-
 Console S/N: 1545
 Kt: 0.54

Traverse Point

Time (min) Stack Gas Temp., Ts (F)

Velocity Head, dP (in.H2O)

Orifice dH (in.H2O)

Gas Meter Volume (cu.ft)

Probe Temp. (F)

Oven Temp. (F)

Impinger Outlet Temp. (F)

Gas Meter Temp. (F)

In Out

Pump Vacuum (in.Hg)

2-1 2.5 129 1.10 0.54 494.29 265 248 54 84 81 -4
 5 129 1.10 0.54 901.05 261 262 54 84 81 -4
 2 7.5 131 1.05 0.52 * 264 252 54 84 81 -4
 10 131 1.15 0.57 903.74 263 251 54 84 81 -4
 3 12.5 132 1.10 0.54 905.12 266 264 55 84 81 -4
 15 132 1.10 0.54 906.46 264 264 55 84 81 -4
 4 17.5 132 0.95 0.47 907.76 266 264 56 84 81 -4
 20 132 0.95 0.47 909.02 266 264 56 84 81 -4
 5 22.5 131 0.85 0.42 910.24 260 260 57 84 81 -4
 25 133 0.82 0.41 911.41 262 260 58 84 81 -4
 6 27.5 133 0.81 0.40 912.66 265 258 55 84 81 -4
 30 133 0.81 0.40 913.82 265 259 54 84 81 -4
 7 32.5 133 0.84 0.47 915.03 266 257 53 84 81 -4
 35 133 0.84 0.47 916.22 264 256 55 84 81 -4
 6 37.5 133 0.85 0.42 917.43 266 261 56 83 80 -4
 40 40 133 0.77 0.38 918.57 264 254 56 83 80 -4
 9 42.5 132 0.90 0.44 919.79 264 255 57 83 80 -5
 45 45 132 0.92 0.45 921.02 264 246 57 83 80 -5
 10 47.5 132 0.95 0.47 922.28 264 250 60 83 80 -5
 50 50 132 0.92 0.45 923.54 265 249 61 83 80 -5
 11 52.5 131 1.00 0.49 * 266 250 62 84 81 -5
 55 55 131 1.05 0.62 926.12 265 251 62 84 81 -5
 12 57.5 130 1.20 0.59 927.51 265 252 63 84 81 -6
 60 60 130 1.30 0.64 928.99 264 253 64 84 81 -7

MOISTURE FIELD DATA SHEET

Project No.: 121413456
 Client: Northern Pulp
 Plant: Power Boiler Outlet
 Location: Pictou NS
 Test: PM-3
 Date: Sept 19, 2015
 Analyst: JJB/JWK

FILTER
 0812-4D

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	904.0	717.2	186.8
2	100 mL H ₂ O	744.9	723.6	21.3
3	Blank	628.7	626.1	2.6
4	200g Silica Gel	922.8	907.7	15.1
		Total Weight Gain (g)	225.8	
		Moisture Volume (mL)	225.8	

$$\text{Volume H}_2\text{O Collected: } \frac{225.8}{10,838.4} \text{ ml}$$

$$X 0.048 = \frac{10,838.4}{\text{ft}^3 \text{H}_2\text{O (Vwc)}}$$

$$\text{DGM Final } \frac{992.79}{\text{ft}^3}$$

$$\text{DGM Initial } \frac{898.29}{\text{ft}^3}$$

$$\text{Final - Initial } \frac{94.5}{\text{ft}^3 (\text{Vmc})}$$

$$\text{Moisture} = \frac{\text{Vwc}}{(\text{Vwc} + \text{Vmc})}$$

$$\text{Moisture} = \frac{10,838.4}{(10,838.4 + 94.5)}$$

$$\text{Moisture} = \frac{0.102891253}{10.29\%}$$

SOURCE TESTING FIELD DATA SHEET

Job No.: 121413456
 Client: Abbott's Boiler Co., Inc.
 Plant: Power Boiler Co., Inc.
 Location: Pm-3
 Test: Pm-3
 Date: Sept 18, 2015
 Operators: JBR/JC
 Gamma: 0.121
 Delta H@: 1.207
 Pitot Coeff: 0.780
 Start: 4:00
 Finish:

Static Pressure (in.H2O): 0.52
 Port Length (in.): 4
 Stack Dia. (in.): .72
 Probe Length (ft.): .8
 Nozzle ID (in.): .2-.6
 Console SN: 1648

Pre-Test Leak Check: ✓
 Vacuum Pressure: -148
 Post-Test Leak Check:
 Vacuum Pressure:

Rt: 0.54

Traverse Point	Time (min)	Stack Gas Temp., Ts (F)	Velocity Head, dp (in.H2O)	Orifice dH (in.H2O)	Gas Meter Volume (cu.ft.)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)		Gas Meter Temp. (F)	Pump Vacuum (in.Hg)
								In	Out		
1-1	2.5	130	1.10	0.53	929.34	225	61	66	67	-1	-1
	5	130	1.10	0.53	932.05	242	230	60	67	67	-1
2	7.5	130	1.10	0.53	933.38	263	232	57	67	67	-1
	10	130	1.10	0.53	934.70	264	236	55	67	67	-1
3	12.5	131	1.05	0.51	936.01	265	243	51	68	67	-1
	15	131	1.05	0.51	937.29	266	243	50	68	67	-1
4	17.5	130	0.87	0.42	938.51	265	250	50	69	67	-1
	20	130	0.57	0.42	266	255	50	70	67	67	-1
5	22.5	131	0.90	0.43	940.89	261	257	50	71	68	-1
	25	131	0.97	0.42	942.05	260	260	50	71	68	-1
6	27.5	130	0.80	0.39	943.24	266	259	51	72	69	-1
	30	130	0.60	0.39	944.38	260	260	52	72	69	-1
7	32.5	132	0.65	0.41	945.51	261	260	54	73	69	-1
	35	133	0.60	0.39	946.69	261	258	55	73	62	-1
8	37.5	131	0.65	0.41	947.86	266	260	55	73	70	-2
	40	131	0.85	0.41	949.05	264	261	56	77	70	-2
9	42.5	130	0.90	0.44	950.27	265	255	56	74	70	-2
	45	130	0.90	0.44	951.50	266	255	56	71	70	-2
10	47.5	132	1.10	0.53	952.70	247	57	74	71	71	-2
	50	132	1.10	0.53	953.92	263	245	57	74	72	-2
11	52.5	130	1.20	0.58	955.33	243	247	57	74	72	-2
	55	130	1.20	0.63	956.60	263	249	57	75	72	-2
12	57.5	131	1.50	0.73	958.76	265	251	57	75	72	-3
	60	130	1.60	0.73	959.95	267	250	57	75	72	-3

SOURCE TESTING FIELD DATA SHEET

Job No.: 121413456
 Client: Northern P.I.
 Plant: Power Boiler Outfit
 Location: P.E.W. A.S.
 Test: P.M.-3
 Date: Sept. 15, 2015
 Operators: J.J. / J.C.
 Gamma: 0.829
 Delta H@: 1.507
 Pitot Coeff.: 0.760
 Start: _____
 Finish: _____

Static Pressure (in.H2O): 0.52
 Port Length (in): 4
 Stack Dia. (in.): 72
 Probe Length (in.): 8
 Nozzle ID (in.): 2.6
 Console SN: 15448

Pre-Test Leak Check: _____
 Vacuum Pressure: _____
 Post-Test Leak Check: _____
 Vacuum Pressure: _____

K': 0.54

Pre-Test Leak Check: _____
 Vacuum Pressure: _____
 Post-Test Leak Check: _____
 Vacuum Pressure: _____

Traverse Point	Time (min)	Stack Gas Temp., Ts (F)	Velocity Head, dp (in.H2O)	Orifice dH (in.H2O)	Gas Meter Volume (cu.ft.)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in.Hg)
									In	Out	
2-1	0	130	0.05	0.51	959.95	261	262	59	77	74	-5
	5	130	1.05	0.51	961.51	264	264	39	77	74	-4
2	7.5	131	1.05	0.51	962.86	266	267	58	77	74	-4
	10	132	1.10	0.54	963.60	266	265	56	77	74	-5
3	12.5	132	1.10	0.54	966.99	265	259	51	78	75	-5
	15	132	1.10	0.54	968.39	266	260	50	78	75	-5
4	17.5	132	0.97	0.47	969.72	261	263	47	78	75	-5
	20	132	1.00	0.49	971.04	261	264	47	78	75	-5
5	22.5	131	0.90	0.44	972.32	262	262	46	78	76	-3
	25	131	0.90	0.44	973.58	261	262	45	78	76	-3
6	27.5	132	0.85	0.42	974.83	260	261	44	78	76	-3
	30	133	0.65	0.12	976.08	260	259	44	78	76	-3
7	32.5	133	0.90	0.14	977.36	261	261	45	78	76	-4
	35	135	0.90	0.44	978.62	261	261	45	78	76	-4
8	37.5	133	0.90	0.14	979.88	243	253	45	78	77	-1
	40	133	0.90	0.44	981.14	244	255	45	78	77	-1
9	42.5	131	1.05	0.51	982.47	264	250	47	79	77	-4
	45	131	1.00	0.49	983.81	264	251	48	79	77	-4
10	47.5	134	1.10	0.54	985.20	265	256	48	79	77	-5
	50	134	1.10	0.54	986.57	265	258	49	79	77	-5
11	52.5	131	1.10	0.54	987.96	266	260	49	79	77	-5
	55	131	1.15	0.56	989.34	261	260	49	79	77	-5
12	57.5	131	1.40	0.69	990.45	265	252	50	79	77	-6
	60	131	1.40	0.69	992.79	266	251	50	79	77	-6

MOISTURE FIELD DATA SHEET

0812-16

Project No.: 121413456

Client: Northern Pulp

Plant: Recovery Outlet

Location: Pictou, NS

Test: PM-1

Date: Sept. 15, 2015

Analyst: JWB

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	973.7	722.8	250.9
2	100 mL H ₂ O	1005.8	734.8	271.0
3	Blank	654.1	625.4	228.7
4	200g Silica Gel	906.4	854.1	52.3
		Total Weight Gain (g)		802.9
		Moisture Volume (mL)		802.9

$$\text{Volume H}_2\text{O Collected: } \frac{802.9}{\text{ml}} \\ X 0.048 = \frac{38.54}{\text{ft}^3 \text{H}_2\text{O (Vwc)}}$$

$$\begin{aligned} \text{DGM Final} &= \frac{491.29}{\text{ft}^3} \\ \text{DGM Initial} &= \frac{386.00}{\text{ft}^3} \\ \text{Final - Initial} &= \frac{105.29}{\text{ft}^3 (\text{Vmc})} \end{aligned}$$

$$\text{Moisture} = \frac{\text{Vwc}}{(\text{Vwc} + \text{Vmc})}$$

$$\text{Moisture} = \frac{38.54}{(38.54 + 105.29)}$$

$$\text{Moisture} = \underline{0.268 = 26.8\%}$$

Job No.: 121413156
 Client: Northern P.I.C.
 Plant: Recovery Outfall
 Location: Pitts, NS
 Test: PMA-1
 Date: Sept. 15/2013
 Operators: J.S./J.C.
 Gamma: 0.919
 Delta H@: 1.507
 Pitot Coeff.: 0.756
 Start: 1/15
 Finish:

SOURCE TESTING FIELD DATA SHEET

Static Pressure (in.H2O): 1.10
 Port Length (in): 4
 Stack Dia. (in): 3.8
 Probe Length (ft): 4
 Nozzle ID (in.): 2.10 (0.30)
 Console SN: 1848

Pre-Test Leak Check: 0
 Vacuum Pressure: -14'
 Post-Test Leak Check:
 Vacuum Pressure:

K: 3.69

T_s DP DH

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dp (in.H2O)	Orifice dH (in.H2O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F) (In) (Out)	Pump Vacuum (in.Hg)
0	0	154	0.51	1.62	388.68	225	260	65	69 69	-1
1	2.5	154	0.51	1.62	390.93	260	270	63	70 69	-2
2	7.5	154	0.51	1.62	393.15	265	290	61	69 69	-2
10	10	154	0.51	1.62	395.34	266	257	60	69 69	-2
3	12.5	155	0.50	1.67	397.53	265	268	61	70 69	-2
4	15	155	0.50	1.59	399.70	264	258	65	71 69	-2
5	17.5	155	0.50	1.59	401.86	265	252	62	71 69	-2
6	20	155	0.50	1.59	404.00	266	251	70	71 69	-2
7	22.5	155	0.49	1.56	406.13	265	263	78	72 70	-2
8	25	155	0.49	1.56	408.25	267	267	76	72 70	-2
9	27.5	155	0.50	1.59	410.39	265	261	80	73 69	-2
10	30	156	0.50	1.59	412.55	266	264	80	73 70	-2
11	32.5	155	0.50	1.59	414.69	265	250	75	74 70	-2
12	35	155	0.50	1.59	416.83	261	252	71	74 71	-2
13	37.5	156	0.50	1.60	419.00	265	261	70	75 70	-2
14	40	156	0.50	1.60	421.17	265	262	70	75 70	-2
15	42.5	154	0.50	1.60	423.36	266	257	71	76 70	-2
16	45	154	0.50	1.60	425.56	265	247	71	76 70	-2
17	47.5	154	0.50	1.60	427.77	265	264	71	76 71	-3
18	50	154	0.50	1.60	429.95	267	263	72	76 71	-3
19	52.5	155	0.50	1.60	432.14	264	255	74	76 72	-3
20	55	155	0.50	1.60	434.30	266	256	74	76 72	-3
21	57.5	155	0.51	1.63	436.48	266	261	74	78 72	-3
22	60	155	0.51	1.63	438.67	266	262	74	79 72	-3

SOURCE TESTING FIELD DATA SHEET

Job No.: 121413466

Client: Northern IP
 Plant: Recovery Outlet
 Location: Pictou, NS
 Test: P-1
 Date: Sept 15/2011
 Operators: J. Ross / JC
 Gamma: 0.819
 Delta H@: 1.567
 Pitot Coeff.: 0.7585
 Start:
 Finish: 13:30

Static Pressure (in.H2O): 1.10
 Port Length (in): 1
 Stack Dia. (in.): 138
 Probe Length (ft): 9
 Nozzle ID (in.): 2-10 (a. 30.5)
 Console S/N: 1848

Pre-Test Leak Check: _____
 Vacuum Pressure: _____
 Post-Test Leak Check: 0
 Vacuum Pressure: -18

K: 3.69

Traverse Point	Time (min)	Stack Gas Temp., Ts (F)	Velocity Head, dp (in.H2O)	Orifice dH (in.H2O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	T _m		Pitot Filter	Gas Meter Temp. (F)	Pump Vacuum (in.Hg)
									In	Out			
0													
1	2.5	155	0.50	1.60	4140.84	266	260	74	78	72	-2	-2	-2
5	153	0.50	1.60	443.04	267	261	74	78	72	-2	-2	-2	-2
7	7.5	153	0.50	1.60	445.22	265	259	75	78	72	-3	-3	-3
10	153	0.50	1.60	447.41	262	260	75	78	72	-2	-2	-2	-2
12.5	155	0.50	1.60	449.60	266	263	75	78	73	-3	-3	-3	-3
15	155	0.50	1.60	451.89	261	260	75	78	73	-3	-3	-3	-3
17.5	154	0.50	1.60	454.09	263	259	74	79	73	-3	-3	-3	-3
20	154	0.50	1.60	456.26	264	261	73	79	73	-3	-3	-3	-3
5	22.5	155	0.50	161	458.33	263	238	73	76	73	-3	-3	-3
7.5	154	0.50	1.61	460.58	264	242	71	78	73	-3	-3	-3	-3
6	21.5	154	0.50	1.61	462.65	264	254	71	78	73	-3	-3	-3
30	155	0.50	1.61	464.89	263	258	71	78	73	-3	-3	-3	-3
7	32.5	155	0.50	1.61	466.88	262	265	71	78	73	-3	-3	-3
35	155	0.50	1.61	469.29	263	253	72	79	73	-3	-3	-3	-3
8	37.5	155	0.50	1.61	471.49	263	258	72	79	73	-3	-3	-3
40	155	0.50	1.61	473.81	264	243	73	79	74	-4	-4	-4	-4
9	42.5	156	0.50	1.61	475.89	265	250	74	80	74	-4	-4	-4
45	156	0.50	1.61	477.60	265	254	74	80	74	-4	-4	-4	-4
16	47.5	156	0.50	1.61	480.14	264	248	75	80	74	-4	-4	-4
50	155	0.50	1.61	482.34	265	257	78	81	75	-4	-4	-4	-4
52.5	156	0.50	1.61	484.58	264	242	80	81	75	-4	-4	-4	-4
55	155	0.50	1.61	486.89	265	262	80	81	75	-4	-4	-4	-4
57.5	154	0.50	1.62	489.00	264	260	80	82	75	-4	-4	-4	-4
60	155	0.50	1.62	491.29	265	253	80	82	75	-4	-4	-4	-4

2/2

COMBUSTION GAS ANALYSIS CONCENTRATION FIELD SHEET

Sampling Methodology: Environment Canada EPS 1/RM/15



Stantec

Project No.: 121413456
Client: Northern Pipe
Plant: Recovery Outlet
Location: Pictou, NS

Fuel Type: Black Liquor

Time Start: 12:00

Personnel: JJR

MOISTURE FIELD DATA SHEET

FILTER #

0812-11

Project No.: 121413456

Client: Northam Pulp

Plant: Recovery Outlet

Location: Picton NS

Test: PM-3

Date: Sept. 16, 2015

Analyst: JLB

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	487.4	723.8	263.6
2	100 mL H ₂ O	1023.7	731.0	292.7
3	Blank	864.7	625.1	239.6
4	200g Silica Gel	923.9	892.2	31.7
		Total Weight Gain (g)		827.6
		Moisture Volume (mL)		827.6

$$\text{Volume H}_2\text{O Collected: } \frac{827.6}{39.72} \text{ ml}$$

$$X 0.048 = \frac{39.72}{\text{ft}^3 \text{H}_2\text{O (Vwc)}}$$

$$\begin{aligned} \text{DGM Final} &= \frac{701.39}{\text{ft}^3} \\ \text{DGM Initial} &= \frac{596.17}{\text{ft}^3} \\ \text{Final - Initial} &= \frac{105.22}{\text{ft}^3 (\text{Vmc})} \end{aligned}$$

$$\text{Moisture} = \frac{\text{Vwc}}{(\text{Vwc} + \text{Vmc})}$$

$$\text{Moisture} = \frac{39.72}{(105.22 + 39.72)}$$

$$\text{Moisture} = \underline{0.274 = 27.4\%}$$

SOURCE TESTING FIELD DATA SHEET

Job No.: 121413456

Client: No Name 217
 Plant: Electrolyt Outlets
 Location: Pittsburgh, PA
 Test: PM-3
 Date: Sept. 16, 2015
 Operators: JJB/JJC
 Gamma: 0.89
 Delta H@: 1.507
 Pilot Coeff.: 0.156
 Start: 9:40
 Finish:

Static Pressure (in.H2O): 1.10
 Port Length (in): 4
 Stack Dia. (in): 1.38"
 Probe Length (ft): 4
 Nozzle ID (in.): 2-16 (0.305)
 Console S/N: 18448

Pre-Test Leak Check: _____
 Vacuum Pressure: _____
 Post-Test Leak Check: _____
 Vacuum Pressure: _____

K: 3.62

Traverse Point	Time (min)	Stack Gas Temp., Ts (F)	Velocity Head, dp (in.H2O)	Orifice dH (in.H2O)	Gas Meter Volume (cu.ft)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in.Hg)
									In	Out	
0					596.17						
1	2.5	155	0.50	1.58	598.32	225	255	61	66	65	-35
2	5	155	0.50	1.58	600.51	235	255	60	66	65	-35
3	7.5	156	0.50	1.58	602.69	265	258	48	67	66	-37
4	10	156	0.50	1.58	604.86	265	260	47	67	66	-37
5	12.5	156	0.48	1.51	607.01	265	260	48	69	66	-37
6	15	156	0.48	1.51	609.14	266	261	48	69	66	-37
7	17.5	156	0.48	1.51	611.26	265	258	49	70	67	-37
8	20	156	0.49	1.55	613.36	265	260	49	70	67	-37
9	22.5	156	0.49	1.55	615.52	264	245	51	72	67	-37
10	25	156	0.49	1.55	617.68	266	247	52	72	67	-37
11	27.5	155	0.49	1.56	619.77	265	263	51	74	68	-37
12	30	155	0.50	1.58	621.97	266	262	51	74	68	-37
13	32.5	154	0.50	1.66	624.17	265	259	52	75	69	-41
14	35	154	0.50	1.66	626.35	262	260	52	75	69	-41
15	37.5	153	0.50	1.60	628.55	266	263	55	77	70	-41
16	40	153	0.50	1.60	630.75	266	264	55	77	71	-41
17	42.5	153	0.50	1.60	632.94	265	259	57	79	71	-41
18	45	153	0.50	1.60	635.18	266	260	58	79	72	-41
19	47.5	151	0.51	1.64	637.39	265	261	60	80	72	-41
20	50	151	0.51	1.64	639.60	265	262	60	80.	73	-41
21	52.5	153	0.51	1.64	641.82	265	261	61	81	73	-41
22	55	153	0.51	1.64	644.03	266	262	61	81	73	-41
23	57.5	153	0.51	1.64	646.22	266	260	63	81	73	-41
24	60	153	0.51	1.64	648.42	265	261	64	81	74	-41

SOURCE TESTING FIELD DATA SHEET

Job No.: 121413456
 Client: ~~Alpha Beta P.I.~~
 Plant: 121413456 RECOVERY UNIT
 Location: 121413456
 Test: PM-5
 Date: Sept 16, 2015
 Operators: J.B./J.C.
 Gamma: 0.899
 Delta H@: 1.307
 Pitot Coeff.: 0.756
 Start: 10:40
 Finish: 10:40

Static Pressure (in.H2O): 1.10
 Port Length (in): 4
 Stack Dia. (in.): 13.8
 Probe Length (ft.): 4
 Nozzle ID (in.): 2-10^{60.505}>
 Console SN: 1843
 Pre-Test Leak Check: _____
 Vacuum Pressure: _____
 Post-Test Leak Check: _____
 Vacuum Pressure: _____
 Kt: 3.69

Traverse Point	Time (min)	Stack Gas Temp., T _s (F)	Velocity Head, dP (in.H2O)	Orifice dH (in.H2O)	Gas Meter Volume (cuff)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)	Gas Meter Temp. (F)		Pump Vacuum (in.Hg)
									In	Out	
1	0	155	0.51	1.64	648.42	261	255	255	C.S.	81	-4
	5	154	0.51	1.64	652.66	266	254	255	S.I.	75	-4
2	7.5	156	0.51	1.64	655.04	265	249	249	S.I.	75	-4
	10	156	0.51	1.64	655.728	266	263	258	S.I.	75	-4
3	12.5	154	0.51	1.64	659.18	265	249	249	S.I.	75	-4
	15	155	0.51	1.65	661.67	265	252	254	S.I.	75	-4
4	17.5	155	0.51	1.65	663.87	265	257	253	S.I.	76	-4
	20	155	0.51	1.65	666.25	266	265	265	S.I.	76	-4
5	22.5	156	0.51	1.65	668.26	265	260	260	S.I.	76	-4
	25	157	0.51	1.64	670.38	265	261	261	S.I.	76	-4
6	27.5	156	0.51	1.65	672.55	262	268	263	S.I.	76	-4
	30	156	0.51	1.65	674.48	265	253	254	S.I.	76	-4
7	32.5	157	0.51	1.64	676.83	265	261	265	S.I.	76	-5
	35	154	0.51	1.65	679.10	265	256	256	S.I.	76	-5
8	37.5	155	0.51	1.65	681.31	265	260	267	S.I.	77	-5
	40	155	0.51	1.65	683.53	265	257	258	S.I.	77	-5
9	42.5	155	0.51	1.65	685.75	265	255	259	S.I.	77	-5
	45	154	0.51	1.65	688.01	266	261	261	S.I.	77	-5
10	47.5	154	0.51	1.65	690.25	264	251	251	S.I.	77	-5
	50	154	0.51	1.65	692.49	265	254	252	S.I.	77	-5
11	52.5	154	0.51	1.66	694.71	264	246	246	S.I.	77	-5
	55	155	0.51	1.65	696.95	265	250	250	S.I.	77	-5
12	57.5	154	0.51	1.66	699.30	265	247	251	S.I.	77	-5
	60	154	0.51	1.65	701.39	265	247	251	S.I.	77	-5

COMBUSTION GAS ANALYSIS CONCENTRATION FIELD SHEET

Sampling Methodology: Environment Canada EPS 1/RM/15



Stantec

Project No.:	121413456
Client:	<u>Northern Pulp</u>
Plant:	<u>Recovery Outfit</u>
Location:	<u>Pictou, NS</u>
Test No.:	3
Date:	Sept. 11, 2015

Fuel Type: _____

Time Start: 9:00

Time Finish: 9:30

Personnel: JJB

MOISTURE FIELD DATA SHEET

FILTER #: _____

0812 - 12

Project No.: 121413456
 Client: Northern Pulp
 Plant: Recovery Outlet
 Location: PICTON NS
 Test: PM-4
 Date: Sept 16, 2015
 Analyst: JJB

Moisture Data

Impinger No.	Impinger Contents	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H ₂ O	1001.2	728.5	272.7
2	100 mL H ₂ O	1018.6	734.4	284.2
3	Blank	848.0	625.6	222.4
4	200g Silica Gel	941.7	915.4	26.3
Total Weight Gain (g)				805.6
Moisture Volume (mL)				805.6

$$\text{Volume H}_2\text{O Collected: } 805.6 \text{ ml}$$

$$X 0.048 = 38.6688 \text{ ft}^3 \text{ H}_2\text{O (Vwc)}$$

$$\begin{aligned} \text{DGM Final} &= 808.97 \text{ ft}^3 \\ \text{DGM Initial} &= 701.45 \text{ ft}^3 \\ \text{Final - Initial} &= 107.02 \text{ ft}^3 (\text{VmC}) \end{aligned}$$

$$\text{Moisture} = \frac{\text{Vwc}}{(\text{Vwc} + \text{VmC})}$$

$$\text{Moisture} = \frac{1 \cdot 38.6688}{(38.6688 + 107.02)} = 145.60\%$$

$$\text{Moisture} = \frac{0.265421}{26.54} = 26.54\%$$

Job No.: 121413456
 Client: Northern Pump
 Plant: Reservoirs Outlets
 Location: Peter, NJ
 Test: PM-4
 Date: Sept. 16, 2015
 Operators: JBR/JC
 Gamma: 0.889
 Delta H@: 1.507
 Pitot Coeff.: 0.756
 Start: 12:30
 Finish:

SOURCE TESTING FIELD DATA SHEET

Static Pressure (in.H2O): 1.14
 Port Length (in): 1
 Stack Dia. (in): 13.8
 Probe Length (ft): 4
 Nozzle ID (in.): 2-10 (0.256)
 Console S/N: 1448
 Pre-Test Leak Check: -18
 Vacuum Pressure: -18
 Post-Test Leak Check: _____
 Vacuum Pressure: _____

K': 359

Traverse Point	Time (min)	Stack Gas Temp., Ts (F)	Velocity Head, dp (in.H2O)	Orifice dH (in.H2O)	Gas Meter Volume (cu.ft.)	Probe Temp. (F)	Oven Temp. (F)	Impinger Outlet Temp. (F)		Gas Meter Temp. (F)	Pump Vacuum (in.Hg)
								In	Out		
1	0	155	0.50	1.61	701.95	255	250	63	74	75	-4
2	2.5	155	0.50	1.61	704.15	260	252	62	75	75	-4
2	7.5	155	0.50	1.61	706.38	263	259	51	77	74	-5
10	155	0.51	1.64	708.62	264	260	49	77	75	-5	-5
3	12.5	153	0.51	1.64	710.85	265	264	48	78	74	-5
3	15	154	0.51	1.64	713.04	265	265	47	78	74	-5
4	17.5	152	0.51	1.64	715.30	265	265	47	78	74	-5
4	20	152	0.50	1.61	717.53	261	268	47	77	74	-5
5	22.5	155	0.50	1.61	719.76	266	259	47	77	74	-5
5	25	155	0.50	1.61	721.99	266	266	47	77	73	-4
6	27.5	155	0.50	1.61	724.22	266	266	47	78	73	-4
6	30	155	0.50	1.61	726.42	265	256	49	78	73	-4
7	32.5	155	0.50	1.61	728.63	264	258	49	78	73	-4
7	35	155	0.50	1.61	730.84	265	258	51	79	74	-4
8	37.5	155	0.50	1.61	733.03	265	257	52	79	74	-4
9	40	155	0.50	1.61	735.21	266	257	52	80	74	-4
9	42.5	154	0.50	1.61	737.42	266	258	52	80	74	-4
9	45	154	0.50	1.61	739.65	265	255	53	80	74	-4
10	47.5	155	0.50	1.61	741.87	266	253	54	80	74	-4
10	50	155	0.50	1.61	744.10	261	255	53	82	75	-4
11	52.5	155	0.50	1.61	746.33	262	257	54	82	76	-4
11	55	155	0.50	1.61	748.55	265	257	54	84	75	-4
12	57.5	155	0.50	1.61	750.78	266	258	54	84	76	-4
12	60	155	0.50	1.61	753.02	265	258	55	84	77	-4
					755.27	263	256	56	84	77	-4

SOURCE TESTING FIELD DATA SHEET

Job No.: 121413456

Client: Northern Piping
 Plant: Desaverk Distillt
 Location: P-4-4
 Test: Sept. 16, 2015
 Date:
 Operators: 113 A/C
 Gamma: 0.829
 Delta H@: 1.607
 Pilot Coeff: 0.736
 Start: ~12:30 PM
 Finish: ~2:33 PM

Pre-Test Leak Check: _____
 Vacuum Pressure: _____
 Post-Test Leak Check: _____
 Vacuum Pressure: _____

K: 3.52

Static Pressure (in.H2O): -4.16
 Port Length (in): 4
 Stack Dia. (in): 13.5
 Probe Length (ft): 4
 Nozzle ID (in.): 2-10 (.3 ss)
 Console SN: 1846

Traverse Point

Time (min)

Stack Gas Temp., Ts (F)

Velocity Head, dP (in.H2O)

Orifice dH (in.H2O)

Gas Meter Volume (cubic ft)

Probe Temp. (F)

Oven Temp. (F)

Impinger Outlet Temp. (F)

Gas Meter Temp. (F)

Pump Vacuum (in.Hg)

In Out

0

1 2.5 155 0.50 1.62 757.54 266 255 5.8 7.8 -5

5 155 0.50 1.62 752.87 265 259 5.9 8.3 -5

2 7.5 165 0.49 1.59 762.05 266 261 4.9 8.2 -5

10 155 0.49 1.59 764.29 266 262 4.9 8.2 -5

3 12.5 155 0.49 1.59 766.55 265 259 4.7 8.2 7.9 -5

15 154 0.49 1.59 768.78 265 261 4.6 8.1 7.7 -5

17.5 155 0.49 1.59 771.01 265 264 4.6 8.3 7.7 -5

20 154 0.49 1.59 773.25 265 257 4.7 8.3 7.7 -5

5 22.5 153 0.49 1.59 775.44 265 261 4.7 8.2 7.7 -5

25 154 0.49 1.59 777.66 265 263 4.9 8.2 7.8 -5

6 27.5 154 0.49 1.59 779.91 265 259 4.9 8.3 7.7 -5

30 155 0.49 1.59 781.16 * 265 266 5.0 8.3 7.7 -5

7 32.5 154 0.49 1.59 784.39 265 258 5.1 8.2 7.7 -5

35 154 0.49 1.59 786.61 265 259 5.1 8.2 7.7 -5

8 37.5 154 0.49 1.59 788.88 265 262 5.1 8.2 7.7 -5

40 154 0.49 1.59 791.15 265 257 5.2 8.2 7.7 -5

47.5 154 0.49 1.59 793.36 265 262 5.2 8.2 7.7 -5

45 153 0.49 1.59 795.79 265 262 5.2 8.2 7.7 -5

10 47.5 153 0.49 1.59 797.84 265 260 5.3 8.2 7.7 -5

50 153 0.49 1.59 800.06 265 258 5.4 8.2 7.7 -5

52.5 153 0.49 1.59 802.29 265 259 5.5 8.1 7.6 -5

55 154 0.49 1.59 804.54 264 250 5.7 8.2 7.6 -6

57.5 154 0.49 1.59 806.73 265 261 5.8 8.1 7.6 -6

60 154 0.49 1.59 808.97 265 252 6.0 8.0 7.6 -6

COMBUSTION GAS ANALYSIS CONCENTRATION FIELD SHEET

Sampling Methodology: Environment Canada EPS 1/RM/15

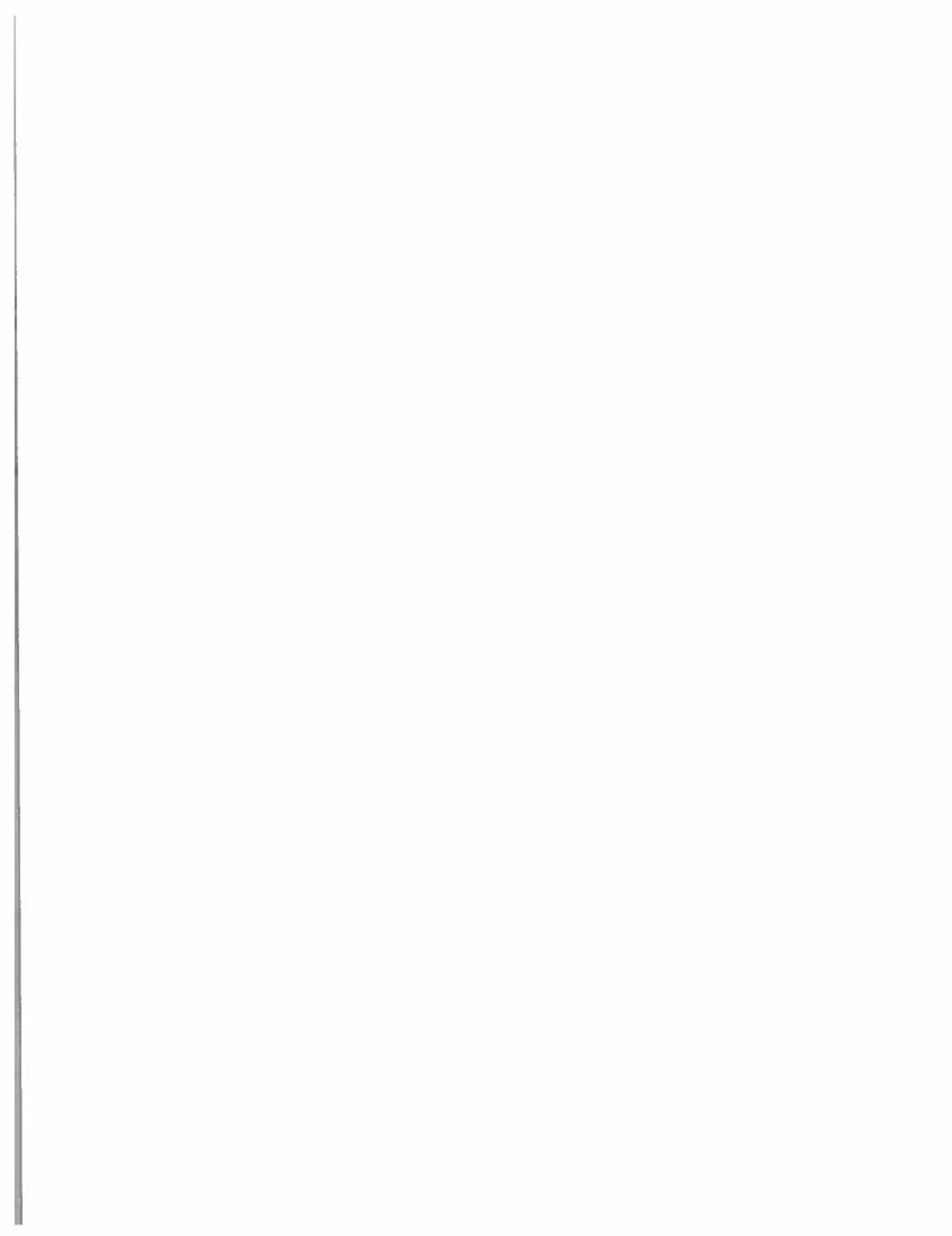


Stantec

Project No.: 121413456
Client: Northern Pulp
Plant: Recovery Outlet
Location: Pictou, NS

Test No.: 9
Date: _____

Fuel Type: _____



**SOURCE EMISSIONS TESTING –
SUMMER ROUND 2015**

October 16, 2015

Appendix D

Calculations

**SOURCE EMISSIONS TESTING –
SUMMER ROUND 2015**

October 16, 2015

Source Testing Data Checklist

Project Number:
Spreadsheet Checker:
Date Checked:
Data Entered By:

		Yes or No	Notes:
Data Entry			
1) Are the facility and client names consistent across the trials?	y	y	
2) Have the stack height, stack diameter, fuel burned, and operating conditions been entered on the Data Entry tab?	y	y	
3) If the sheet has been modified to include more/less points or traverses have the average and summation formulas been adjusted (Calc sheets)?	na	na	
4) Have any changes to the testing protocol been entered in the sheet (as appropriate)?	na	na	
5) For clients with multiple tests (e.g. PIM and Formaldehyde)	na	na	
A) Are the data copied over correctly (if appropriate)?			
B) Are the facility and client names consistent between all tests?			
C) If appropriate, does the data calculated in each trial agree between the different tests (velocity, volume, molecular weights, etc.)?	na	na	
Analysis			
1) Have the results been corrected to the reference conditions stated in the Pre-Test Plan/Approval to Operate?	y	y	
2) If applicable, are the results on the Summary sheet corrected to a particular O ₂ or CO ₂ concentration?	y	y	
3) Have the isokineticity values been scanned for low (< 90%) and high (> 120%) numbers?	y	y	
4) Looking at the Data Entry, Calculations, and Summary sheets, are the results consistent across all trials?	y	y	
5) Has a scan of the raw data (including gas data) been performed to find any obvious types?	y	y	
6) If source has been tested previously, are the results similar?	n	y	
7) For PM tests, are there any outliers on the Recovery sheet (in particular, the Probe Wash)?	n	y	
8) Have the calibration data been checked (Cp, nozzle ID, gamma)?	y	y	
9) If appropriate, are the SO ₂ emission reasonable (based on fuel type)?	y	y	
10) If relevant, do the Chain of Custody forms agree with what was analyzed? Do the lab results make sense?	y	y	
Final Product			
1) Are the labels on the velocity charts meaningful/correct (West Traverse vs. Traverse 1)?	y	y	
2) Has the axis been formatted (min and max), so the data is easy to see?	y	y	
3) Have the calibration documents been saved?	y	y	
4) Have the fieldsheets been scanned and saved?	y	y	

Raw Data for: Northern Pulp Power Boiler PM

Test #1

Client: Northern Pulp

Job Number: 121413455

Plant: Power Boiler

Location: Picton, NS

Test: PM-1

Date: 17-Sep-15

Personnel: JJD/C

Test Start: 9:10 AM
Test End: 11:10 AM

Parameters

Barometric Pressure, psbar [in. Hg] Stack Static Pressure, psstatic [in. H₂O]) Ambient Temp, (°F) H₂O Volume Collected, V_w [mL]

H₂O Volume Collected from Probe Wash [mL] Total Sampling Points, N Sampling Time per Point, (min) Readings Taken Every — mins Regulatory Agency

Traverse Point	Time [min]	Stack Gas Temp, T _s [°F]	S-type Pitot data P [in. H ₂ O])	Orifice delta H [in. H ₂ O])	Gas Meter Volume [ft ³ ft]	Gas Meter Temp Inlet [°F]	Outlet [°F]
Traverse 1	1	2.5	133	0.35	809.370	61	60
	5	133	0.35	0.25	810.150	61	60
	7.5	133	0.36	0.28	811.250	63	61
	10	134	0.62	0.29	812.240	63	61
	12.5	132	0.62	0.29	813.210	63	61
	15	132	0.64	0.30	814.200	63	61
	17.5	133	0.57	0.27	815.190	63	61
	20	133	0.57	0.27	816.170	64	62
	22.5	131	0.57	0.27	817.150	64	62
	25	133	0.57	0.27	818.100	64	62
	27.5	133	0.57	0.27	819.060	64	62
	30	133	0.59	0.26	820.050	63	63
	32.5	132	0.60	0.28	821.040	63	63
	35	133	0.61	0.29	822.030	64	64
	37.5	133	0.73	0.33	823.060	66	64
	40	134	0.76	0.36	824.170	66	64
	42.5	135	0.91	0.44	825.290	66	64
	45	132	0.93	0.45	826.530	67	65
	47.5	133	1.10	0.53	827.790	67	65
	50	134	1.10	0.53	829.050	67	65
	52.5	133	1.20	0.57	830.440	67	65
	55	133	1.16	0.57	831.230	67	65
	57.5	131	1.38	0.62	831.570	67	65
	60	132	1.36	0.62	832.110	67	65

Traverse 2	1	62.5	121	0.95	834.110	68	66
	65	130	0.95	0.45	837.170	68	66
	67.5	130	0.96	0.43	838.680	68	66
	70	131	0.90	0.43	838.820	68	66
	72.5	132	0.80	0.38	840.110	68	66
	75	132	0.80	0.38	841.210	69	67
	77.5	133	0.82	0.39	841.350	69	67
	80	133	0.73	0.26	844.450	69	67
	82.5	134	0.68	0.36	845.590	69	67
	85	134	0.67	0.32	846.680	69	67
	87.5	134	0.77	0.35	847.750	70	68
	90	134	0.71	0.34	848.840	70	68
	107.5	134	1.10	0.53	857.460	72	69
	110	133	1.10	0.53	858.940	72	69
	112.5	132	1.10	0.53	860.200	72	69
	115	132	1.43	0.70	862.220	72	70
	117.5	133	1.45	0.70	864.660	72	70
	120	131	1.50	0.49	866.420	72	70

Impinger No.	Impinger Contains	Final Weight [g]	Tare Weight [g]	Weight of Moisture [g]
1	100 mL H ₂ O	886.7	768.9	190.8
2	100 mL H ₂ O	781.2	727.8	23.4
3	Blank	629.6	627.4	2.2
4	200g Silica Gel	911.2	805.3	5.9
				Total Weight Gain [g]: 222.3
				Moisture Volume [mL]: 222.3

Calculations for: Northern Pulp Power Boiler PM

Test #1

Client: Northern Pulp

Job Number: 121413456

Plant: Power Boiler

Location: Picton, NS

Test: PB-1

Date: 17-Sep-15

Personnel: LRJAC

Calculated Parameters

Stack Gas Pressure, P_s (mHg)
Stack Gas Molecular Weight, Dry Basis, M_d (kDa-mole)
Volume of Water Vapour Collected, V_{wc} (cu.ft.)
Stack Gas Moisture Content (% as dry basis)
Stack Gas Molecular Weight, Wet Basis, M_w (kDa-mole)

30.01	29.44	10.570	0.181	27.23
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Isokinetic Checks

Isokinetic Checks					Isokinetics				
		Check range		Within Criteria			Gas Meter	Isokinetics	
		Check average		Within Criteria			V _m (ft.s.)	V _m (ft.s.)	
Traverse	Point	Time (min)	Stack Gas Temp, T _s (R)	Stack Gas Velocity, Us (ft/s)	Orifice diam H (in. H ₂ O)	Meter Press., P _m (in. Hg)	Avg. Temp, T _m (R)	Volume, Vm (cu. ft.)	V _m (ft.s.)
Traverse 1	1	2.5	583	0.55	0.26	41.93	30.02	521	0.824
	5	583	0.55	0.28	41.93	30.02	521	0.815	105.37
	7.5	583	0.50	0.28	43.80	30.02	522	0.821	104.27
	10	584	0.62	0.29	44.56	30.02	522	0.870	100.69
	12.5	582	0.62	0.29	44.46	30.02	522	0.900	101.87
	15	582	0.64	0.30	45.20	30.02	522	0.947	101.87
	17.5	583	0.57	0.27	42.89	30.02	523	0.890	100.37
	20	583	0.57	0.27	42.69	30.02	523	0.960	105.16
	22.5	581	0.57	0.27	42.62	30.02	523	0.970	103.01
	25	583	0.57	0.27	42.69	30.02	523	0.980	103.91
	27.5	583	0.57	0.27	42.69	30.02	524	0.990	103.01
	30	583	0.50	0.28	41.43	30.02	524	0.999	104.21
	32.5	582	0.60	0.28	43.78	30.02	525	0.990	103.06
	35	583	0.61	0.29	44.10	30.02	525	0.990	103.06
	37.5	583	0.73	0.35	48.31	30.03	525	1.110	106.44
	40	584	0.76	0.36	49.34	30.03	525	1.120	104.87
	42.5	585	0.91	0.44	50.03	30.03	526	1.053	103.76
	45	582	0.95	0.45	55.07	30.03	526	1.240	104.93
	47.5	585	1.10	0.53	59.40	30.04	526	1.260	104.06
	50	584	1.10	0.53	58.35	30.04	526	1.300	100.08
	52.5	583	1.20	0.57	61.94	30.04	526	1.350	103.84
	55	583	1.20	0.57	61.84	30.04	526	1.420	104.49
	57.5	581	1.30	0.62	64.36	30.05	526	1.184	108.81
	60	582	1.30	0.62	64.42	30.05	526	1.440	101.85
								1.224	101.73
Traverse 2	1	62.5	581	0.95	0.45	55.02	30.03	527	1.260
	65	580	0.95	0.48	54.97	30.03	527	1.220	103.80
	67.5	580	0.90	0.43	53.51	30.03	527	0.220	101.25
	70	581	0.90	0.43	53.55	30.03	527	0.187	18.60
	72.5	582	0.90	0.48	50.53	30.03	527	1.280	106.18
	75	582	0.90	0.48	50.53	30.03	528	2.100	168.30
	77.5	583	0.75	0.36	48.87	30.03	528	1.120	104.48
	80	583	0.75	0.36	48.87	30.03	528	1.120	103.90
	82.5	584	0.86	0.33	48.67	30.02	528	1.140	105.66
	85	584	0.67	0.22	48.12	30.02	528	1.090	106.08
	87.5	584	0.72	0.25	48.02	30.03	528	1.070	104.80
	90	584	0.71	0.24	47.98	30.03	528	1.080	102.91
	92.5	584	0.80	0.39	50.62	30.03	530	1.160	104.67
	95	582	0.62	0.40	51.29	30.03	530	1.200	103.90
	97.5	585	0.92	0.44	54.13	30.03	530	1.240	106.15
	100	585	0.87	0.45	54.82	30.03	530	1.250	103.57
	102.5	583	1.05	0.51	57.84	30.04	531	1.110	103.84
	105	584	1.03	0.53	59.35	30.04	531	1.148	102.17
	107.5	584	1.10	0.55	59.35	30.04	531	1.148	103.72
	110	583	1.10	0.55	59.30	30.04	531	1.248	112.77
	112.5	582	1.50	0.73	69.19	30.05	531	1.260	95.92
	115	582	1.45	0.70	68.03	30.05	531	1.530	89.71
	117.5	583	1.45	0.70	68.03	30.05	531	1.590	105.38
	120	581	1.50	0.73	68.13	30.05	531	1.540	102.15
Total	120	583	0.89	0.42	Average	Average	Average	Total	48.374
					52.31	52.31	52.31		57.050

Combustion Gas Data for: Northern PulpClient: Northern Pulp
Job Number: 121413456

Plant: Power Boiler

Location: Picton, NS

Test: PM-1

Date: 17-Sep-15

Personnel: JJB/JC

Test Start: 9:30 AM
Test Finish: 10:00 AM

Time (min)	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	NO _x (ppm)
0	12.2	5.5	75	0	48
5	13.1	5.6	83	0	48
10	13.2	5.7	68	0	49
15	13.0	5.8	64	0	44
20	12.9	6.1	68	0	47
25	12.7	6.0	73	0	51
30	12.8	6.0	72	0	52
Average:	12.8	5.6	72	0	48

Raw Data for: Northern Pulp Power Boiler PM

Test #2

Client: Northern Pulp
Job Number: 121413456

Plant: Power Boiler

Location: Picton, NS

Test: PM-2

Date: 17-Sep-15

Personnel: JNB/NVC

Test Start: 1:40 PM

Test Finish: 3:40 PM

Barometric Pressure, Pbar [in. Hg]

Stack Static Pressure, Psstatic [in. H2O]

Ambient Temp, [°F]

H2O Volume Collected, Vw [mL]

Total # Sampling Points, [mL]

Sampling Time Per Point, [min]

Regulatory Agency

Parameters		Particulate Collected from Filter [mg]:		Particulate Collected from Probe Wash [mg]:		Particulate Collected from Impinger Wash [mg]:		Total Particulate Collected [mg]:	
Barometric Pressure, Pbar [in. Hg]		30.00		Q2, (%)		11.9		72.7	
Stack Static Pressure, Psstatic [in. H2O]		0.18		CO2, (%)		6.6		165.2	
Ambient Temp, [°F]		63		N2, (%)		61.5		21.5	

Nozzle Volume Collected, Vw [mL]

Total # Sampling Points, [mL]

Sampling Time Per Point, [min]

Regulatory Agency

Traverse	Point	Time [min]	Stack Gas Temp, Ts [°F]	S-type Pilot delta P [in. H2O]	Orifice delta H [in. H2O]	Gas Meter Volume [cu. ft.]	Inlet [°F]	Gas Meter Temp Outlet [°F]	Weight of Moisture Volumes [ml.]
Traverse 1	1	2.5	130	1.20	0.54	867.020	78	78	223.5
	5	5	131	1.10	0.54	869.710	80	78	
	7.5	7.5	131	1.10	0.54	871.650	82	78	
	10	10	131	1.00	0.49	872.550	82	78	
	12.5	12.5	131	0.92	0.43	873.400	81	78	
	15	15	131	0.90	0.44	874.840	82	78	
	17.5	17.5	131	0.80	0.39	876.020	82	78	
	20	20	131	0.80	0.39	877.160	82	78	
	22.5	22.5	130	0.80	0.39	878.280	83	80	
	25	25	130	0.75	0.37	879.350	83	80	
	27.5	32	0.80	0.40	880.540	83	80		
	30	32	0.80	0.40	881.720	83	80		
	32.5	32	0.85	0.42	882.920	83	80		
	35	35	130	0.85	0.42	884.100	84	80	
	37.5	40	131	0.92	0.45	885.300	84	81	
	40	130	0.91	0.45	886.500	84	81		
	42.5	130	1.10	0.54	887.700	84	81		
	45	130	1.10	0.54	889.220	84	81		
	47.5	130	1.50	0.74	890.750	84	81		
	50	130	1.50	0.74	892.310	84	81		
	52.5	130	1.10	0.54	893.720	84	81		
	55	131	1.50	0.74	895.250	84	81		
	57.5	131	1.30	0.64	896.750	84	81		
	60	130	1.50	0.74	898.290	84	81		
Traverse 2	1	62.5	129	1.10	0.54	898.290	84	81	
	65	129	1.10	0.54	901.050	84	81		
	67.5	131	1.50	0.63	902.740	84	81		
	70	131	1.15	0.57	903.120	84	81		
	72.5	132	1.10	0.54	906.460	84	81		
	75	132	0.93	0.47	907.750	84	81		
	77.5	132	0.84	0.42	916.220	84	81		
	80	132	0.85	0.42	917.430	84	81		
	82.5	131	0.85	0.42	918.570	84	81		
	85	133	0.82	0.41	911.440	84	81		
	87.5	132	0.81	0.40	912.640	84	81		
	90	133	0.81	0.40	913.820	84	81		
	92.5	132	0.95	0.47	912.240	84	81		
	95	132	0.84	0.42	915.030	84	81		
	97.5	132	0.93	0.47	917.560	84	81		
	100	131	0.85	0.42	918.240	84	81		
	102.5	132	0.90	0.44	919.790	84	81		
	105	132	0.92	0.43	921.020	84	81		
	107.5	132	0.95	0.47	922.240	84	81		
	110	132	0.97	0.45	923.540	84	81		
	112.5	131	1.00	0.49	923.000	84	81		
	115	131	1.03	0.52	926.120	84	81		
	117.5	130	1.20	0.59	927.510	84	81		
	120	130	1.30	0.64	928.920	84	81		

Impinger No.

Cameras

Final Weight

Tare Weight

Weight of

Moisture [g]

100 ml. H2O

100 ml. H2O

Blank

200g Silica Gel

11.9

754.0

828.1

925.4

912.1

223.5

223.5

Stack Diameter, [in.]

Stack Area, [sq. in.]

Probe Length, [in.]

Nozzle Diameter, [in.]

Pilot Coefficient, [Cp]

Gamma, mean constant

Port Length [in.]

72

28.27

0

0.175

0.78

0.829

4

Calculations for: Northern Pulp Power Boiler P&I
Test #2

Client: Northern Pulp
Job Number: 121413458

Plant: Power Boiler
Location: Picton, NS
Test: P&I-2
Date: 17-Sep-15
Personnel: J.S.WNC

Calculated Parameters

Stack Gas Pressure, ps (in.Hg)
Stack Gas Molecular Weight, Dry Basis, Molar (lb/mole)
Volume of Water Vapour Collected, Vol (cu.ft.)
Stack Gas Moisture Content (% as received)
Stack Gas Molecular Weight, Wet Basis, M (lb/mole)

	30.01 29.53 10.720 0.173 27.53	Check range Check average	Within Criteria Within Criteria
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Traverses

Traverse Point	Time (min)	Stack Gas Temp, Ts (K)	S-type Pitot, static P (in. H2O)	Orifice dia H (in. H2O)	Stack Gas Velocity, Us (ft/s)	Gas Meter Vm [ft/s]	Avg. Temp, Tm (K)	Volume, Vm [cu. ft.]	Vol. @ Ref. Vm (cu. ft.)	Kinetics 1 (%)
Isokineticity Checks										
Traverse 1	1	2.5	500	1.20	0.54	61.61	30.04	538	1,130	97.01
	5	5	501	1.10	0.54	50.04	30.04	510	1,103	98.99
	7.5	7.5	501	1.10	0.54	50.04	30.04	540	1,110	99.84
	10	10	501	0.90	0.48	50.29	30.04	540	1,077	101.37
	12.5	12.5	503	0.92	0.45	50.08	30.03	540	1,034	101.69
	15	15	501	0.90	0.44	53.40	30.03	541	1,040	101.72
	17.5	17.5	501	0.80	0.39	50.35	30.03	541	1,080	102.66
	20	20	501	0.80	0.39	50.35	30.03	541	1,140	99.18
	22.5	22.5	500	0.60	0.39	50.30	30.03	542	1,120	99.24
	25	25	500	0.75	0.37	48.71	30.03	542	1,110	99.46
	27.5	27.5	502	0.80	0.40	50.39	30.03	542	1,150	99.55
	30	30	502	0.80	0.40	50.39	30.03	542	1,160	99.74
	32.5	32.5	500	0.85	0.42	51.85	30.03	542	1,200	102.50
	35	35	500	0.65	0.42	51.85	30.03	542	1,180	100.92
	37.5	37.5	501	0.92	0.45	53.50	30.03	543	1,200	99.24
	40	40	500	0.91	0.45	53.65	30.03	543	1,250	101.52
	42.5	42.5	500	1.10	0.54	50.96	30.04	543	1,220	100.88
	45	45	500	1.10	0.54	50.96	30.04	543	1,112	99.74
	47.5	47.5	500	1.50	0.74	68.80	30.05	543	1,530	98.85
	50	50	500	1.50	0.74	68.80	30.05	543	1,560	98.75
	52.5	52.5	500	1.10	0.54	50.96	30.04	543	1,410	104.18
	55	55	501	1.50	0.74	68.84	30.05	543	1,540	124.9
	57.5	57.5	501	1.30	0.84	64.18	30.05	543	1,480	101.38
	60	60	500	1.50	0.74	68.88	30.05	543	1,540	97.49
	12	12								
Traverse 2	1	62.5	500	1.10	0.54	50.94	30.04	543	1,430	117.57
	65	65	500	1.10	0.54	50.94	30.04	543	1,350	100.16
	67.5	67.5	501	1.50	0.65	68.94	30.05	543	1,150	72.84
	70	70	501	1.15	0.57	60.36	30.04	543	1,540	111.36
	72.5	72.5	502	1.10	0.54	50.96	30.04	543	1,340	102.13
	75	75	502	1.10	0.54	50.96	30.04	543	1,340	99.17
	77.5	77.5	502	0.95	0.47	54.81	30.03	543	1,300	101.51
	80	80	502	0.95	0.47	54.81	30.03	543	1,260	100.33
	82.5	82.5	501	1.00	0.42	51.90	30.03	543	1,220	102.60
	85	85	503	0.82	0.41	51.06	30.03	543	1,200	98.92
	87.5	87.5	503	0.61	0.40	50.75	30.03	543	1,220	105.27
	90	90	501	0.81	0.40	50.75	30.03	543	1,160	99.55
	92.5	92.5	503	0.64	0.42	51.96	30.03	543	1,210	102.53
	95	95	503	0.84	0.42	51.98	30.03	543	1,180	100.84
	97.5	97.5	503	0.85	0.42	51.96	30.03	543	1,210	102.12
	100	100	503	0.90	0.42	49.48	30.03	542	1,140	101.08
	102.5	102.5	502	0.90	0.44	53.44	30.03	542	1,220	100.97
	105	105	502	0.92	0.45	54.04	30.03	542	1,230	101.15
	107.5	107.5	502	0.95	0.47	54.81	30.03	542	1,260	100.51
	110	110	502	0.92	0.45	54.04	30.03	542	1,140	102.13
	112.5	112.5	501	1.05	0.49	50.29	30.04	543	1,203	113.22
	115	115	501	1.05	0.52	57.68	30.04	543	1,120	99.77
	117.5	117.5	500	1.20	0.59	61.61	30.04	543	1,390	99.24
	120	120	500	1.20	0.54	64.12	30.05	543	1,460	100.61
Total	120	Average 501	Average 1.02	Average 0.50	Average 0.51	Average 30.04	Average 542	Total 61,370	Total 51,116	Average 100.07

Combustion Gas Data for: Northern Pulp

Client: Northern Pulp
Job Number: 121413456

Plant: Power Boiler
Location: Picton, NS
Test: PM-2
Date: 17-Sep-15
Personnel: JIB/JWC

Test Start: 2:00 PM
Test Finish: 2:30 PM

	Time (min)	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	NOx (ppm)
	0	12.6	6.2	180	0	53
	5	12.5	6.3	160	0	58
	10	12.1	6.5	165	0	66
	15	11.9	6.6	252	0	62
	20	10.9	6.8	238	0	67
	25	11.0	7.0	200	0	65
	30	12.0	6.9	138	0	65
Average:		11.9	6.6	190	0	62

Raw Data for: Northern Pulp Power Boiler PM

Test #3

Client: Northern Pulp

Job Number: 121413456

Plant: Power Boiler
Location: Picton, NS
Test: PA-3
Date: 17-Sep-15
Personnel: JJB/JC

Test Start: 8:00 AM
Test Finish: 10:00 AM

Parameters
Barometric Pressure, Psbar [in. Hg]
Stack Static Pressure, Psstatic [in. H2O]
Ambient Temp, (°F)
H2O Volume Collected, Vw [mL]
Total # Sampling Points,
Sampling Time per Point, (min)
Readings Taken Every — mins
Regulatory Agency

Traverse Point	Time (min)	Stack Gas Temp, Ts (°F)	S-type Pitot data P [in. H2O]	Orifice delta H [in. H2O]	Gas Meter Volume (cu. ft.)	Gas Meter Temp Inlet (°F)	Outlet (°F)
Traverse 1	1	2.5	130	1.10	0.53	929.340	66
	5	130	1.10	0.53	912.050	67	67
	7.5	130	1.10	0.53	913.380	67	67
	10	130	1.10	0.53	934.700	67	67
	12.5	131	1.05	0.51	936.010	68	67
	15	131	1.05	0.51	937.290	68	67
	17.5	130	0.87	0.42	938.510	69	67
	20	130	0.87	0.42	939.720	70	67
	22.5	131	0.90	0.43	940.950	71	68
	25	131	0.79	0.42	941.680	71	68
	27.5	130	0.80	0.39	942.240	72	69
	30	130	0.80	0.64	944.180	72	69
	32.5	132	0.85	0.44	945.540	72	69
	35	133	0.80	0.39	946.880	73	69
	37.5	131	0.85	0.41	947.560	73	70
	40	131	0.85	0.41	949.050	73	70
	42.5	130	0.90	0.44	949.720	74	70
	45	130	0.90	0.44	951.500	74	71
	47.5	132	1.10	0.53	952.700	74	71
	50	132	1.10	0.53	953.920	74	72
	52.5	130	1.20	0.58	955.230	74	72
	55	130	1.30	0.63	956.400	75	72
	57.5	131	1.50	0.73	958.160	75	72
	60	130	1.50	0.73	960.880	75	72
Traverse 2	1	62.5	130	1.05	0.51	959.950	77
	2	65	130	1.05	0.51	962.540	77
	67.5	131	1.05	0.51	964.210	77	74
	70	132	0.85	0.42	974.830	78	74
	72.5	132	1.10	0.54	963.400	78	75
	75	132	1.10	0.54	964.990	78	75
	77.5	132	0.97	0.47	977.260	78	75
	80	132	1.00	0.49	978.620	78	76
	82.5	131	0.90	0.44	979.140	78	77
	85	131	0.90	0.44	979.220	78	76
	87.5	131	1.05	0.51	982.470	79	77
	90	133	0.85	0.42	984.830	79	77
	107.5	134	0.85	0.42	985.200	79	77
	110	134	1.10	0.54	986.370	79	77
	112.5	131	1.10	0.54	987.560	79	77
	115	131	1.15	0.56	989.340	79	77
	117.5	131	1.40	0.69	990.350	79	77
	120	131	1.40	0.69	992.790	79	77

Impinger No.	Impinger Contents 100 mL H2O	Final Weight (g)	Tare Weight (g)	Weight of Moisture (g)
1	100 mL H2O	90.0	717.2	186.6
2	100 mL H2O	744.0	723.6	21.3
Blank		628.7	628.1	2.6
200g Silica Gel		922.0	907.7	15.1
				Total Weight Gain (g)
				225.8
				Moisture Volume (mL)
				225.8

Parameter	Value	Unit
Particulate Collected from Filter (mg):	168.1	
Particulate Collected from Probe Wash (mg):	39.0	
Particulate Collected from Impinger Wash (mg):	39.2	
Total Particulate Collected (mg):	205.1	

Parameter	Value	Unit
O2 (%):	02.1%	
CO2 (%):	CO2.1%	
NO (%):	NO.0	
SO2 (%):	SO2.0	

Calculations for: Northern Pulp Power Boiler PM

Test #3

Client: Northern Pulp
Job Number: 124413456

Plant: Power Boiler
Location: Picton, NS
Test: PH-3
Date: 17-Sep-15
Personnel: JJB/JAC

Calculated Parameters

Stack Gas Pressure, P_a (in Hg)
Stack Gas Molecular Weight, Dry Basis, Mrd (lb/mole)
Volume of Water Vapour Collected, Vwv (cu. ft.)
Stack Gas Moisture Content (% as decimal)
Stack Gas Molecular Weight, Wet Basis, Mw (lb/mole)

Isokinetic Checks

	Traverse Point	Time [min]	Stack Gas Temp, T_s [R]	S-type Photo, dist. P (in. H2O)	Office Saks H (in. H2O)	Stack Gas Velocity, Us (ft/s)	Stack Gas Velocity, Us (ft/s)	Mass Flow, \dot{m} [lb/s]	Avg. Temp, Tm (R)	Gas Meter Volume, Vm (cu. ft.)	Vol @ Ref., Vm (cu. ft.)	Isokinetics I (%)
Traverse 1	1	2.5	590	1.10	0.53	58.90	30.04	527	1,360	1,154	103.09	
	5	5	590	1.10	0.53	58.90	30.04	527	1,350	1,145	102.23	
	7.5	7.5	590	1.10	0.53	58.90	30.04	527	1,330	1,128	100.72	
	10	10	590	1.10	0.53	58.90	30.04	527	1,320	1,119	99.96	
	12.5	12.5	591	1.05	0.51	57.60	30.04	528	1,310	1,110	101.52	
	15	15	591	1.05	0.51	57.60	30.04	528	1,280	1,084	98.20	
	17.5	17.5	590	0.87	0.42	52.39	30.03	528	1,220	1,032	103.66	
	20	20	590	0.87	0.42	52.39	30.03	529	0,480	0.414	41.60	
	22.5	22.5	591	0.90	0.43	53.33	30.03	520	1,180	1,585	157.58	
	25	25	591	0.79	0.42	49.87	30.03	520	1,180	1,004	105.10	
	27.5	27.5	590	0.80	0.39	50.23	30.03	521	1,160	0.877	102.29	
	30	30	590	0.80	0.64	56.23	30.05	531	1,140	0.981	100.59	
	32.5	32.5	592	0.85	0.44	51.87	30.03	531	1,160	0.976	99.33	
	35	35	593	0.85	0.39	50.36	30.03	531	1,140	0.959	100.69	
	37.5	37.5	591	0.85	0.41	51.82	30.03	532	1,160	0.982	100.45	
	40	40	591	0.85	0.41	51.82	30.03	532	1,180	1,000	101.71	
	42.5	42.5	590	0.90	0.44	53.26	30.03	532	1,220	1,025	101.16	
	45	45	590	0.90	0.44	51.24	30.03	532	1,230	1,033	101.99	
	47.5	47.5	582	1.10	0.53	59.00	30.04	531	1,200	1,007	90.99	
	50	50	582	1.10	0.53	59.00	30.04	533	1,220	1,023	91.50	
	52.5	52.5	590	1.20	0.58	61.52	30.04	533	1,410	1,182	101.09	
	55	55	590	1.30	0.63	64.04	30.05	534	1,470	1,232	101.18	
	57.5	57.5	581	1.50	0.84	68.84	30.05	534	1,560	1,308	100.07	
	60	60	590	1.50	0.73	68.79	30.05	534	1,590	1,313	101.91	
Traverse 2	1	62.5	590	1.05	0.51	57.55	30.00	536	1,560	1,320	118.84	
	65	65	590	1.05	0.51	57.55	30.04	536	1,350	1,127	102.87	
	67.5	67.5	581	1.05	0.51	57.50	30.04	536	1,330	1,127	103.06	
	70	70	582	1.10	0.54	59.00	30.04	536	1,380	1,160	103.76	
	72.5	72.5	582	1.10	0.54	59.00	30.04	537	1,390	1,158	103.58	
	75	75	582	1.10	0.54	59.00	30.04	537	1,400	1,166	104.32	
	77.5	77.5	582	0.97	0.47	55.41	30.04	537	1,320	1,008	105.54	
	80	80	582	1.00	0.49	56.20	30.03	537	1,320	1,029	103.14	
	82.5	82.5	581	0.90	0.44	53.23	30.04	537	1,280	1,085	105.25	
	85	85	581	0.90	0.44	53.23	30.03	537	1,260	1,048	103.59	
	87.5	87.5	582	0.95	0.42	51.87	30.03	537	1,250	1,040	105.84	
	90	90	589	0.85	0.42	59.00	30.03	537	1,250	1,040	105.32	
	92.5	92.5	585	0.90	0.44	53.51	30.03	537	1,280	1,085	105.54	
	95	95	585	0.90	0.44	53.51	30.03	537	1,260	1,048	103.94	
	97.5	97.5	581	0.90	0.44	53.42	30.03	538	1,260	1,047	103.57	
	100	100	581	0.90	0.44	53.42	30.03	538	1,260	1,047	103.67	
	102.5	102.5	581	1.05	0.51	57.60	30.04	538	1,330	1,105	101.65	
	105	105	581	1.00	0.49	59.21	30.04	538	1,340	1,113	104.34	
	107.5	107.5	584	1.10	0.54	59.10	30.04	538	1,360	1,155	103.45	
	110	110	584	1.10	0.54	59.10	30.04	538	1,370	1,138	101.97	
	112.5	112.5	581	1.10	0.54	58.85	30.04	538	1,360	1,155	102.21	
	115	115	581	1.15	0.56	60.20	30.04	538	1,380	1,146	98.24	
	117.5	117.5	581	1.40	0.69	64.51	30.04	538	1,510	1,253	117.72	
	120	120	581	1.40	0.69	60.51	30.05	538	1,940	1,612		
Total	120	Average	581	Average	Average	Average	Average	Average	Total	Total	Average	
									63,450	53,122		
									30.04	30.04		2722.63

Combustion Gas Data for: Northern PulpClient: Northern Pulp
Job Number: 121413456Plant: Power Boiler
Location: Pictou, NS
Test: PM-3
Date: 17-Sep-15
Personnel: JJB/JCTest Start: 8:30 AM
Test Finish: 9:00 AM

Time [min]	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	NO _x (ppm)
0	11.5	6.8	83	0	52
5	11.9	6.6	55	0	52
10	11.9	6.7	62	0	55
15	12.0	6.6	57	0	52
20	11.5	6.8	71	0	55
25	12.1	6.5	82	0	54
30	12.0	6.5	69	0	56
Average:	11.8	6.7	67	0	54

DATA ENTRY

Northern Pulp
Pictou, NS
Fuel: Natural Gas
Operating Conditions: normal
Emission Control Equipment: scrubber
Stack Height from Grade: 51 m
Stack Diameter: 1.93 m

Reference Temperature, Tref (F): 77
(K): 298
Reference Pressure, Pref (in.Hg): 29.92
(Bar): 1.0

Parameter	Symbol	Units	Test 1	Test 2	Test 3	Average
Test ID	-	-	PM-1	PM-2	PM-3	-
Date	-	-	17-Sep-15	17-Sep-15	17-Sep-15	n/a
Start Time	-	-	9:10 AM	1:40 PM	8:00 AM	n/a
End Time	-	-	11:10 AM	3:40 PM	10:00 AM	n/a
Total Sampling Time	-	min	120	120	120	120
Stack Diameter	D	in.	72	72	72	72
Average Stack Gas Temperature	Ts	F	133	131	131	132
Average Dry Gas Meter Temperature	Tm	F	67	82	74	74
Barometric Pressure	Pbar	in.Hg	30.00	30.00	30.00	30.00
Stack Static Pressure	Pstatic	in.H2O	0.18	0.18	0.52	0.29
Average Pressure Drop (Head)	dP	in.H2O	0.88	1.02	1.02	0.87
Average deltaH Orifice	dH	in.H2O	0.42	0.50	0.51	0.47
Average Meter Temperature	Tm	F	67	82	74	74
Gas Sample Volume	Vm	c.u.ft	57.05	61.97	63.45	60.82
Average Isokinetics	I	%	104	100	103	102
Nozzle Diameter	Da	in.	0.175	0.175	0.175	0.175
Pitot Coefficient	Cp	-	0.780	0.780	0.780	0.780
Gamma, meter constant	y	-	0.829	0.829	0.829	0.829
Reference Temperature	Tref	R	537	537	537	537
Reference Pressure	Pref	in.Hg	29.92	29.92	29.92	29.92
Stack Gas Oxygen Content	Co2	%	12.8	11.8	11.8	12.2
Stack Gas Carbon Dioxide Content	Cco2	%	5.8	6.6	6.7	6.4
Stack Gas Nitrogen Content	Cn2	%	81.3	81.5	81.5	81.5
Stack Gas Sulphur Dioxide Content	Cso2	ppm	0.0	0.0	0.0	0.0
Stack Gas Nitrogen Oxides Content	Cnox	ppm	48.4	62.3	53.7	54.8
Stack Gas Carbon Monoxide Content	Cco	ppm	71.9	190.4	67.1	109.8
Volume of Water Collected	Vw	mL	222.3	223.5	225.8	223.9
Particulate Collected from Filter	-	mg	184.8	198.8	166.1	183.2
Particulate Collected from Probe Wash	-	mg	67.0	60.0	39.0	55.3
Particulate Collected from Impinger Wash	-	mg	15.8	5.9	39.2	20.3
Total Particulate Collected (excluding impingers)	Mp	mg	251.8	258.7	205.1	238.5

Legend:

- F - degrees Fahrenheit
- K - degrees Kelvin
- Bar - bars
- in.Hg - inches of mercury
- in. - inches

in.H2O - inches of water
 cu.ft - cubic feet
 R - degrees Rankin
 NOx - as NO2

CALCULATIONS

Northern Pulp
 Pictou, NS
 Fuel: Natural Gas
 Operating Conditions: normal
 Emission Control Equipment: scrubber
 Stack Height from Grade: 51 m
 Stack Diameter: 1.93 m

Variable	Symbol	Units	Calculation	Test 1	Test 2	Test 3	Average
Stack Area	A _s	sq.ft sq.m	$A_s = \pi \times ((D/12)^2 \times 4)$ $A_s (\text{sq.m}) = A_s (\text{sq.ft}) \times 0.0929$	28.27 2.63	28.27 2.63	28.27 2.63	28.27 2.63
Barometric Pressure Stack Static Pressure Avg. Stack Temperature Avg. Meter Temperature Nozzle Diameter	P _{bar} P _{static} T _s T _m D _n	kPa kPa R R mm	$P_{bar} (\text{kPa}) = P_{bar} (\text{in.Hg}) \times 3.386$ $P_{static} (\text{kPa}) = P_{static} (\text{in.Hg}) \times 0.249$ $T_s (\text{R}) = T_s (\text{F}) + 460$ $T_m (\text{R}) = T_m (\text{F}) + 460$ $D_n (\text{mm}) = D_n (\text{in.}) \times 25.4$	101.6 0.04 593 527 4	101.6 0.04 591 542 4	101.6 0.13 591 534 4	101.6 0.07 592 534.0 4.4
Gas Meter Pressure Sample Volume at Ref Cond Volume of Water Vapour Water Fraction	P _m V _m V _{wv} B _{wf}	in.Hg cu.ft cu.m cu.ft	$P_m = P_{bar} + (dH / 13.6)$ $V_m = Tref/Ts \times (V_m \times P_m \times R) / Tm$ $V_{wv} (\text{cu.m}) = 0.02832 \times V_{wv} (\text{cu.ft})$ $V_{wv} = 0.0480 \times V_w$ $B_{wf} = V_{wv} / (V_{wv} + V_{m,0})$	30.03 48.40 1.37 10.67 0.181	30.04 51.12 1.45 10.73 0.173	30.04 53.14 1.50 10.84 0.169	30.03 50.9 1.44 10.75 0.2
Molecular Weight, Dry Molecular Weight, Wet	M _d M _w	lb/lbmol lb/lbmol	$M_d = 0.44 (\text{CO}_2) + 0.37 (\text{CH}_4) + 0.19 (\text{N}_2)$ $M_w = M_d (1 - B_{wf}) + (18 \times B_{wf})$	29.44 27.38	29.53 27.53	29.54 27.58	29.5 27.5
Stack Pressure Stack Gas Velocity Actual Stack Gas Flow Rate Dry Stack Gas Flow Rate	P _s U _s Q Q _d	in.Hg ft/s m/s scfm scfm Rcfm Rcfm	$P_s = P_{bar} + (P_{static} / 13.6)$ $U_s = 0.533 \times C_p \times (dH \times P_m \times T_m) / (P_m \times M_w) \times 0.3$ $m/s = 0.304 ft/s ; U_s (m/s)$ $Q = 60 \times U_s \times A_s$ $Q_t = Q \times (1-B_{wf}) \times (Tref/Ts) \times (P_m/Pref)$ $Q_t (\text{Rcfm}) = 0.000472 \times Q_t (\text{Rcfm})$	30.01 52.31 15.94 88.738 66.060 31.18	30.01 56.51 17.22 99.868 72.202 34.08	30.04 56.73 17.29 96.233 72.872 34.40	30.02 55.2 16.8 93.613 70.376 33.2
Sulphur Dioxide - SO ₂ SO ₂ Measured Concentration Uncorrected @ Ref Cond SO ₂ Emission Rate	C _{so2} C _{so2} ER _{so2}	ppm mg/Rcm g/s kg/hr	Measurement from Flue Gas Analyzer $C_{so2} (\text{mg/Rcm}) = C_{so2} (\text{ppm}) \times 2.62$ $ER_{so2} = C_{so2}/1000 \times Q_t$ $ER_{so2} (\text{kg/hr}) = 3.6 \times ER_{so2} (\text{g/s})$	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00
SO ₂ Concentration Corrected to 11% O ₂ Corrected to 3% O ₂ Corrected to 12% CO ₂	C _{so2} C _{so2} C _{so2}	mg/Rcm mg/Rcm mg/Rcm	$C_{so2} (11\% \text{O}_2) = C_{so2} (\text{mg/Rcm}) \times (20.9-11) / (20.9-\text{Ca}_2)$ $C_{so2} (3\% \text{O}_2) = C_{so2} (\text{mg/Rcm}) \times (20.9-3) / (20.9-\text{Ca}_2)$ $C_{so2} (12\% \text{CO}_2) = C_{so2} (\text{mg/Rcm}) \times (12/\text{Ca}_2)$	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.00 0.00
Nitrogen Oxides - NO _x NO _x Measured Concentration Uncorrected @ Ref Cond NO _x Emission Rate	C _{nox} C _{nox} ER _{nox}	ppm mg/Rcm g/s kg/hr	Measurement from Flue Gas Analyzer $C_{nox} (\text{mg/Rcm}) = C_{nox} (\text{ppm}) \times 1.382$ $ER_{nox} = C_{nox}/1000 \times Q_t$ $ER_{nox} (\text{kg/hr}) = 3.6 \times ER_{nox} (\text{g/s})$	48.43 91.14 2.84 10.23	62.29 117.22 3.99 14.38	53.71 101.09 3.48 12.52	54.81 103.15 3.44 12.38
NO _x Concentration Corrected to 11% O ₂ Corrected to 3% O ₂ Corrected to 12% CO ₂	C _{nox} C _{nox} C _{nox}	mg/Rcm mg/Rcm mg/Rcm	$C_{nox} (11\% \text{O}_2) = C_{nox} (\text{mg/Rcm}) \times (20.9-11) / (20.9-\text{Ca}_2)$ $C_{nox} (3\% \text{O}_2) = C_{nox} (\text{mg/Rcm}) \times (20.9-3) / (20.9-\text{Ca}_2)$ $C_{nox} (12\% \text{CO}_2) = C_{nox} (\text{mg/Rcm}) \times (12/\text{Ca}_2)$	111.99 202.49 188.11	128.35 232.07 212.76	110.46 199.73 182.07	116.93 211.43 194.31
Carbon Monoxide - CO CO Measured Concentration Uncorrected @ Ref Cond CO Emission Rate	C _{co} C _{co} ER _{co}	ppm mg/Rcm g/s kg/hr	Measurement from Flue Gas Analyzer $C_{co} (\text{mg/Rcm}) = C_{co} (\text{ppm}) \times 1.143$ $ER_{co} = C_{co}/1000 \times Q_t$ $ER_{co} (\text{kg/hr}) = 3.6 \times ER_{co} (\text{g/s})$	71.86 82.28 2.57 9.24	190.43 218.04 7.43 26.75	67.14 76.88 2.64 9.52	109.81 125.73 4.21 15.17
CO Concentration Corrected to 11% O ₂ Corrected to 3% O ₂ Corrected to 12% CO ₂	C _{co} C _{co} C _{co}	mg/Rcm mg/Rcm mg/Rcm	$C_{co} (11\% \text{O}_2) = C_{co} (\text{mg/Rcm}) \times (20.9-11) / (20.9-\text{Ca}_2)$ $C_{co} (3\% \text{O}_2) = C_{co} (\text{mg/Rcm}) \times (20.9-3) / (20.9-\text{Ca}_2)$ $C_{co} (12\% \text{CO}_2) = C_{co} (\text{mg/Rcm}) \times (12/\text{Ca}_2)$	101.09 182.79 169.81	238.75 431.67 395.75	84.01 151.89 138.46	141.28 255.45 234.67
Particulate Concentration Particulate Emission Rate	C _p ER _p	mg/Rcm g/s kg/hr	$C_p = M_p / V_{m,0}$ $ER_p = C_p/1000 \times Q_t$ $ER_p (\text{kg/hr}) = 3.6 \times ER_p (\text{g/s})$	183.66 5.73 20.62	178.74 6.09 21.93	136.28 4.69 16.87	166.22 5.50 19.81
Particulate Concentration Corrected to 11% O ₂ Corrected to 3% O ₂ Corrected to 12% CO ₂	C _p C _p C _p	mg/Rcm mg/Rcm mg/Rcm	$C_p (11\% \text{O}_2) = C_p (20.9-11) / (20.9-\text{Ca}_2)$ $C_p (3\% \text{O}_2) = C_p (20.9-3) / (20.9-\text{Ca}_2)$ $C_p (12\% \text{CO}_2) = C_p (12/\text{Ca}_2)$	225.67 408.02 379.05	195.71 353.86 324.41	148.91 269.25 245.44	190.10 343.71 316.30

Legend:
 sq.ft = square foot
 sq.m = square metres
 ft = 3.142
 R = degrees Rankin
 ppm = parts per million

in.Hg = inches of mercury
 cu.ft = cubic feet
 cu.m = cubic metres
 Ref Cond = reference temperature and pressure (25 °C and 101.3 kPa)
 Rcfm = dry reference cubic metres per second
 Rcfm = actual cubic feet per minute

mg/Rcm = milligrams per dry reference cubic metre
 g/s = grams per second
 NO_x = NO₂
 acfm = actual cubic feet per minute

OFFICIAL STACK TESTING RESULTS

Northern Pulp

Pictou, NS

Fuel: Natural Gas

Operating Conditions: normal

Emission Control Equipment: scrubber

Stack Height from Grade: 51 m

Stack Diameter: 1.93 m

Parameter	Test 1	Test 2	Test 3	Average	NSENV Limits
Test ID Test Date	PM-1 17-Sep-15	PM-2 17-Sep-15	PM-3 17-Sep-15	- -	- -
Stack Gas Temperature (C) Moisture Content (%) Velocity (m/s) Volumetric Flow (Rcms)	56.1 18.1 15.9 31.2	55.1 17.3 17.2 34.1	55.2 16.9 17.3 34.4	55.4 17.5 16.8 33.2	- - - -
Oxygen - O2 (%) Carbon Dioxide - CO2 (%)	12.8 5.81	11.9 6.61	11.8 6.66	12.2 6.36	- -
Sulphur Dioxide - SO2 SO2 Measured Concentration (ppm) Uncorrected at Ref Cond (mg/Rcm) Emission Rate (kg/hr)	0.0 0.0 0.00	0.0 0.0 0.00	0.0 0.0 0.00	0.0 0.0 0.00	- - -
Nitrogen Oxides - NOx NOx Measured Concentration (ppm) Uncorrected at Ref Cond (mg/Rcm) Emission Rate (kg/hr)	48.4 91.1 10.23	62.3 117.2 14.38	53.7 101.1 12.52	54.8 103.2 12.38	- - -
Carbon Monoxide - CO CO Measured Concentration (ppm) Uncorrected at Ref Cond (mg/Rcm) Emission Rate (kg/hr)	71.9 82.3 9.24	190.4 218.0 26.75	67.1 76.9 9.52	109.8 125.7 15.17	- - -
Particulate Matter - PM Particulate Concentration (mg/Rcm) Concentration, corrected to 11% O2 (mg/Rcm) Particulate Emission Rate (kg/hr)	183.7 225.7 20.62	178.7 195.7 21.93	136.3 148.9 16.87	166.2 190.1 19.81	- 150 -

Legend: C - degrees Celsius
 m/s - metres per second
 Rcms - dry reference cubic metres per second
 ppm - parts per million

Ref Cond - reference temperature and pressure (25 C and 101.3 kPa)
 mg/Rcm - milligrams per dry reference cubic metre
 NOx - as NO2
 ND - non-detectable

Particulate Recoveries / Impinger Catch, Probe Wash, Filter Catch

Client: Northern Pulp
 Facility: Paper Mill
 Location: Dixie, NS
 Job Number: 121113496

IMPINGER CATCH

Container ID	Bottle Pre Weights [g]		Sample ID	Recoveries				Bottle Post Weights [g]		Unconnected Particulate Weight [g]	
	Date Analyzed by			Jar + Sample + Rinse [g]	Total Volume [ml]	Precise Volume [ml]	Total Rinse [ml]	Average			
	Trial 1	Trial 2	Average	[g]	[g]	[g]	[g]	Trial 1	Trial 2		
N1	112.6340	117.5244	112.5242	PM4-1	684.8	372.8	222.3	40.6	130.7	112.6510	0.0158
W1	117.0277	117.9275	117.8775	PM4-2	699.2	373.0	223.5	24.9	127.9	117.9342	0.0059
B5	110.4620	110.3401	110.3401	PM4-3	1175.0	375.9	225.8	36.7	810.0	110.4259	0.0439
U3	111.1023	111.1020	111.1022	V48	660.0	371.8	268.2	—	286.2	111.1041	0.0022
											0.00008

PROBE WASH

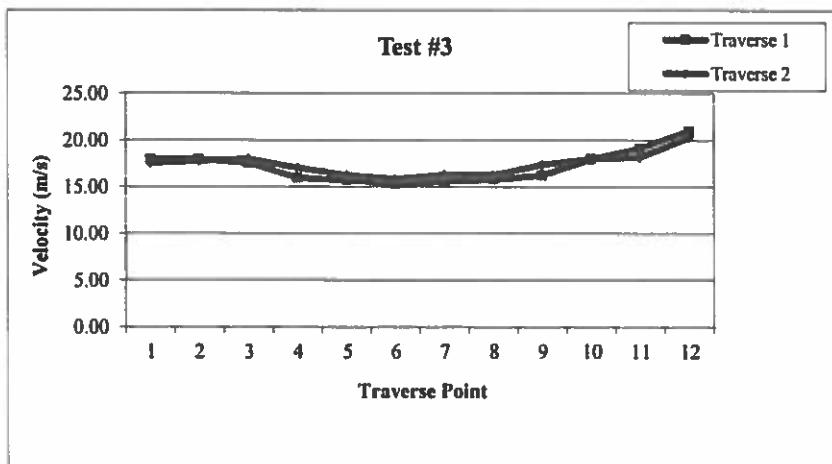
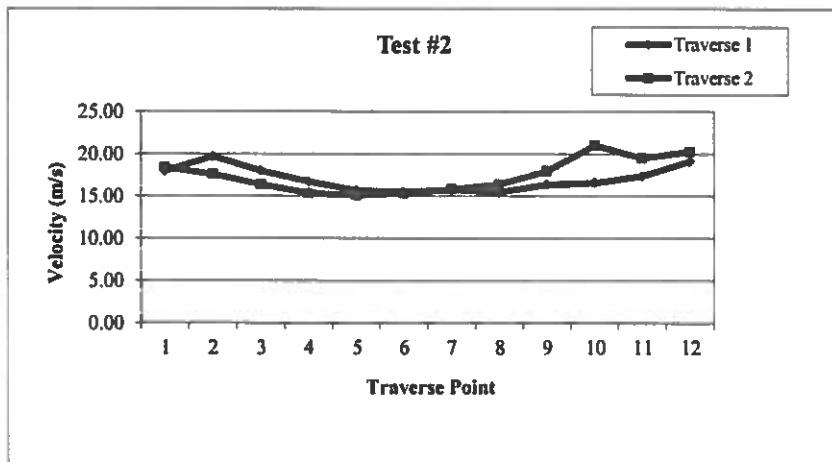
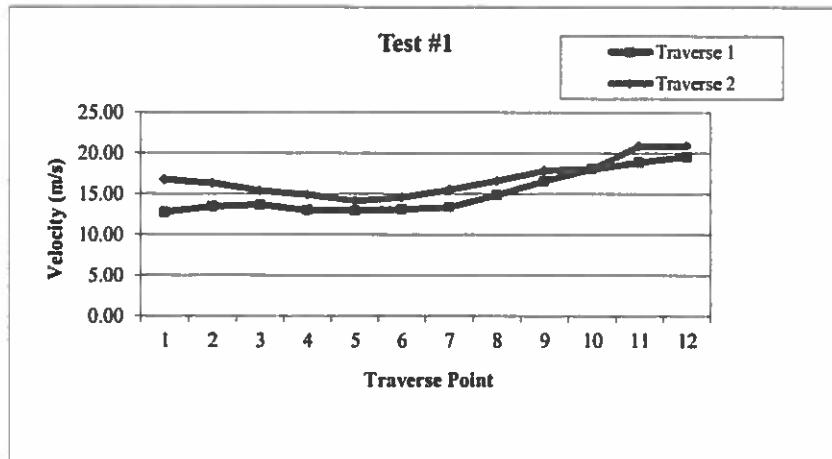
Container ID	Bottle Pre Weights [g]		Sample ID	Recoveries				Bottle Post Weights [g]		Unconnected Particulate Weight [g]	
	Date Analyzed by			Jar + Acetone [g]	Total Acetone [ml]	Precise Acetone [ml]	Total Acetone [ml]	Average			
	Trial 1	Trial 2	Average	[g]	[g]	[g]	[g]	Trial 1	Trial 2		
K3	110.4656	110.4551	110.4554	PM4-1	395.1	298.7	108.4	24.9	133.3	110.9160	0.0776
C2	111.6305	111.6351	111.6353	PM4-2	398.8	310.2	88.6	18.1	105.7	111.7017	0.0651
Y4	110.9559	110.9564	110.9567	PM4-3	381.5	285.5	96.0	17.3	111.3	110.6404	0.0445
B1	111.6523	111.6520	111.6522	AB	340.9	295.1	54.9	—	54.9	111.6540	0.0026
											0.000038

Density of Acetone: 0.7850 g/ml

FILTER CATCH

Filter ID	Pre Weights [g]		Sample ID	Post Weights [g]				Particulate Weight from Filter [g]	
	Date Analyzed by			Jar	Total	Average	Acetone	Date	
	Trial 1	Trial 2	Average	[g]	[g]	[g]	[g]	[g]	
0716-06	0.3316	0.3315	0.3316	PM4-1	0.5216	0.5111	0.5164	0.1845	
0812-25	0.3705	0.3705	0.3707	PM4-2	0.6667	0.6622	0.5985	0.1948	
0812-40	0.3723	0.3720	0.3722	PM4-3	0.5385	0.5380	0.5393	0.1861	

Stack Gas Velocity Profiles
Pictou, NS



Source Testing Data Checklist

Project Number: 121413456
 Spreadsheet Checker: CAL
 Date Checked: 10/14/2015
 Data Entered By:

Data Entity	Yes or No	Notes:
1) Are the facility and client names consistent across the trials?		
2) Have the stack height, stack diameter, fuel burned, and operating conditions been entered on the Data Entry tab?		
3) If the sheet has been modified to include more/less points or traverses have the average and summation formulas been adjusted (Calc sheets)?		
4) Have any changes to the testing protocol been entered in the sheet (as appropriate)?		
5) For clients with multiple tests (e.g. PM and Formaldehyde):		
A) Are the data copied over correctly (if appropriate)?		
B) Are the facility and client names consistent between all tests?		
C) If appropriate, does the data calculated in each trial agree between the different tests (velocity, volume, molecular weights, etc.)?		
Analysis		
1) Have the results been corrected to the reference conditions stated in the Pre-Test Plan/Approval to Operate?		
2) If applicable, are the results on the Summary sheet corrected to a particular O ₂ or CO ₂ concentration?		
3) Have the isotokineticity values been scanned for low (< 90%) and high (> 120%) numbers?		
4) Looking at the Data Entry, Calculations, and Summary sheets, are the results consistent across all trials?		
5) Has a scan of the raw data (including gas data) been performed to find any obvious typos?		
6) If source has been tested previously, are the results similar?		
7) For PMA tests, are there any outliers on the Recovery sheet (in particular, the Probe Wash)?		
8) Have the calibration data been checked (Cp, nozzle ID, gamma)?		
9) If appropriate, are the SO ₂ emission reasonable (based on fuel type)?		
10) If relevant, do the Chain of Custody forms agree with what was analyzed? Do the lab results make sense?		
Final Product		
1) Are the labels on the velocity charts meaningful/correct (West Traverse vs. Traverse 1)?		
2) Has the axis been formatted (min and max) so the data is easy to see?		
3) Have the calibration documents been saved?		
4) Have the fieldsheets been scanned and saved?		

Calculations for: Northern Pulp Recovery Boiler PW

Client: Northern Pulp
Job Number: 121413456

Calculated Parameters

Stack Gas Pressure, P_s (in lb/in²)
Stack Gas Molecular Weight, Dry Basis, M_d (lb/mole)
Volume of Water Vapour Attached, V_w (ft³/lb)
Stack Gas Moisture Content (%) as decimal
Stack Gas Molecular Weight, Wet Basis, M_s (lb/mole)

Laikineticity Checks

	Within Criteria	Without Criteria
Check range	29.84	29.84
Check average	34.539	34.539
	0.304	0.304
	28.26	28.26

Traverse Point	Time (min)	Starch Gels Temp, Ts (°R)	Osmotic Pressure, data P (in. H2O)	Water Press., Pm (in. Hg)	Velocity, Us (in/s)	Volume, Vm (cu. ft.)	Avg. Temp., Tm (°R)	Vol. @ Ref., Vm (cu. ft.)	(%)	
									1	2
Traverse 1	1	614	0.51	1.62	40.68	30.02	529	2,580	2,178	115.43
	2	614	0.51	1.62	40.68	30.02	529	2,350	1,942	110.04
	3	615	0.50	1.62	40.68	30.02	529	2,220	1,874	99.32
	4	615	0.50	1.62	40.68	30.02	529	2,190	1,848	97.98
	5	615	0.50	1.62	40.68	30.02	529	2,160	1,847	98.94
	6	615	0.50	1.59	40.31	30.02	529	2,140	1,829	97.54
	7	615	0.50	1.59	40.31	30.02	529	2,170	1,829	97.40
	8	616	0.50	1.59	40.31	30.02	529	2,160	1,820	96.50
	9	616	0.49	1.58	39.91	30.01	531	2,130	1,781	95.82
	10	616	0.50	1.58	40.21	30.02	531	2,140	1,783	96.47
	11	616	0.50	1.58	40.35	30.02	532	2,160	1,800	98.41
	12	616	0.50	1.58	40.31	30.02	532	2,140	1,815	97.29
	13	616	0.50	1.58	40.31	30.02	532	2,170	1,897	96.22
	14	616	0.50	1.58	40.31	30.02	533	2,140	1,795	98.13
	15	616	0.50	1.58	40.31	30.02	533	2,140	1,820	97.58
	16	616	0.50	1.58	40.35	30.02	533	2,170	1,820	97.58
	17	616	0.50	1.60	40.35	30.02	533	2,170	1,820	97.58
	18	616	0.50	1.60	40.28	30.02	533	2,190	1,760	94.17
	19	614	0.50	1.60	40.28	30.02	534	2,210	1,850	99.01
	20	614	0.50	1.60	40.28	30.02	534	2,180	1,825	97.97
	21	615	0.50	1.59	40.31	30.02	534	2,190	1,832	98.11
	22	615	0.50	1.60	40.35	30.02	534	2,160	1,807	98.76
	23	616	0.50	1.60	40.35	30.02	535	2,160	1,820	98.52
	24	616	0.50	1.60	40.28	30.02	535	2,290	1,919	102.69
	25	615	0.49	1.58	40.31	30.02	531	2,140	1,800	98.41
	26	615	0.50	1.58	40.35	30.02	532	2,160	1,815	97.29
	27	615	0.50	1.58	40.31	30.02	532	2,140	1,829	97.54
	28	616	0.50	1.58	40.31	30.02	532	2,170	1,829	97.40
	29	615	0.50	1.58	40.31	30.02	532	2,160	1,820	96.50
	30	615	0.50	1.58	40.31	30.02	532	2,140	1,803	95.82
	31	615	0.50	1.58	40.31	30.02	532	2,140	1,781	95.82
	32	615	0.50	1.58	40.31	30.02	532	2,140	1,781	95.82
	33	615	0.50	1.58	40.31	30.02	532	2,140	1,781	95.82
	34	615	0.50	1.58	40.31	30.02	532	2,140	1,781	95.82
	35	615	0.50	1.58	40.31	30.02	532	2,140	1,781	95.82
	36	615	0.50	1.58	40.31	30.02	532	2,140	1,781	95.82
	37	615	0.50	1.58	40.31	30.02	532	2,140	1,781	95.82
	38	616	0.50	1.60	40.35	30.02	533	2,170	1,820	97.58
	39	614	0.50	1.60	40.28	30.02	531	2,190	1,760	94.17
	40	614	0.50	1.60	40.28	30.02	531	2,160	1,850	99.01
	41	614	0.50	1.60	40.28	30.02	531	2,140	1,825	97.97
	42	614	0.50	1.60	40.28	30.02	531	2,170	1,825	97.54
	43	614	0.50	1.60	40.28	30.02	531	2,140	1,825	97.40
	44	614	0.50	1.60	40.28	30.02	531	2,170	1,825	97.54
	45	614	0.50	1.60	40.28	30.02	531	2,140	1,825	97.40
	46	614	0.50	1.60	40.28	30.02	531	2,170	1,825	97.54
	47	614	0.50	1.60	40.28	30.02	531	2,140	1,825	97.40
	48	614	0.50	1.60	40.28	30.02	531	2,170	1,825	97.54
	49	614	0.50	1.60	40.28	30.02	531	2,140	1,825	97.40
	50	615	0.50	1.60	40.31	30.02	532	2,160	1,832	98.11
	51	615	0.50	1.60	40.31	30.02	532	2,170	1,808	96.77
	52	615	0.50	1.60	40.31	30.02	532	2,170	1,726	92.47
	53	615	0.50	1.60	40.31	30.02	532	2,070	1,877	100.43
	54	615	0.50	1.60	40.31	30.02	532	2,250	1,726	92.40
	55	615	0.50	1.60	40.25	30.02	535	2,180	1,868	100.07
	56	615	0.50	1.60	40.25	30.02	535	2,190	1,860	98.37
	57	613	0.50	1.60	40.31	30.02	536	2,250	1,827	97.83
	58	613	0.50	1.60	40.31	30.02	536	2,190	1,910	102.30
	59	613	0.50	1.60	40.28	30.02	536	2,200	1,833	98.11
	60	614	0.50	1.60	40.28	30.02	536	2,170	1,808	96.77
	61	614	0.50	1.60	40.31	30.02	536	2,170	1,726	92.47
	62	615	0.50	1.60	40.31	30.02	536	2,070	1,877	100.43
	63	615	0.50	1.60	40.28	30.02	536	2,250	1,726	92.40
	64	614	0.50	1.60	40.31	30.02	536	2,190	1,868	100.07
	65	615	0.50	1.60	40.31	30.02	536	2,180	1,860	98.37
	66	615	0.50	1.60	40.31	30.02	536	2,190	1,910	102.30
	67	615	0.50	1.60	40.31	30.02	536	2,200	1,833	98.11
	68	615	0.50	1.60	40.31	30.02	536	2,170	1,726	92.47
	69	615	0.50	1.60	40.31	30.02	536	2,070	1,877	100.43
	70	615	0.50	1.60	40.28	30.02	536	2,250	1,726	92.40
	71	615	0.50	1.60	40.31	30.02	536	2,190	1,868	100.07
	72	615	0.50	1.60	40.31	30.02	536	2,180	1,860	98.37
	73	615	0.50	1.60	40.31	30.02	536	2,190	1,910	102.30
	74	615	0.50	1.60	40.28	30.02	536	2,200	1,833	98.11
	75	615	0.50	1.60	40.28	30.02	536	2,170	1,726	92.47
	76	615	0.50	1.60	40.28	30.02	536	2,070	1,877	100.43
	77	615	0.50	1.60	40.28	30.02	536	2,250	1,726	92.40
	78	615	0.50	1.60	40.31	30.02	536	2,190	1,868	100.07
	79	615	0.50	1.60	40.31	30.02	536	2,180	1,860	98.37
	80	615	0.50	1.60	40.31	30.02	536	2,190	1,910	102.30
	81	615	0.50	1.60	40.31	30.02	536	2,200	1,833	98.11
	82	615	0.50	1.60	40.31	30.02	536	2,170	1,726	92.47
	83	615	0.50	1.60	40.31	30.02	536	2,070	1,877	100.43
	84	615	0.50	1.60	40.28	30.02	536	2,250	1,726	92.40
	85	614	0.50	1.60	40.31	30.02	536	2,190	1,868	100.07
	86	614	0.50	1.60	40.31	30.02	536	2,180	1,860	98.37
	87	614	0.50	1.60	40.31	30.02	536	2,190	1,910	102.30
	88	615	0.50	1.60	40.31	30.02	536	2,200	1,833	98.11
	89	615	0.50	1.60	40.31	30.02	536	2,170	1,726	92.47
	90	615	0.50	1.60	40.31	30.02	536	2,070	1,877	100.43
	91	615	0.50	1.60	40.28	30.02	536	2,250	1,726	92.40
	92	615	0.50	1.60	40.31	30.02	536	2,190	1,868	100.07
	93	615	0.50	1.60	40.31	30.02	536	2,180	1,860	98.37
	94	615	0.50	1.60	40.31	30.02	536	2,190	1,910	102.30
	95	615	0.50	1.60	40.31	30.02	536	2,200	1,833	98.11
	96	615	0.50	1.60	40.31	30.02	536	2,170	1,726	92.47
	97	615	0.50	1.60	40.31	30.02	536	2,070	1,877	100.43
	98	615	0.50	1.60	40.28	30.02	536	2,250	1,726	92.40
	99	615	0.50	1.60	40.31	30.02	536	2,190	1,868	100.07
	100	615	0.50	1.60	40.31	30.02	536	2,180	1,860	98.37
	101	615	0.50	1.60	40.31	30.02	536	2,190	1,910	102.30
	102	615	0.50	1.60	40.31	30.02	536	2,200	1,833	98.11
	103	615	0.50	1.60	40.31	30.02	536	2,170	1,726	92.47
	104	615	0.50	1.60	40.31	30.02	536	2,070	1,877	100.43
	105	615	0.50	1.60	40.28	30.02	536	2,250	1,726	92.40
	106	615	0.50	1.60	40.31	30.02	536	2,190	1,868	100.07
	107	615	0.50	1.60	40.31	30.02	536	2,180	1,860	98.37
	108	615	0.50	1.60	40.31	30.02	536	2,190	1,910	102.30
	109	615	0.50	1.60	40.31	30.02	536	2,200	1,833	98.11
	110	615	0.50	1.60	40.31	30.02	536	2,170	1,726	92.47
	111	615	0.50	1.60	40.31	30.02	536	2,070	1,877	100.43
	112	615	0.50	1.60	40.31	30.02	536	2,250	1,726	92.40
	113	615	0.50	1.60	40.31	30.02	536	2,190	1,868	100.07
	114	615	0.50	1.60	40.31	30.02	536	2,180	1,860	98.37
	115	615	0.50	1.60	40.31	30.02	536	2,190	1,910	102.30
	116	615	0.50	1.60	40.31	30.02	536	2,200	1,833	98.11
	117	615	0.50	1.60	40.31	30.02	536	2,170	1,726	92.47
	118	615	0							

Combustion Gas Data for: Northern PulpClient: Northern Pulp
Job Number: 121413456Plant: Recovery Boiler
Location: Pictou, NS
Test: PM-1
Date: 15-Sep-15
Personnel: JJBTest Start: 12:00 PM
Test Finish: 12:30 PM

Time (min)	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	NOx (ppm)
0	5.2	10.5	2401	41	
5	5.3	10.4	1224	38	
10	5.3	10.4		45	
15	5.3	10.4		46	
20	5.3	10.4	2288	46	
25	5.3	10.4	2314	43	
30	5.3	10.4	1940	45	
Average:	5.3	10.4	2033	44	

Raw Data for: Northern Pulp Recovery Boiler PM

Test #2

Client: Northern Pulp

Job Number: 121413456

Plant: Recovery Boiler

Location: Picton, NS

Test: PA-3

Date: 16-Sep-15

Personnel: JHS

Test Start: 8:40 AM

Test Finish: 10:40 AM

Barometric Pressure, Psbar [in. Hg]

Stack Static Pressure, Psstatic [in. H2O]

Ambient Temp. [°F]

H2O Volume Collected, Vw [mL]

Total # Sampling Points

Sampling Time per point, [min]

Readings Taken Every — mins

Regulatory Agency

Traverse Point

Time

Stack Gas Temp, Ts [°F]

S-type Pitot

delta P

[in. H2O]

Gas Meter

Volume

[cu. ft.]

Orifice

dia. H

[in. H2O]

Inlet

Temp [°F]

Outlet

Temp [°F]

Stack

Gas

Flow

Rate [ft/min]

	Impinger	Final Weight	Tare Weight	Weight of
	Centrif.	[g]	[g]	Moisture [g]
1	100 mL H2O	867.4	723.8	263.6
2	100 mL H2O	1023.7	731.0	292.7
3	Blank	864.7	625.1	239.6
4	2000 Scales	922.9	892.2	31.7
				Total Weight Gain [g]
				827.6
				Moisture Volume [mL]
				827.6

Particulates Collected from Filter (mg):	12.1
Particulates Collected from Probe Wash (mg):	1.5
Particulates Collected from Impinger Wash (mg):	8.1
Total Particulates Collected (mg):	13.5

Stack Diameter, [in.]	13.6
Stack Area, [sq. in.]	10.4
Probe Length, [in.]	4
Nozzle Diameter, [in.]	0.305
Pilot Coefficient, (Cp)	0.756
Gamma, meter constant	0.829
Port Length [in.]	4

Traverse 1	1	2.5	155	0.50	1.51	390.120	66	63
	5	5	155	0.50	1.51	400.510	66	63
	2	7.5	156	0.50	1.51	602.650	67	64
	10	10	156	0.50	1.51	604.340	67	64
	12.5	12.5	156	0.48	1.51	667.810	69	66
	15	15	156	0.48	1.51	669.140	69	66
	17.5	17.5	156	0.48	1.51	611.260	70	67
	20	20	156	0.48	1.51	612.350	70	67
	22.5	25	155	0.48	1.51	613.520	72	67
	27.5	27.5	155	0.48	1.51	617.600	72	67
	30	30	154	0.50	1.56	619.770	74	68
	32.5	32.5	154	0.50	1.59	621.970	74	68
	35	37.5	153	0.50	1.60	624.170	75	68
	40	40	153	0.50	1.60	612.350	75	69
	42.5	42.5	153	0.50	1.60	630.750	77	71
	45	45	153	0.50	1.60	632.940	77	71
	47.5	47.5	151	0.51	1.61	631.180	77	72
	50	50	151	0.51	1.61	637.790	80	72
	52.5	52.5	151	0.51	1.61	639.600	80	72
	55	55	151	0.51	1.61	641.420	81	73
	57.5	57.5	151	0.51	1.61	644.030	81	73
	60	60	151	0.51	1.61	646.230	81	73
						648.420	81	74

Traverse 2	1	62.5	155	0.51	1.61	650.560	81	74
	65	65	154	0.51	1.61	652.860	81	75
	67.5	70	156	0.51	1.61	655.070	81	75
	72.5	72.5	157	0.51	1.61	657.280	82	76
	75	75	155	0.51	1.61	659.480	82	75
	77.5	77.5	155	0.51	1.63	661.670	82	76
	80	80	155	0.51	1.63	663.870	82	76
	82.5	82.5	156	0.51	1.63	665.250	82	76
	85	85	157	0.51	1.64	668.260	82	76
	87.5	87.5	156	0.51	1.65	670.380	82	76
	90	90	156	0.51	1.65	672.500	82	76
	92.5	92.5	157	0.51	1.64	674.620	82	76
	95	95	154	0.51	1.63	676.830	82	76
	97.5	97.5	155	0.51	1.63	679.100	82	76
	100	100	155	0.51	1.63	681.110	82	77
	102.5	102.5	155	0.51	1.63	683.330	82	77
	105	105	154	0.51	1.63	685.750	82	77
	107.5	107.5	154	0.51	1.63	688.010	84	77
	110	110	154	0.51	1.66	690.250	84	77
	112.5	112.5	154	0.51	1.66	692.490	84	77
	115	115	155	0.51	1.65	694.710	82	77
	117.5	117.5	154	0.51	1.66	696.950	82	77
	120	120	154	0.51	1.66	699.300	82	77

Calculations for: Northern Pulp Recovery Boiler Pw
Test #2

Client: Northern Pulp

Job Number: 12141456

Plant: Recovery Boiler

Location: Picton, NS

Test: Pw-3

Date: 18-Sep-15

Personnel: J.B.

Calculated Parameters

Stack Gas Pressure, P_w [in.Hg]
 Stack Gas Molecular Weight, Dry Basis, M_w [(lb/lb-mole)]
 Volume of Water Vapour Collected, V_w [cu.ft.]
 Stack Gas Moisture Content (% as decimal)
 Stack Gas Molecular Weight, Wet Basis, M_w [(lb/lb-mole)]

20.94	20.88	39.775	0.312	26.18
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Isokinetic Checks

Check range
 Within Criteria
 Within Criteria

Traverse Point	Time (min)	Stack Gas Temp, T _s (R)	S-type Pitot, delta p (in.H2O)	Office dH (in.H2O)	Stack Gas Velocity, Us (ft/s)	Meter Press., Pm [in.Hg]	Avg. Temp., Tm (R)	Gas Meter Vm (ft/s.)	Vol. @ Ref., Vm ^c [cu. ft.]	Volume, Vm (cu. ft.)	Gas Meter Vm (cu. ft.)	Isokinetics [%]
Traverse 1												
1	2.5	615	0.50	1.58	40.38	30.02	526	2.150	1.827	98.73	100.56	
	5	615	0.50	1.58	40.39	30.02	526	2.190	1.861			
	7.5	616	0.50	1.58	40.41	30.02	527	2.180	1.849			
	10	616	0.50	1.58	40.41	30.07	527	2.170	1.841			
	12.5	616	0.48	1.51	39.80	30.01	526	2.150	1.820			
	15	616	0.48	1.51	39.80	30.01	526	2.130	1.803			
	17.5	616	0.48	1.51	39.80	30.01	526	2.120	1.791			
	20	616	0.48	1.55	39.80	30.01	526	2.100	1.774			
	22.5	616	0.48	1.55	39.80	30.01	526	2.160	1.822			
	25	615	0.48	1.55	39.57	30.01	520	2.090	1.754			
	27.5	615	0.49	1.58	39.57	30.01	521	2.170	1.825			
	30	614	0.50	1.58	40.35	30.02	531	2.200	1.850			
	32.5	614	0.50	1.60	40.35	30.02	532	2.200	1.849			
	35	613	0.50	1.60	40.32	30.02	532	1.830	1.830			
	37.5	613	0.50	1.60	40.32	30.02	534	2.180	1.842			
	40	613	0.50	1.60	40.32	30.02	534	2.200	1.840			
	42.5	613	0.50	1.60	40.22	30.02	535	2.190	1.828			
	45	613	0.50	1.60	40.22	30.02	536	2.240	1.868			
	47.5	611	0.51	1.64	40.85	30.02	536	2.210	1.842			
	50	611	0.51	1.64	40.85	30.02	536	2.210	1.842			
	52.5	613	0.51	1.64	40.72	30.02	537	2.220	1.847			
	55	613	0.51	1.64	40.72	30.02	537	2.210	1.839			
	57.5	613	0.51	1.64	40.72	30.02	537	2.130	1.830			
	60	613	0.51	1.64	40.72	30.02	538	2.180	1.820			
Traverse 2												
1	62.5	615	0.51	1.64	40.78	30.02	538	2.240	1.861			
	65	614	0.51	1.64	40.75	28.95	538	2.200	1.822			
	67.5	615	0.51	1.64	40.82	30.02	538	2.210	1.835			
	70	616	0.51	1.64	40.82	30.02	539	2.210	1.833			
	72.5	617	0.51	1.64	40.85	30.02	539	2.200	1.825			
	75	615	0.51	1.65	40.78	30.02	539	2.190	1.817			
	77.5	615	0.51	1.65	40.78	30.02	539	2.200	1.822			
	80	615	0.51	1.65	40.78	30.02	539	2.180	1.972			
	82.5	616	0.51	1.65	40.82	30.02	539	2.10	1.868			
	85	617	0.51	1.64	40.85	30.02	539	2.120	1.757			
	87.5	616	0.51	1.65	40.82	30.02	539	2.170	1.794			
	90	616	0.51	1.65	40.82	30.02	539	2.130	1.785			
	92.5	617	0.51	1.64	40.85	30.02	539	2.120	1.823			
	95	614	0.51	1.65	40.75	30.02	540	2.220	1.838			
	97.5	615	0.51	1.65	40.78	30.02	540	2.210	1.828			
	100	615	0.51	1.65	40.78	30.02	540	2.220	1.838			
	102.5	615	0.51	1.65	40.78	30.02	540	2.220	1.836			
	105	614	0.51	1.65	40.75	30.02	541	2.260	1.868			
	107.5	614	0.51	1.65	40.75	30.02	541	2.240	1.853			
	110	614	0.51	1.65	40.75	30.02	541	2.240	1.851			
	112.5	614	0.51	1.66	40.75	30.02	540	2.220	1.838			
	115	615	0.51	1.65	40.78	30.02	540	2.240	1.853			
	117.5	614	0.51	1.65	40.75	30.02	540	2.350	1.944			
	120	614	0.51	1.65	40.75	30.02	540	2.080	1.730			
Total	120	615	Average	Average	Average	Average	535	Total	Total	Average	Average	Average
			0.50	1.60	40.50	30.02		105.220	67.785	98.44		

Combustion Gas Data for: Northern PulpClient: Northern Pulp
Job Number: 121413456

Plant: Recovery Boiler

Location: Pictou, NS

Test: PM-3

Date: 16-Sep-15

Personnel: JJB

Test Start: 9:00 AM
Test Finish: 9:30 AM

	Time (min)	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	NO _x (ppm)
0	5.4	10.4	17.5	57		
5	5.5	10.3	22.2	58		
10	5.5	10.3	23.8	58		
15	5.4	10.4	14.4	60		
20	5.4	10.4	32.1	60		
25	5.6	10.3	54.5	60		
30	5.4	10.4	48.9	61		
Average:	5.5	10.4	30.5	59		

Calculations for: Northern Pulp Recovery Boiler PW
Test #3

Client: Northern Pulp
Job Number: 121413458

Plant: Recovery Boiler
Location: Pictou, NS
Test: PW-4
Date: 10-Sep-15
Personnel: JBL/BC

Calculated Parameters

Stack Gas Pressure, P_s [in.Hg]
Stack Gas Molecular Weight, Dry Basis, M_d [lb/mole]
Volume of Water Vapour Collected, V_w [cu.ft.]
Stack Gas Moisture Content (%) as defined
Stack Gas Molecular Weight, Wet Basis, M_w [lb/mole]

Isokineticity Checks

	Traverse Point	Time (min)	Stack Gas Temp, T_s (R)	S-type Pipe, delta P (in. Hg)	Orifice delta H (in. Hg)	Stack Gas Velocity, V_s (ft/s)	Meter Press., Pm (in. Hg)	Avg. Temp., T _m (R)	Gas Meter Volume, V _m [cu. ft.]	Vol. @ Ref., V _m [cu. ft.]	Isokinetics %
	Traverse 1	1	2.5	615	0.50	1.61	40.30	30.02	530	2,200	1,015
		5	615	0.50	1.61	40.30	40.30	30.02	530	2,230	1,060
		7.5	615	0.50	1.61	40.30	40.70	30.02	530	2,240	1,083
		10	615	0.51	1.64	40.64	40.64	30.02	530	2,230	1,056
		12.5	613	0.51	1.64	40.67	40.67	30.02	530	2,230	1,058
		15	614	0.51	1.64	40.60	40.60	30.02	530	2,220	1,050
		17.5	612	0.51	1.61	40.20	40.20	30.02	530	2,230	1,060
		20	612	0.50	1.61	40.20	40.20	30.02	530	2,230	1,060
		22.5	615	0.50	1.61	40.20	40.20	30.02	530	2,230	1,062
		25	615	0.50	1.61	40.20	40.20	30.02	530	2,230	1,060
		27.5	615	0.50	1.61	40.20	40.20	30.02	530	2,230	1,062
		30	615	0.50	1.61	40.20	40.20	30.02	530	2,230	1,060
		32.5	615	0.50	1.61	40.20	40.20	30.02	530	2,230	1,062
		35	615	0.50	1.61	40.20	40.20	30.02	530	2,230	1,060
		37.5	615	0.50	1.61	40.20	40.20	30.02	530	2,230	1,062
		40	615	0.50	1.61	40.20	40.20	30.02	530	2,230	1,060
		42.5	614	0.50	1.61	40.27	40.27	30.02	537	2,230	1,055
		45	614	0.50	1.61	40.27	40.27	30.02	537	2,230	1,046
		47.5	615	0.50	1.61	40.20	40.20	30.02	530	2,230	1,050
		50	615	0.50	1.61	40.20	40.20	30.02	530	2,230	1,042
		52.5	615	0.50	1.61	40.20	40.20	30.02	530	2,230	1,023
		55	615	0.50	1.61	40.20	40.20	30.02	537	2,190	97.54
		57.5	615	0.50	1.61	40.20	40.20	30.02	537	2,180	97.54
		60	615	0.50	1.61	40.20	40.20	30.02	537	2,180	98.33
		62.5	615	0.50	1.61	40.20	40.20	30.02	537	2,180	98.33
		65	615	0.50	1.61	40.20	40.20	30.02	537	2,180	98.14
		67.5	615	0.49	1.59	39.90	39.90	30.02	540	2,230	98.70
		70	615	0.49	1.59	39.90	39.90	30.02	540	2,230	98.45
		72.5	614	0.49	1.59	39.86	39.86	30.02	540	2,230	98.95
		75	614	0.49	1.59	39.90	39.90	30.02	540	2,230	98.77
		77.5	615	0.49	1.59	39.86	39.86	30.02	540	2,230	98.67
		80	614	0.49	1.59	39.86	39.86	30.02	540	2,230	98.32
		82.5	614	0.49	1.59	39.82	39.82	30.02	540	2,230	98.44
		85	614	0.49	1.59	39.82	39.82	30.02	540	2,240	98.51
		87.5	614	0.49	1.59	39.82	39.82	30.02	541	2,250	98.47
		90	615	0.49	1.59	39.86	39.86	30.02	541	2,250	98.47
		92.5	614	0.49	1.59	39.82	39.82	30.02	541	2,250	98.51
		95	614	0.49	1.59	39.86	39.86	30.02	540	2,250	98.51
		97.5	614	0.49	1.59	39.86	39.86	30.02	540	2,250	98.51
		100	614	0.49	1.59	39.86	39.86	30.02	540	2,250	98.51
		102.5	614	0.49	1.59	39.86	39.86	30.02	540	2,250	98.51
		105	613	0.49	1.59	39.86	39.86	30.02	540	2,250	98.47
		107.5	615	0.49	1.59	39.86	39.86	30.02	540	2,250	98.53
		110	613	0.49	1.59	39.86	39.86	30.02	540	2,250	98.53
		112.5	613	0.49	1.59	39.86	39.86	30.02	540	2,250	98.79
		115	614	0.49	1.59	39.86	39.86	30.02	539	2,250	100.67
		117.5	614	0.49	1.59	39.86	39.86	30.02	539	2,190	97.96
		120	614	0.49	1.59	39.86	39.86	30.02	538	2,240	100.41
		122	614	0.50	1.60	40.13	40.13	30.02	535	107.320	Average
	Total	120	614	0.50	1.60	40.13	40.13	30.02	535	107.320	Total
										88.803	Average

Combustion Gas Data for:

Northern Pulp

Client: Northern Pulp
Job Number: 121413456Plant: Recovery Boiler
Location: Picton, NS
Test: PM-4
Date: 16-Sep-15
Personnel: JBL/CTest Start:
Test Finish:

	Time (min)	O ₂ (%)	CO ₂ (%)	CO (ppm)	SO ₂ (ppm)	NO _x (ppm)
	0	5.2	10.5	1591	53	
	5	5.2	10.5	1230	52	
	10	5.2	10.5	907	53	
	15	5.2	10.5	201	55	
	20	5.2	10.5	197	56	
	25	5.3	10.4	123	55	
	30	5.3	10.4	139	55	
Average:		5.2	10.5	827	54	

DATA ENTRY

Northern Pulp
Pictou, NS
Fuel: Fuel oil
Operating Conditions: normal
Emission Control Equipment: precipitator
Stack Height from Grade: 69 m
Stack Diameter: 3.51 m

Reference Temperature, Tref (F):	77
	(K): 298
Reference Pressure, Pref (in.Hg):	29.92
	(Bar): 1.0

Parameter	Symbol	Units	Test 1	Test 2	Test 3	Average
Test ID	-	-	PM-1	PM-3	PM-4	-
Date	-	-	15-Sep-15	16-Sep-15	16-Sep-15	n/a
Start Time	-	-	11:15 AM	8:40 AM	12:30 PM	n/a
End Time	-	-	1:30 PM	10:40 AM	2:30 PM	n/a
Total Sampling Time	-	min	120	120	120	120
Stack Diameter	D	in.	138	138	138	138
Average Stack Gas Temperature	Ts	F	155	155	154	155
Average Dry Gas Meter Temperature	Tm	F	74	75	78	76
Barometric Pressure	Pbar	in.Hg	29.90	29.90	29.90	29.90
Stack Static Pressure	Pstatic	in.H2O	1.10	1.10	1.10	1.10
Average Pressure Drop (Head)	dP	in.H2O	0.50	0.50	0.50	0.50
Average deltaH Orifice	dH	in.H2O	1.60	1.60	1.60	1.60
Average Meter Temperature	Tm	F	74	75	78	76
Gas Sample Volume	Vm	cu.ft	105.29	105.22	107.02	105.84
Average Isokinetics	i	%	98	98	99	99
Nozzle Diameter	Dn	in.	0.305	0.305	0.305	0.305
Pivot Coefficient	Cp	-	0.756	0.756	0.756	0.756
Gamma, meter constant	y	-	0.829	0.829	0.829	0.829
Reference Temperature	Tref	R	537	537	537	537
Reference Pressure	Pref	in.Hg	29.92	29.92	29.92	29.92
Stack Gas Oxygen Content	Co2	%	5.3	5.5	5.2	5.3
Stack Gas Carbon Dioxide Content	Cco2	%	10.4	10.4	10.5	10.4
Stack Gas Nitrogen Content	Cn2	%	84.3	84.2	84.3	84.3
Stack Gas Sulphur Dioxide Content	Cso2	ppm	43.7	59.1	54.1	52.3
Stack Gas Nitrogen Oxides Content	Cnox	ppm	0.0	0.0	0.0	0.0
Stack Gas Carbon Monoxide Content	Cco	ppm	2033.4	304.6	626.9	988.3
Volume of Water Collected	Vw	mL	802.9	827.6	805.6	812.0
Particulate Collected from Filter	-	mg	13.7	12.1	12.9	12.9
Particulate Collected from Probe Wash	-	mg	6.1	1.5	0.1	2.6
Particulate Collected from Impinger Wash	-	mg	8.04	8.05	72.92	29.67
Total Particulate Collected (excluding impingers)	Mp	mg	19.8	13.51	12.97	15.43

Legend:

- F - degrees Fahrenheit
- K - degrees Kelvin
- Bar - bars
- in.Hg - inches of mercury
- in. - inches

in.H2O - inches of water
 cu.ft - cubic feet
 R - degrees Rankin
 NOx - as NO2

CALCULATIONS

Northern Pulp
 Pictou, NS
 Fuel: Fuel oil
 Operating Conditions: normal
 Emission Control Equipment: precipitator
 Stack Height from Grade: 69 m
 Stack Diameter: 3.51 m

Variable	Symbol	Units	Calculation	Test 1	Test 2	Test 3	Average
Stack Area	As	sq.ft sq.m	$As = \pi \times ((D/12)^2 / 4)$ $As (\text{sq.m}) = As (\text{sq.ft}) \times 0.0929$	103.87 9.65	103.87 9.65	103.87 9.65	103.87 9.65
Barometric Pressure Stack Static Pressure Avg. Stack Temperature Avg. Meter Temperature Nozzle Diameter	Pbar Pstatic Ts Tm Dn	in.Hg in.Hg R R mm	$Pbar (\text{kPa}) = Pbar (\text{in.Hg}) \times 3.386$ $Pstatic (\text{kPa}) = Pstatic (\text{in.Hg}) \times 0.349$ $Ts (R) = Ts (F) + 460$ $Tm (R) = Tm (F) + 460$ $Dn (\text{mm}) = Dn (\text{in.}) \times 25.4$	101.2 0.27 615 534 8	101.2 0.27 615 535 8	101.2 0.27 614 538 8	101.2 0.27 615 535.9 7.7
Gas Meter Pressure Sample Volume at Ref Cond Volume of Water Vapour Water Fraction	Pm Vm Vw Bw	in.Hg cu.ft cu.m cu.ft	$Pm = Pbar + (\Delta H / 13.6)$ $Vm = Tref/Prof \times (Vm + Pm \times z) / Tm$ $Vm (\text{cu.m}) = 0.01332 \times Vm (\text{cu.ft})$ $Vw = 0.0480 \times Vw$ $Bw = Vw / (Vm + Vw)$	30.02 88.06 2.49 38.54 0.304	30.02 87.77 2.49 39.72 0.312	30.02 88.81 2.52 38.67 0.303	30.02 88.2 2.50 38.98 0.3
Molecular Weight, Dry Molecular Weight, Wet	Md Mw	lb/lbmol lb/lbmol	$Md = 0.44 (\text{Co2}) + 0.32 (\text{Ca2}) + 0.28 (\text{Ca1})$ $Mw = Md (1 - Bw) + (18 \times Bw)$	29.88 26.26	29.88 26.18	29.88 26.28	29.9 26.2
Stack Pressure Stack Gas Velocity Actual Stack Gas Flow Rate Dry Stack Gas Flow Rate	Ps Us Q Qs	in.Hg ft/s m/s scfm scfm	$Ps = Pbar + (Pstatic / 13.6)$ $Us = 0.513 \times C_p \times ((\Delta P + Ts/(Ps \times Mw))^{0.5}$ $Us (\text{m/s}) = 0.3048 \times Us (\text{ft/s})$ $Q = 60 \times Us \times As$ $Qs = Q \times (1 - Bw) \times (Tref/Prof) \times (Ps/\text{Prof})$ $Qs (\text{scfm}) = 0.000472 \times Qs (\text{scfm})$	29.98 40.34 12.30 251,404 153,063 72.25	29.98 40.50 12.34 252,407 152,124 71.80	29.98 40.13 12.23 250,073 152,602 72.03	29.98 40.3 12.3 251,295 152,596 72.0
Sulphur Dioxide - SO2 SO2 Measured Concentration Uncorrected @ Ref Cond SO2 Emission Rate	Co1 Co1 ERm1	ppm mg/Rem g/s kg/hr	Measurement from Flue Gas Analyse $Co1 (\text{mg/Rem}) = Co1 (\text{ppm}) \times 2.62$ $ERm1 = Co1/2000 \times Qo$ $ERm1 (\text{kg/hr}) = 3.6 \times ERm1 (\text{g/s})$	43.71 114.53 8.27 29.79	59.14 154.95 11.13 40.05	54.14 141.85 10.22 36.78	52.33 137.11 9.87 35.54
SO2 Concentration Corrected to 11% O2 Corrected to 3% O2 Corrected to 12% CO2	Co1 Co1 Co1	mg/Rem mg/Rem mg/Rem	$Co1 (11\% \text{O}_2) = Co1 (\text{mg/Rem}) \times (20.9-11) / (20.9-\text{Co2})$ $Co1 (3\% \text{O}_2) = Co1 (\text{mg/Rem}) \times (20.9-3) / (20.9-\text{Co2})$ $Co1 (12\% \text{CO}_2) = Co1 (\text{mg/Rem}) \times (12/\text{Co2})$	72.62 131.30 131.97	99.34 179.61 179.53	89.61 162.03 162.56	87.19 157.64 158.02
Nitrogen Oxides - NOx NOx Measured Concentration Uncorrected @ Ref Cond NOx Emission Rate	Cox Cox ERmax	ppm mg/Rem g/s kg/hr	Measurement from Flue Gas Analyse $Cox (\text{mg/Rem}) = Cox (\text{ppm}) \times 1.982$ $ERmax = Cox/1000 \times Qo$ $ERmax (\text{kg/hr}) = 3.6 \times ERmax (\text{g/s})$				
NOx Concentration Corrected to 11% O2 Corrected to 3% O2 Corrected to 12% CO2	Cox Cox Cox	mg/Rem mg/Rem mg/Rem	$Cox (11\% \text{O}_2) = Cox (\text{mg/Rem}) \times (20.9-11) / (20.9-\text{Co2})$ $Cox (3\% \text{O}_2) = Cox (\text{mg/Rem}) \times (20.9-3) / (20.9-\text{Co2})$ $Cox (12\% \text{CO}_2) = Cox (\text{mg/Rem}) \times (12/\text{Co2})$				
Carbon Monoxide - CO CO Measured Concentration Uncorrected @ Ref Cond CO Emission Rate	Coo Coo EReo	ppm mg/Rem g/s kg/hr	Measurement from Flue Gas Analyse $Coo (\text{mg/Rem}) = Coo (\text{ppm}) \times 1.148$ $EReo = Coo/1000 \times Qo$ $EReo (\text{kg/hr}) = 3.6 \times EReo (\text{g/s})$	2033.40 2328.24 168.21 605.54	304.57 348.73 25.04 90.14	626.86 717.75 51.70 186.11	988.28 1131.58 81.65 293.93
CO Concentration Corrected to 11% O2 Corrected to 3% O2 Corrected to 12% CO2	Coo Coo Coo	mg/Rem mg/Rem mg/Rem	$Coo (11\% \text{O}_2) = Coo (\text{mg/Rem}) \times (20.9-11) / (20.9-\text{Co2})$ $Coo (3\% \text{O}_2) = Coo (\text{mg/Rem}) \times (20.9-3) / (20.9-\text{Co2})$ $Coo (12\% \text{CO}_2) = Coo (\text{mg/Rem}) \times (12/\text{Co2})$	1476.19 2669.07 2682.75	223.56 404.22 404.05	453.42 819.82 822.53	717.72 1297.70 1303.11
Particulate Concentration Particulate Emission Rate	Ca ERp	mg/Rem g/s kg/hr	$Ca = Mp / Vm$ $ERp = Ca/1000 \times Qo$ $ERp (\text{kg/hr}) = 3.6 \times ERp (\text{g/s})$	7.94 0.57 2.07	5.44 0.39 1.41	5.16 0.37 1.34	6.18 0.45 1.60
Particulate Concentration Corrected to 11% O2 Corrected to 3% O2 Corrected to 12% CO2	Ca Ca Ca	mg/Rem mg/Rem mg/Rem	$Ca (11\% \text{O}_2) = Ca \times (20.9-11) / (20.9-\text{Co2})$ $Ca (3\% \text{O}_2) = Ca \times (20.9-3) / (20.9-\text{Co2})$ $Ca (12\% \text{CO}_2) = Ca \times (12/\text{Co2})$	5.04 6.56 9.15	3.49 4.54 6.30	3.26 4.25 5.91	3.93 5.12 7.12

Legend:
 sq.ft - square feet
 sq.m - square metres
 PI - 3.142
 R - degree Rankin
 ppm - parts per million

in.Hg - inches of mercury
 cu.ft - cubic feet
 cu.m - cubic metres
 Ref Cond - reference temperature and pressure (25 C and 101.3 kPa)
 Rems - dry reference cubic metres per second
 Rcfm - dry reference cubic feet per minute

mg/Rem - milligrams per dry reference cubic metre
 g/s - grams per second
 NOx - as NO2
 acfm - actual cubic feet per minute

OFFICIAL STACK TESTING RESULTS

Northern Pulp

Pictou, NS

Fuel: Fuel oil

Operating Conditions: normal

Emission Control Equipment: precipitator

Stack Height from Grade: 69 m

Stack Diameter: 3.51 m

Parameter	Test 1	Test 2	Test 3	Average	NSENV Limits
Test ID Test Date	PM-1 15-Sep-15	PM-3 16-Sep-15	PM-4 16-Sep-15	- -	- -
Stack Gas Temperature (C) Moisture Content (%) Velocity (m/s) Volumetric Flow (Rcms)	68.2 30.4 12.3 72.2	68.1 31.2 12.3 71.8	68.0 30.3 12.2 72.0	68.1 30.6 12.3 72.0	- - - -
Oxygen - O2 (%) Carbon Dioxide - CO2 (%)	5.29 10.41	5.46 10.36	5.23 10.47	5.32 10.41	- -
Sulphur Dioxide - SO2 SO2 Measured Concentration (ppm) Uncorrected at Ref Cond (mg/Rcm) Emission Rate (kg/hr)	43.71 72.62 29.79	59.14 99.34 40.05	54.14 89.61 36.78	52.33 87.19 35.54	- - -
Nitrogen Oxides - NOx NOx Measured Concentration (ppm) Uncorrected at Ref Cond (mg/Rcm) Emission Rate (kg/hr)					- - -
Carbon Monoxide - CO CO Measured Concentration (ppm) Uncorrected at Ref Cond (mg/Rcm) Emission Rate (kg/hr)	2033.4 2328.2 605.54	304.6 348.7 90.14	626.9 717.8 186.11	988.3 1131.6 293.93	- - -
Particulate Matter - PM Particulate Concentration (mg/Rcm) Concentration, Corrected to 11% O ₂ (mg/Rcm) Particulate Emission Rate (kg/hr)	7.9 5.04 2.07	5.44 3.49 1.41	5.16 3.26 1.34	6.18 3.93 1.60	- 77 -

Legend: C - degrees Celsius

m/s - metres per second

Rcms - dry reference cubic metres per second

ppm - parts per million

Ref Cond - reference temperature and pressure (25 C and 101.3 kPa)

mg/Rcm - milligrams per dry reference cubic metre

NOx - as NO₂

ND - non-detectable

Particulate Recoveries: Impinger Catch, Probe Wash, Filter Catch

Client: Northern Pulp
 Facility: Recovery Boiler
 Location: Pictou, NS
 Job Number: 124113456

IMPINGER CATCH

Container ID	Batcher Pre Weights (g)			Sample ID	Recoveries			Batcher Post Weights (g)		
	Analyzed by Date		Air + Sample + Residue		Batcher Weigh.	Total Force (N)	Batcher Post Weight (g)	Date Analyzed by	Uncorrected Particulate Weight (g)	Corrected Particulate Weight (g)
	Trial 1	Trial 2	Average		(g)	(g)		Trial 1	Trial 2	Average
X1	105.9279	105.9290	105.9285	PM-1	381.1	802.9	312	105.9285	105.9290	105.9287
X2	111.9272	111.9270	111.9271	PM-2	1294.7	3766.9	827.6	111.9250	111.9260	111.9250
M3	112.8624	112.8624	112.8624	PM-3	1352.4	3783.3	805.6	112.8702	112.8707	112.8700
V1	111.1023	111.1020	111.1022	W6	660.0	371.6	268.2	268.2	111.1041	111.1044
L3	111.1023	111.1020	111.1022						0.00227	0.00006

PROBE WASH

Container ID	Batcher Pre Weights (g)			Sample ID	Recoveries			Batcher Post Weights (g)				
	Analyzed by Date		Air + Acetone		Tare	Recovered Acetone	Residue	Total Acetone	Date Analyzed by	Uncorrected Particulate Weight (g)	Corrected Particulate Weight (g)	
	Trial 1	Trial 2	Average		(g)	(g)	(g)	(g)		Trial 1	Trial 2	Average
I4	117.1338	117.1340	117.1339	PM-1	379.0	300.5	20.5	77.3	117.1326	117.1329	117.1326	
I3	108.8548	108.8546	108.8548	PM-2	354.2	300.9	44.3	49.3	109.8584	109.8589	109.8586	
D4	108.8760	108.8757	108.8759	PM-3	374.4	306.8	65.6	84	108.8793	108.8798	108.8796	
B1	111.6523	111.6520	111.6522	AB	340.9	295.1	54.8	54.8	111.6547	111.6549	111.6548	

Density of Acetone: 0.7850 g/ml

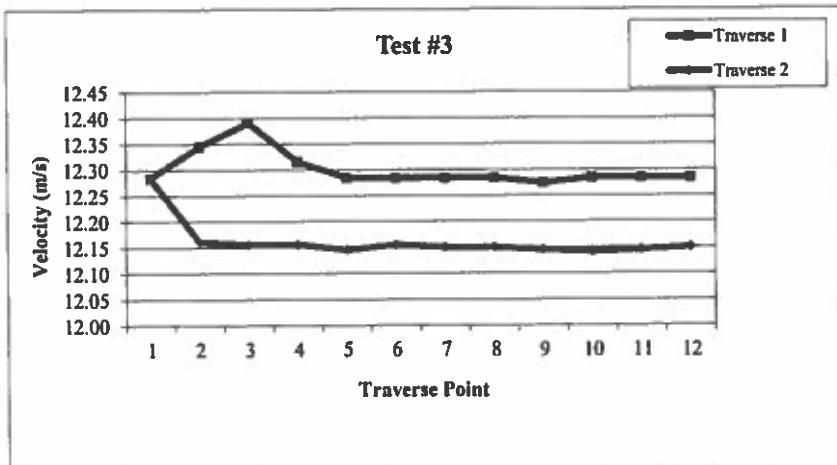
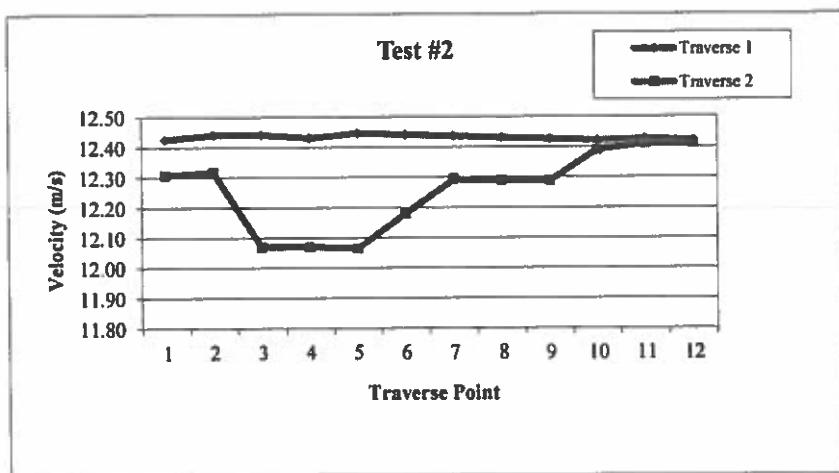
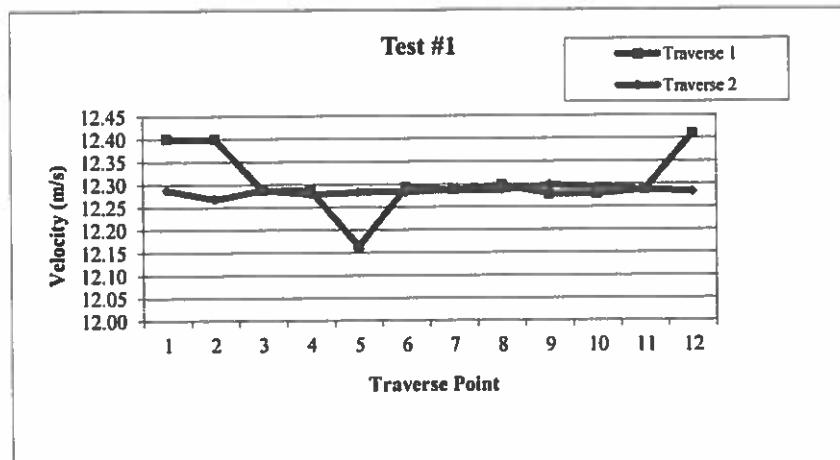
FILTER CATCH

Filter ID	Pre Weights (g)			Sample ID	Post Weights (g)			Particulate Weight From Filter (g)		
	Analyzed by Date		Average		Tare	Recovered	Total Acetone	Date Analyzed by	Uncorrected	Corrected
	Trial 1	Trial 2	Average		(g)	(g)	(g)			
0012-16	0.3702	0.3705	0.3704	PM-1	0.3641	0.3641	0.3641	0.0137	0.0137	0.0137
0012-11	0.3703	0.3701	0.3702	PM-2	0.3623	0.3622	0.3623	0.0121	0.0121	0.0121
0012-12	0.3693	0.3690	0.3692	PM-3	0.3618	0.3622	0.3620	0.0129	0.0129	0.0129

Northern Pulp
Recovery Boiler

121413456

Stack Gas Velocity Profiles
Pictou, NS



Project: 121413456

Test: PM 1 (Power Boiler)

Date: Oct 14/15

Analyst: CAC

Hand Calculations

Page 1 of 6

revised May 29,

Absolute stack gas pressure (Ps) in in.Hg is:

$$Ps = P_{bar} + \frac{P_{static} \text{ in.H}_2\text{O}}{13.6 \text{ in.H}_2\text{O/in.Hg}}$$

$$Ps = \frac{30.00}{13.6} + \frac{0.18}{13.6}$$

$$Ps = \underline{30.00} \text{ in.Hg}$$

The molecular weight of the stack gas on a dry basis (Md) in lb/lb-mole is:

$$Md = 0.44(\%CO_2) + 0.32(\%O_2) + 0.28[(\%N_2) + (\%CO)] + 0.40\%Ar$$

$$Md = 0.44 \times \underline{5.8} + 0.32 \times \underline{12.8} + 0.28 \left(\frac{\underline{81.3}}{0.40} + \frac{\cancel{+} \cancel{+}}{\cancel{+} \cancel{+}} \right)$$

$$Md = \underline{2.55} + \underline{4.16} + \underline{22.76} + \cancel{+}$$

$$Md = \underline{29.41} \text{ lb/lb-mole}$$

The volume of water vapour collected at reference conditions (Vwc) in ft³ is:

$$Vwc = 0.0480 \text{ ft}^3/\text{mL} \times \text{volume of moisture collected mL.}$$

$$Vwc = 0.0480 \times \underline{222.3}$$

$$Vwc = \underline{10.67} \text{ ft}^3$$

The average \bar{H} orifice in in.H₂O is:

$$\bar{H}_{\text{orifice avg.}} = \frac{\sum H_{\text{orifice}}}{\# \text{ points}}$$

$$\bar{H}_{\text{orifice avg.}} = \frac{20.15}{48}$$

$$\bar{H}_{\text{orifice avg.}} = 0.42 \text{ in.H}_2\text{O}$$

The pressure at the gas meter (P_m) in in.Hg is:

$$P_m = P_{\text{bar}} + \frac{\bar{H}_{\text{orifice avg. in.H}_2\text{O}}}{13.6 \text{ in.H}_2\text{O/in.Hg}}$$

$$P_m = 30.00 + \frac{0.42}{13.6}$$

$$P_m = 30.00 + 0.031$$

$$P_m = 30.03 \text{ in.Hg}$$

The temperature of the gas meter (T_m) in °R is:

$$T_m = \frac{\sum \text{meter temp. } ^\circ\text{F}}{\# \text{ points}} + 460$$

$$T_m = \frac{6398}{72} + 460$$

$$T_m = 66.64 + 460$$

$$T_m = 526.64 \text{ } ^\circ\text{R}$$

The total volume of gas metered (V_m) in ft³ is:

$$V_m = V_f \text{ ft}^3 - V_i \text{ ft}^3$$

$$V_m = \underline{866.42} - \underline{809.37}$$

$$V_m = \underline{57.05} \text{ ft}^3$$

The dry gas volume at reference conditions (V_{mc}) in ft³ is:

$$V_{mc} = \frac{T_{ref} \text{ } ^\circ R}{P_{ref} \text{ in.Hg}} \times \frac{P_m \text{ in.Hg} \times V_m \text{ ft}^3 \times ?}{T_m \text{ } ^\circ R}$$

$$V_{mc} = \frac{\underline{53.4}}{\underline{29.92}} \times \frac{\underline{30.03}}{} \times \frac{\underline{57.05}}{\underline{586.64}} \times \underline{0.821}$$

$$V_{mc} = \underline{48.40} \text{ ft}^3 \times 1 \text{ m}^3 / 35.31 \text{ ft}^3 = \underline{1.37} \text{ m}^3$$

The stack gas moisture content, i.e. the proportion by volume of water vapour in the gas stream (B_{wo}) is:

$$B_{wo} = \frac{V_{wc} \text{ ft}^3}{V_{wc} \text{ ft}^3 + V_{mc} \text{ ft}^3}$$

$$B_{wo} = \frac{\underline{10.67}}{\underline{10.67} + \underline{48.4}}$$

$$B_{wo} = \frac{\underline{10.67}}{\underline{59.07}}$$

$$B_{wo} = \underline{0.181}$$

The Molecular weight of the stack gas on a wet basis (M_s) in lb/lb-mole is:

$$M_s = M_d \text{ lb/lb-mole} (1 - B_{wo}) + 18 \text{ lb/lb-mole} \times B_{wo}$$

$$M_s = \frac{29.41}{\cancel{29.41}} \times (1 - \frac{0.181}{\cancel{0.181}}) + 18 \times \frac{0.181}{\cancel{0.181}}$$

$$M_s = \frac{29.41}{\cancel{29.41}} \times \frac{0.819}{\cancel{0.819}} + \frac{3.25}{\cancel{+ 3.25}}$$

$$M_s = \frac{27.34}{\cancel{27.34}} \text{ lb/lb-mole}$$

The average temperature of the stack ($T_{s_{avg}}$) in °R is:

$$T_{s_{avg}} = \frac{\sum T_s \text{ °F}}{\# \text{ points}} + 460$$

$$T_{s_{avg}} = \frac{6379}{48} + 460$$

$$T_{s_{avg}} = \frac{132.9}{\cancel{132.9}} + 460$$

$$T_{s_{avg}} = \underline{592.9} \text{ °R}$$

The average velocity ($U_{s_{avg}}$) of the stack in ft/s is:

$$U_{s_{avg}} = \frac{\sum V}{\# \text{ points}}$$

$$U_{s_{avg}} = \frac{2510.8}{48}$$

$$U_{s_{avg}} = \frac{52.36}{\cancel{52.36}} \text{ ft/s} \times 1 \text{ m} / 3.281 \text{ ft} = \frac{15.94}{\cancel{15.94}} \text{ m/s}$$

$$U_{s1} = 85.33 C_p \sqrt{\frac{\Delta P_1 \cdot T_{s1}}{P_s \cdot M_s}} \approx 85.33(0.78) \sqrt{\frac{0.88(59)}{30.01(2)}}$$

$$U_{s1} = \underline{41.96} \text{ ft/s}$$

The cross-sectional area of the stack (As) in ft² is:

$$As = \frac{\pi (D/4)^2}{4}$$

$$As = \frac{\pi}{4} \times (\frac{72/12}{2})^2$$

$$As = 0.7854 \times \underline{2.27} \quad 3.6$$

$$As = \underline{28.27} \text{ ft}^2$$

The volumetric stack gas flowrate on a dry basis at reference conditions (Qs) in ft³/hr is:

$$Qs = 3600 \text{ s/hr} \times Us \text{ ft/s} \times As \text{ ft}^2 \times (1 - Bwo) \times \frac{T_{ref} \text{ }^{\circ}\text{R}}{T_{avg} \text{ }^{\circ}\text{R}} \times \frac{Ps \text{ in.Hg}}{P_{ref} \text{ in.Hg}}$$

$$Qs = 3600 \times \underline{52.3} \times \underline{28.27} \times (1 - \underline{0.181}) \times \frac{537}{592.7} \times \frac{36.01}{29.92}$$

$$Qs = 3600 \times \underline{52.3} \times \underline{28.27} \times \underline{0.819} \times \underline{0.906} \times \underline{1.003}$$

$$Qs = \underline{3960113.8} \text{ ft}^3/\text{hr} \times 1 \text{ hr} / 60 \text{ min} = \underline{66001.9} \text{ ft}^3/\text{min}$$

$$Qs = \underline{66002} \text{ ft}^3/\text{min} \times 1 \text{ m}^3 / 35.31 \text{ ft}^3 \times 1 \text{ min} / 60 \text{ s} = \underline{31.2} \text{ m}^3/\text{s}$$

The total amount of particulate matter collected (Mp) in mg is:

$$Mp = \underline{251.8} \text{ mg}$$

The concentration of the particulate matter in the stack gas on a dry basis at reference conditions (Cp) in lb/ft³ is:

$$Cp = 2.205 \times 10^{-6} \text{ lb/mg} \times \frac{Mp \text{ mg}}{Vmc \text{ ft}^3}$$

$$Cp = 2.205 \times 10^{-6} \text{ lb/mg} \times \frac{\underline{251.8}}{48.4}$$

$$Cp = \underline{1.15 \times 10^{-5}} \text{ lb/ft}^3 \times 453,590 \text{ mg/lb} \times 35.31 \text{ ft}^3/\text{m}^3 = \underline{183.7} \text{ mg/m}^3$$

The emission rate of the particulate matter from the stack on a dry basis at reference conditions (ERp) in lb/hr is:

$$Erp = Cp \text{ lb/ft}^3 \times Qs \text{ ft}^3/\text{hr}$$

$$ERp = \underline{1.15 \times 10^{-5}} \times \underline{3960.114}$$

$$ERp = \underline{45.54} \text{ lb/hr} \times 1 \text{ kg/2.20 lb} = \underline{20.7} \text{ kg/hr}$$